



AVANT HYDRO
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Dianella Centre Precinct Structure Plan

Local Water Management Report



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1. EXECUTIVE SUMMARY

This **Local Water Management Report [LWMR]** has been prepared to support the *Dianella Centre Precinct Structure Plan [PSP]* (URBIS, 2026) which encompasses Lots 59, 78, 100 & 110 Grand Promenade; Lots 70 & 71 Alexander Drive; and Lot 79 Chester Avenue, Dianella, and is herein referenced to as the Study Area.

The PSP covers an area of approximately 9 ha and incorporates an existing School (Our Lady's Assumption School) and library (Stirling Libraries – Dianella) and a proposed re-development of the balance of the PSP area, including Dianella Plaza with mixed use and commercial/retail (Centre Zone) uses, Figure 1.

This LWMR provides the framework for the application of total water cycle management to the development, consistent with the Department of Water and Environmental Regulation's principles of Water Sensitive Urban Design as described in the *Stormwater Management Manual for Western Australia* (DWER, 2022) and *State Planning Policy 2.9 Water* (WAPC, 2025a) and associated design guidelines (WAPC, 2025b).

It identifies the hydrological characteristics of the site and demonstrates that the proposed re-development can be supported with the application of an appropriate water management strategy.

A summary of the LWMR design objectives is presented in Table 1.

Table 1: Summary of LWMR Design Principles and Criteria

Key Guiding Principles	
- Facilitate implementation of sustainable best practice in urban water management - Provide integration with planning processes and clarity for agencies involved with implementation - To minimise public risk, including risk of injury or loss of life. - Protection of infrastructure and assets from flooding and inundation. - To maintain the total water cycle.	
Category	LWMR Design Criteria
Water Conservation and Sustainability	- Ensure non-potable water supply systems are considered as part of an integrated water supply. - Household target water use of 100 kL/person/year. - Scheme water target use of 40-60 kL/person/year. - Use of waterwise landscaping practices both at development and lot scale.
Stormwater Management	- Maintenance of the pre-development hydrological regime including outflow rates. - Safe conveyance and management of stormwater runoff in accordance with ARR 2019 (Ball et al., 2019) - At source retention of the 5% AEP (20% AEP) and detention/retention of stormwater runoff up to the 1% AEP (100 year ARI) storm event. - Water quality treatment systems and water sensitive urban design structures designed in accordance with <i>Stormwater Management Manual for Western Australia</i> (DoW, 2007) Chapter 9 (<i>Structural Controls</i>) and <i>Australian Runoff Quality</i> (Engineers Australia, 1997). - Non-structural measures to reduce applied nutrient loads.
Groundwater Management	- Ensure adequate separation, minimum 1.5 m between building floor levels and the design groundwater level. - Manage fertiliser and pesticide application in vegetated areas. - Manage and minimise changes in groundwater levels and groundwater quality following development.
Water Quality	- Adopt nutrient load reduction design objectives for stormwater runoff. - Minimise nutrient applications to vegetated areas.

2. INTRODUCTION

2.1 BACKGROUND

Avant Hydro has been appointed by Greenpool Capital to prepare this **Local Water Management Report [LWMR]** to support the *Dianella Centre Precinct Structure Plan [PSP]* (URBIS, 2026). The PSP covers approximately 9 ha and includes Lots 59, 78, 100 & 110 Grand Promenade; Lots 70 & 71 Alexander Drive; and Lot 79 Chester Avenue, Dianella, and is herein referred to as the Study Area. The Study Area is bound by Grand Promenade to the south, Alexander Drive to the west, Waverley Street to the north and residential properties to the east.

This LWMR outlines a conceptual water management strategy for stormwater, groundwater, water supply and water quality management, at a level of detail suitable for the purpose of the local planning scheme. This is consistent with the level of water management reporting required, and the general requirements for a LWMR as outlined in Table D.1 of *State Planning Policy 2.9 Water* design guidelines (WAPC, 2025b).

2.2 STATUTORY FRAMEWORK

2.2.1 Regional Planning

The Study Area is zoned *Urban* in the Metropolitan Region Scheme, and predominantly *District Centre* in the City of Stirling Local Planning Scheme No. 3, with the south-east corner zoned as *Service Station* and north-east corner as *Hotel*. The draft City of Stirling Planning Scheme No. 4 shows the whole area zoned as *Centre*. This new planning scheme was supported by the City of Stirling council in June 2025.

There are no guiding water management documents for the Study Area.

2.2.2 Local Planning

The majority of the Study Area is located within the Dianella Centre Plan area (City of Stirling, 2012) which was prepared and adopted by the City of Stirling in 2012.

The *Dianella Centre Precinct Structure Plan [PSP]* (URBIS, 2026) predominantly proposes a mix of Mixed Use and Centre Zones with circulation and parking areas to maintain traffic flow and the retention of Our Lady's Assumption School and Stirling Libraries - Dianella, Figure 1.

This LWMR is presented in support of this PSP and develops surface water and groundwater management strategies at a local scale and has been prepared in accordance with the requirements of DWER (2017a; 2022) and WAPC (2025a&b).

2.3 KEY DESIGN PRINCIPLE AND OBJECTIVES

The LWMR uses the following documents to define its content, key principles and objectives some of which are described in further detail below:

- *Decision Process for Stormwater Management in Western Australia* (DWER, 2017a);
- *Stormwater Management Manual for Western Australia* (DWER, 2022);
- *City of Stirling On Site Stormwater Drainage Criteria* (City of Stirling, 2024);
- *State Planning Policy 2.9 – Water* (WAPC, 2025a);
- *State Planning Policy 2.9 – Water: Planning for Water Guidelines* (WAPC, 2025b); and
- *Local Governmental Guidelines for Subdivision Development* (IPWEA, 2026).

2.3.1 Decision Process for Stormwater Management in Western Australia (DWER, 2017a)

The *Decision Process for Stormwater Management in Western Australia* (DWER, 2017a) was developed to provide an approach and outcome criteria for planning and designing stormwater management systems for urban developments and retrofitting of existing stormwater management systems. The document is the third edition and was originally published in 2005 then updated in 2009.

The purpose of the decision process is to:

- Design urban stormwater management systems that reduce risk to people and property from flooding to within acceptable levels;
- Design urban stormwater management systems that mimic natural hydrological process for the relevant stormwater catchment;
- Retain natural water bodies as the receiving environments for runoff of suitable quality from minor and major rainfall events;
- Retain and plant vegetation (preferably local native species), where possible, to reduce stormwater runoff volumes and peak flow rates, reduce urban temperatures, improve water quality, increase urban biodiversity and improve aesthetics and urban amenity;
- Implement stormwater management systems and site management, maintenance and other practices to prevent, reduce and treat pollutants' and
- Design urban stormwater management systems that achieve good urban amenity and provide multiple functions.

2.3.2 Stormwater Management Manual for Western Australia (DWER, 2022)

The Water and Rivers Commission (Department of Water, DoW, 2006-2017; Department of Water and Environmental Regulation, DWER, 2017-present) released *A Manual for Managing Urban Stormwater Quality in Western Australia* in 1998 to define and practically describe Best Management Practices (BMP's) to reduce pollutant and nutrient inputs to stormwater drainage systems. The Manual also aimed to provide guidelines for the incorporation of water sensitive design principles into urban planning and design, which would enable the achievement of improved water quality from urban development.

The document was released to provide a guideline for best planning and management practices and was intended for use by Water and Rivers Commission, but also by other State and Local Government Authorities and sectors of the urban development industry.

In consultation with a working team comprising industry and government representatives a major review of the manual was completed in 2007. The revised manual was officially launched in August 2007.

Principle objectives for managing urban water in WA are stated as:

- Water Quality: To maintain or improve the surface and groundwater quality within development areas relative to pre-development conditions.
- Water Quantity: To maintain the total water cycle balance within development areas relative to the pre-development conditions.
- Water Conservation: To maximise the reuse of stormwater.
- Ecosystem Health: To retain natural drainage systems and protect ecosystem health.
- Economic Viability: To implement stormwater systems that are economically viable in the long term.
- Public Health: To minimise the public risk, including risk of injury or loss of life to the community.
- Protection of Property: To protect the built environment from flooding and waterlogging.

- Social Values: To ensure that social aesthetic and cultural values are recognised and maintained when managing stormwater.
- Development: To ensure the delivery of best practice stormwater management through planning and development of high quality developed areas in accordance with sustainability and precautionary principles

The manual was reviewed and updated in 2022 from the August 2007 version to ensure all information contained in the document was correct and up-to-date.

2.3.3 City of Stirling On Site Stormwater Drainage Criteria (City of Stirling, 2024)

The *City of Stirling On Site Stormwater Drainage Criteria* has been devised by the City of Stirling to aid private property owners who seek to develop or subdivide their property whilst managing stormwater runoff within their property.

The criteria states that on-site retention storage volumes are to be designed to cater for the 20 year ARI (5% AEP) critical storm event. However in the case that the overflow from the on-site 20 year ARI (5% AEP) stormwater system could not be safely stored within its boundaries or have an overflow path where it would not enter other private properties, then the on-site storage volumes are to be designed to cater for the 100 year ARI (1% AEP) critical storm event.

The criteria further states that no private lot connections to the City's stormwater system would be permitted unless the applicant (property owner) has provided sufficient evidence that on-site stormwater retention will be adversely affected by a shallow groundwater table.

General information of drainage infrastructure locations and soakwell sizes and capacities are also detailed in the criteria.

2.3.4 State Planning Policy 2.9 – Water (WAPC, 2025a) and Planning for Water Guidelines (WAPC, 2025b)

State Planning Policy 2.9 – Water (WAPC, 2025a) and its associated *Planning for Water Guidelines* (WAPC, 2025b) were prepared under Part 3 of the Planning and Development Act 2005 and released by the Western Australian Planning Commission in December 2025. This document repealed a number of former State Planning Policies and replaced *Better Urban Water Management* (WAPC, 2008) and Government sewerage policy which had till then been the planning instrument and process for urban water development in Western Australia.

The Policy outlines how water resource management should be integrated into the planning process with objectives:

- Protect and improve the environmental, social, cultural and economic values of the state's water resources;
- Protect public health and the long-term supply of good quality and affordable drinking water;
- Manage the risk of flooding to people, property and infrastructure;
- Ensure the secure and sustainable supply, use, disposal and re-use of water resources;
- Ensure future development is resilient to the water-related impacts of climate change; and
- Minimise future costs and protect public health by ensuring appropriate wastewater infrastructure is provided.

This Policy and its Guidelines apply to the preparation and assessment of proposals in relation to water matters, including regional and sub-regional frameworks, region and local planning schemes and scheme amendments, local planning policies, planning strategies, precinct plans, activity centre plans, structure plans, subdivision applications and development applications across Western Australia.

The most appropriate report type as detailed in WAPC (2025b) for this stage of planning is the LWMR. The stated requirements in for a LWMR in WAPC (2025b) largely mirror those of the similarly titled Local Water Management Strategy in *Better Urban Water Management* (WAPC, 2008).

2.3.5 Local Government Subdivisional Guidelines (IPWEA, 2026)

The Institution of Public Works Engineering Australia [IPWEA] Subdivisional Guidelines (Edition 3.1 – March 2026) aim to achieve best practice for managing both water quantity and quality in a sustainable way as required in *State Planning Policy 2.9 – Water* (WAPC, 2025a).

Design criteria are to be used as a guide for development of the urban water management system for strategic planning, subdivision and development. Water management requires consideration of water quality and quantity.

Post-development annual discharge (the critical 1 Exceedance per Year [EY] event) volume and peak flow should be maintained relative to pre-development conditions in all parts of the catchment where there are identified impacts on significant ecosystems. The built environment also needs to be protected from flooding (up to the 1% Annual Exceedance Probability [AEP]) and waterlogging, minimising the public risk.

Surface and groundwater quality should be at least maintained at pre-development levels (winter concentrations) and, if possible, improved. This should be achieved through a treatment train approach including non-structural measures (e.g. community education), on-site retention of the first 15 mm of rainfall and bio-retention structures/systems sized at 2% of the constructed impervious areas. As compared to a development that does not actively manage stormwater quality; the following design objectives are required:

- At least 80% reduction of the total suspended solids;
- At least 60% reduction of total phosphorus;
- At least 45% reduction of total nitrogen; and
- At least 70% reduction of gross pollutants.

Key elements of the water-sensitive design include water conservation, flood protection, management of frequent events, groundwater drainage and general drainage design principles.

3. PROPOSED DEVELOPMENT

The Dianella Centre Precinct Structure Plan [PSP] is located within the City of Stirling and covers an area of 8.95 ha. The PSP proposes re-development of the existing Dianella Plaza complex and surrounding commercial lots to provide broader and revitalised retail zones supplemented by mixed use zones for upward of 600 apartment dwellings and public realm improvements.

The proposed Mixed Use zone incorporates R-AC0 and R-AC1 R-codes with the existing Stirling Libraries – Dianella coded R80. Both the library and Our Lady’s Assumption School are proposed to remain unchanged with the associated PSP re-development.

Key elements of the PSP related to urban water management include:

- Retention and infiltration of frequently occurring rainfall events from roof areas and circulation and parking areas within underground storage and/or planted treatment areas.
- Retention and infiltration of the minor event stormwater (5% AEP / 20 year ARI) within the Study Area.
- Retention of rarer major event stormwater (1% AEP / 100 year ARI) within underground storage or temporarily within low-points in the circulation and parking areas and/or discharge to the external City of Stirling drainage system, consistent with pre-development.
- Retention of existing trees, where possible, within circulation and parking areas.
- Use of local native vegetation species in public realm areas to reduce nutrient input and conserve water resources.

A breakdown of the land use within the Study Area is presented in Table 2 below.

Table 2: Precinct Land Use Breakdown

Land Use Description	Area (ha)
Centre Zone	2.38
Mixed Use Zone	2.96
Private Community Purpose Zone	1.24
Activity Shared Zone	0.23
Circulation and Parking	2.15
Total	8.95

4. PRE-DEVELOPMENT ENVIRONMENT

4.1 EXISTING LAND USE

The majority of the Study Area as at April 2026 comprises of impervious areas either in the form of roofing or hardstand associated with the existing buildings (e.g. Dianella Plaza, Stirling Libraries – Dianella, our Lady’s Assumption School, etc.) and parking areas.

Two cleared, vacant areas are currently located in the north-west and south-west corners of the Study Area. Part of the north-west was formerly the Dianella Hotel (demolished in late-2015) and the south-west area was formerly a petrol station (demolished in 2023).

4.2 CLIMATE

The Dianella area, along with most of the Greater Perth Metropolitan Area, is characterised by a Mediterranean climate with warm dry summers and cool wet winters with rainfall predominantly occurring from May to September.

Rainfall data is provided by the following Bureau of Meteorology [BoM] rain gauges - *Perth Regional Office* (Site ID: 009034; 1880-1991), located 6.5 km south of the Study Area, and *Perth Metro WA* (Site ID: 009225; 1993-2025), located 2.5 km south of the Study Area, Figure 2.

The long-term average annual rainfall for Perth, 1880 to 2025, is 833 mm and short-term (50-year average) is 753 mm, a 10% decline from the long-term average. This is consistent with the decreasing rainfall trend across south-west Western Australia since the 1970s (DoW, 2015b) and is evident at the Perth rainfall gauges with pre-1930s annual rainfall typically exceeding 800 mm in most years whereas post-1970, there are few years with rainfall above 800 mm, Figure 2.

The seasonal rainfall distribution has also altered, with a reduction of monthly rainfall across the wetter months of May to August but no reduction or slight increases in the drier months (November to April), Figure 2 *top*.

Average annual pan evaporation is estimated at 1,925 mm for the Study Area from pan evaporation data recorded at the Department of Primary Industries and Regional Development (DPIRD) Floreat Park weather station (2009-2025). This is slightly lower than estimated pan evaporation for the Study Area from Luke et al. (1987) of 1,850 mm. Average monthly pan evaporation from DPIRD (2026) is shown on Figure 2.

4.3 TOPOGRAPHY

The topography (DoW, 2008) of the Study Area is shown on Figure 3 and shows the land generally grades south-west to north-east from about 30 mAHD to 26 mAHD, towards Waverley Street. A small portion of the western area grades outward towards the adjacent road reserves (Grand Promenade & Alexander Drive). Feature survey of the Study Area (Jurovich Surveying, 2024) is attached as Appendix B.

External drainage basins are visible in the DoW (2008) LiDAR DEM on Figure 3 to the west and north-east of the Study Area.

4.4 SURFACE GEOLOGY

Surface geology mapping by Gozzard (1986) is shown on Figure 4.

The Study Area is generally mapped as “S8” *Sand*. “S8” soils are described in Gozzard (1986) as very light grey at surface, yellow at depth, fine to medium-grained, sub-rounded quartz, moderately well sorted and of aeolian origin.

A geotechnical investigation of the proposed Stage 1 of the re-development, the western half of the Study Area, was conducted by Galt Geotechnics in April 2024 involving the excavation of 5 boreholes, BH01 to BH05, to a target depth of 1.5 m; Perth Sand Penetrometer tests adjacent to each borehole; Cone Penetration Tests [CPTs], CTPu01 to

CPTu08, to a target depth of 8 m; and 3 inverse auger infiltration tests, IT01 to IT03, at depths of 0.91 m. Test locations are shown on Figure 4.

The surface geology of the Study Area is inferred in Galt Geotechnics (2024) as Sand to 8 m depth. Loose sand was encountered within the upper 2 m of the soil profile, typically in the north of the investigation area, and was described as fine- to medium-grained and of grey, brown and yellow colour. Medium Dense to Dense Sand was encountered elsewhere underlying the investigation area and was described as comprising fine- to medium-grained gravelly sand with fine to medium sized gravel. Bore lithological logs in Galt Geotechnics (2024) typically describe the soil profile to 0.7-1 m as Fill Gravelly Sand / Fill Sand with Natural Sand thereafter to the target depth of 1.5 m.

The in-situ derived unsaturated hydraulic conductivities ranged from 7.4 to 8.7 m/day at the tested depth of 0.91 m. Avant Hydro notes that testing locations were typically in car parks where in-situ natural soils have been previously compacted for the current commercial land use.

No groundwater was encountered in boreholes but the groundwater level was inferred from CPT results at about 5.2 to 6.2 m below natural surface (Galt Geotechnics, 2024).

The geotechnical results in Galt Geotechnics (2024) aligns with regional surface geology mapping in Gozzard (1986) and are likely to similarly occur across the balance of the Study Area.

A copy of the geotechnical investigation (Galt Geotechnics, 2024) is attached in Appendix C.

4.5 ACID SULPHATE SOILS

The Study Area is generally classified as Class 1, having a moderate to low risk of Acid Sulphate Soils [A.S.S.] occurring within 3 m of natural surface but a high to moderate risk of A.S.S. at depths beyond 3 m of natural soil surface (DWER, 2017b), Figure 4.

4.6 GROUNDWATER

4.6.1 Regional Hydrogeology

The hydrogeological formations under the Study Area can be grouped into three distinct aquifers, each being assigned the name of the major geological unit contributing to it. In descending order of depth from natural surface they are: Superficial Aquifer (unconfined); Leederville Aquifer (confined) and Yarragadee Aquifer (confined).

Superficial Aquifer

The Superficial aquifer in the Study Area forms part of the Gngangara Mound and flows in southerly direction towards the Swan River. The aquifer underlying the Study Area has a maximum thickness of 40 m and three formations have been inferred from Davidson (1995) as underlying the Study Area which are, in order of increasing depth: Bassendean Sand; Gngangara Sand; and Ascot Formation. The base of the superficial formations at the Study Area is approximately -15 mAHD.

The Bassendean Sand consists of fine- to coarse-grained, moderately-sorted, sub-rounded to rounded quartz sand. The sand is mapped as highly permeable with horizontal hydraulic conductivity ranging between 10 m to 50 m/day.

Gngangara Sand beneath the Bassendean Sand consists of pale-grey, fine- to very coarse-grained, very poorly-sorted, sub-rounded to rounded quartz and feldspar (Davidson & Yu, 2008).

The Ascot Formation beneath the Gngangara Sand consists of hard to friable, grey calcarenite with thinly interbedded sand, with shell fragments commonly near the base of the formation. Sands are fine- to coarse-grained and are poorly sorted and angular to rounded in shape (Davidson, 1995).

The Ascot Formation overlies the Kardinya Shale (part of the Osborne Formation) and which is a confining bed, consisting of moderately to tightly consolidated, interbedded siltstones and shales (Davidson, 1995).

Vertical fluctuations in the groundwater table may be several metres and occur seasonally, consistent with Perth's winter-dominated Mediterranean rainfall pattern. Rainfall recharge to the superficial aquifer is 15 to 20% of total annual rainfall (Davidson, 1995). The regional aquifer salinity underlying the Study Area is 250 to 500 mg/L TDS and fresh with Nitrate concentrations generally exceeding 1 mg/L (Davidson, 1995).

Leederville Aquifer

The Leederville aquifer is found at the base of the superficial aquifer and flow south-westward beneath the Study Area (Davidson, 1995). The aquifer is multi-layered and consists of discontinuous interbedded sandstones, siltstones and shales with average horizontal hydraulic conductivity in the sandstone beds of 10 m/day and in the siltstone and shale beds of 1×10^{-6} m/day and average transmissivity of 300 to 400 m²/day (Davidson, 1995). The Leederville aquifer in the vicinity of the Study Area is fresh at less than 500 mg/L TDS (Davidson, 1995).

Yarragadee Aquifer

The Yarragadee aquifer is a multi-layered aquifer which underlies the entire Perth region and is more than 2000 m thick (Davidson, 1995). The top of the aquifer beneath the Study Area is at approximately -850 mAHD and is confined from the Leederville aquifer by the Gage Formation which underlies the South Perth Shale (Davidson, 1995). The aquifer is interbedded in similar proportion to the Leederville aquifer and has similar average horizontal hydraulic conductivities in respective sandstones and siltstone/shale beds. The flow direction beneath the Study Area is generally south/south-west (Davidson, 1995). The Yarragadee aquifer in the vicinity of the Study Area is likely fresh to marginally brackish at between 500 mg/L and 2,000 mg/L TDS (Davidson, 1995).

4.6.2 Groundwater Levels and Quality

Groundwater levels across the Study Area have been inferred from available groundwater contour mapping in WRC (1997) and DoE (2004).

The groundwater contours presented in WRC (1997) were produced from the then maximum groundwater levels recorded in the then Waters and Rivers Commission [WRC] (now Department of Water and Environmental Regulation) long-term bore monitoring network and effectively represent maximum groundwater levels [MGLs]. Across the Study Area, WRC (1997) groundwater contours suggest that groundwater flow is in a south-west direction from about 25.3 mAHD (north) to 24.7 mAHD (south) with the depth to MGL from natural surface generally greater than 2 m except in the east corner of the Study Area, Figure 5.

Groundwater contours in DoE (2004) are based on groundwater levels measured in Department of Water and Environmental Regulation bores [DWER] on May 2003, i.e. an approximate annual minima. These contours show groundwater levels beneath the Study Area at approximately 19.5 to 20.2 mAHD, a few metres lower than the groundwater minima inferred in Galt Geotechnics (2014) for April 2024 of about 23 mAHD, Figure 5.

The nearest long-term DWER bore to the Study Area is *Lakes And Wetlands Bore – 637* (Site Ref No: 61610204), located 500 m north-east of the Study Area, Figure 5. There are two distinct periods of data for this bore, being 1947 to 1976 and 1980 to 2026, with a downward shift of about 1 m over the latter period. The annual recorded groundwater maxima at the bore from 1980 to 2026 ranged from about 23.5 to 24.5 mAHD with the 2025 recorded peak of approximately 24.7 mAHD this highest recorded over this period. These groundwater levels are well below the approximate WRC (1997) MGL inferred from the bore of about 25.8 mAHD. The seasonal variation at the bore is on average about 1.2 m. Groundwater levels beneath the Study Area may be similarly lower than the MGLs inferred from WRC (1997) although levels within the bore may also be influenced by the nearby Water Corporation compensation basins, Figure 6, which have base inverts less than 24 mAHD compared to the surrounding topography at 26 to 27 mAHD.

Groundwater levels across the Study Area may also be marginally controlled by Water Corporation's nearby Waverley Street compensation basin, Figure 6, which is up-gradient of the Study Area and has a base invert of less than 23 mAHD and a low water level of 23.24 mAHD, Figure 3, about 2.5 m lower than the inferred WRC (1997) MGL, Figure 5.

No groundwater quality data has been captured at *Lakes And Wetlands Bore – 637* nor any bores at similar proximity to the Study Area.

Avant Hydro understands groundwater monitoring bores have been installed within the Study Area as part of a contamination investigation for a former dry cleaning tenancy (Section 4.9) but Avant Hydro does not have a copy of the reporting associated with this nor any collected data.

4.6.3 Groundwater Resources for Irrigation

The Department of Water and Environmental Regulation manages the groundwater of the State under the *Rights in Water and Irrigation Act 1914* (RIWI Act). The Study Area is located within the City of Stirling sub-area of the Perth Groundwater Management Area for the superficial and the Perth Confined North sub-area for the Leederville and Yarragadee aquifers. The City of Stirling sub-area generally aligns with the local government boundary but excludes areas in Balcatta, Gwelup, Stirling and Warwick which form a separate Gwelup sub-area.

The Perth Groundwater Management Area forms part of the Gngangara Groundwater Allocation Plan area. A new groundwater allocation plan (DWER, 2022) was released in June 2022 to replace the previous allocation plan (DoW, 2009). The new plan changed the allocation limits for the City of Stirling in the superficial aquifer from 11,150,000 kL/year in DoW (2009) to 15,121,000 kL/year in DWER (2022) of which only 6,338,000 kL/year is available for general licencing. The majority of the allocation in the sub-area is categorised as “exempt”, mostly related to estimates of water use in domestic garden bores and market gardens, with a further 2,550,000 kL/year allocated for public water supply.

The DWER groundwater allocation limit and water allocations applicable to the Study Area are shown in Table 3 based on a Resource Allocation Report from DWER as at 28 November 2025.

Table 3: DWER Groundwater Resource Allocation and Limit, November 2025

GW Sub -Area	Aquifer	Allocation Limit Licensable component, (kL/yr)	Allocated (kL/yr)	Additionally Requested (kL/yr)	% Allocated, committed & requested
City of Stirling	Superficial Swan	6,338,000	8,073,058	0	127
Perth North Confined	Leederville	1,245,000	1,451,667	2,253	117
Perth North Confined	Yarragadee	80,000	80,000	0	100

A water supply source is required for irrigation of planted areas and for construction / dust suppression. This water can be sourced either from scheme water or groundwater abstraction from the superficial aquifer.

Scheme water can be a viable option if the required allocation is low and only required for a short-term period to establish vegetation. Otherwise, it can be costly and is not consistent with water efficiency and water sensitive urban design principles and guidelines.

Groundwater abstraction from the superficial aquifer is generally the preferred non-potable water supply source, however, all groundwater aquifers beneath the Study Area are fully or over allocated. Water trading is an alternative method to obtain a Licence to Take Water from a third party but the majority of existing licences within the City of Stirling sub-area are either held by the City of Stirling, education institutions or sporting clubs and limited water may be available for trading. There are numerous contaminated sites within the Study Area and groundwater modelling and further analytical testing is recommended to ensure abstraction activities do not significantly impact existing contaminant plumes within the vicinity of the Study Area and to ensure that groundwater is suitable for irrigation.

The development zones within the Study Area will remain in private ownership as will the associated drainage assets. Therefore, should a groundwater licence be obtained, it will be retained by the developer as no drainage assets will be transferred to the City of Stirling.

A reticulation system is present at Dianella Plaza to irrigate carpark trees and it is likely these small irrigation volumes are supplied from scheme water.

4.7 SURFACE WATER

There are no watercourses which flow through the Study Area nor are there any open water bodies located within the Study Area.

The Study Area is located within the Bayswater Main Drain sub-catchment of the Swan-Canning catchment (DBCA, 2018). The Bayswater Main Drain [BMD], also referred to as Bayswater Brook, is a permanently flowing drainage network of both open and piped drains and several compensation basins [CBs]. The BMD was formerly a number of natural watercourses that were modified to allow development of the area with the BMD generally flowing north-west to south-east towards the Swan River (DBCA, 2018). The BMD is managed by Water Corporation for flood protection of the surrounding commercial and residential areas. Local government managed drains feed into the BMD and several of the compensation basins are located within parks and recreation reserves managed by the local government (DBCA, 2018).

The Study Area is located adjacent to the Waverley Street CB, Figure 6. City of Stirling managed drainage infrastructure is shown on Figure 6 *right* and suggests there are four drainage discharge points from the Study Area. Of these, 3 are in the north-east drain to the Waverley Street drainage system and thereafter to the Waverley Street CB with the fourth in the south-west of the Study Area that drains to the Alexander Drive drainage system and thereafter to a City of Stirling drainage sump at the corner of Grand Promenade and Alexander Drive, Figure 6.

No existing internal drainage details have been provided to Avant Hydro for the Study Area, however, details in MPA (2023) suggest that existing roof areas discharge to the carpark stormwater system and not separate underground storage units. It is unclear to Avant Hydro whether there is a direct connection of the Dianella Plaza carpark stormwater drainage system to the City of Stirling drainage as shown on Figure 6 *right*, and whether any of the carpark pits shown on the feature survey, Appendix B, also function as soakwells and retain and infiltrate stormwater runoff from relatively frequent rainfall events within the carpark. In rarer events, stormwater will flow with the grade of the land which for the eastern half of Dianella Plaza is south-west to north-east towards Waverley Street and the associated discharge points to the City of Stirling drainage system, Figure 6 *right*. Most of the western half of the Study Area drains radially outward towards Alexander Drive / Grand Promenade and it is unclear where stormwater runoff generated within these areas is wholly retained within the Study Area or there are outlets to nearby City of Stirling drainage infrastructure on Alexander Drive and Grand Promenade.

It is expected that all stormwater runoff currently generated within Our Lady's Assumption School is retained and infiltrated on-site.

4.8 WETLANDS AND VEGETATION

There are no mapped Geomorphic wetlands (DBCA, 2025) within or in close proximity to the Study Area. The nearest mapped wetland is Water Corporation's Morley Drive Compensation Basin, Figure 6 *left*, which is located 400 m north of the Study Area and is mapped in DBCA (2025) as a Conservation sumpland.

There are no Bush Forever sites located within or in close proximity to the Study Area with then nearest site located in Dianella Regional Open Space, 400 m north of the Study Area.

4.9 CONTAMINATED SITES

Current / former service stations located in the south-east and south-west of the Study Area corners of the Study Area are classified on the Contaminated Sites Database as *Remediated for Restricted Use* due to the presence of hydrocarbons in soil and groundwater. Some historical remedial works were conducted but residual contamination was considered to remain in the soil and was still suitable for commercial/industrial land use (MPA, 2023). MPA (2023) notes that this contamination is between 5 to 8 m below natural surface and is unlikely to be impacted during any proposed re-development works.

The former dry cleaner tenancy in Dianella Plaza is also classified as *Remediated for restricted use* due to use of chlorinated solvents (Tetrachloroethylene) associated with dry cleaning activities. Findings summarised in MPA (2023) indicates that the Department of Health were satisfied the tenancy was suitable for commercial use as the chlorinated solvents in groundwater no longer posed a public health risk to site users.

Some fragments of anthropogenic waste including suspected asbestos-containing fibre cement sheet fragments were noted in MDA (2023) in the surface soils associated with the now demolished Dianella Hotel in the north-west of the Study Area.

The Environmental and Hazardous Materials Assessment in MPA (2023) identified some hazardous materials (asbestos, synthetic mineral fibres) and further investigation is recommended prior to commencement of any future refurbishment and/or demolition works to identify and removed said hazardous materials.

5. WATER SUSTAINABILITY

5.1 WATER SUPPLY

The Study Area is currently provided scheme water via an existing DN100 reticulation main on the southern verge of Waverley Street; and DN150 reticulation mains on the western verge of Alexander Drive and northern verge of Grand Prom.

The site servicing report for Stage 1 (Colliers, 2026) notes that upgrades to the surrounding Water Corporation infrastructure and the establishment of a new service for the premises is required to support the proposed development. Stage 1 of the re-development generally incorporates the mixed use zones and is currently only serviced via the DN100 main on Waverley Street. Colliers (2026) indicates that further connections are likely required from the Alexander Drive and Grand Promenade mains to support these areas and satisfy the expected fire servicing requirements.

A dead DN100 reticulated connection which traverses through the Study Area will also need to be completely removed or capped (Colliers, 2026).

5.2 WASTEWATER MANAGEMENT

The Study Area is generally currently serviced via 2 DN100 VC lot connections located in the south-east and north-east of the Study Area which connect to a DN900 transfer branch within the Waverley Street road reserve (Bedford Bypass Sewer Main), and a DN225 lot connection in the south-west which connects to a DN230 VC gravity pipe on Grand Prom which ultimately connects to the DN1370 transfer main on Alexander Drive (Colliers, 2026).

Further detail on water supply and wastewater is to be provided in a servicing report for the PSP area.

5.3 WATER USE EFFICIENCY MEASURES

The *State Planning Policy 2.9 Water* (WAPC, 2025a) was developed to ensure that urban development is located adequately, serviced with appropriate wastewater, stormwater and groundwater management infrastructure and contributes towards the management of water quality and quantity, ecological health and the social and cultural values of water resources. This section addresses water conservation measures and fit for purpose non-potable supply.

The Water Conservation Strategy for the development is detailed below, with initiatives to be considered for adoption:

- Use of water-wise practices, including water efficient fixtures and fittings (WELD rated taps, showerheads, toilets, appliances, rainwater tanks) and water-wise landscaping including native plant species;
- Residential apartments in Mixed Use Zones to be constructed to current 7-star building standards as per the current National Construction Code [NCC]. The NCC 2022 was published on 01 October 2022 and incorporates a minimum 7-star energy efficient rating for new dwellings. NCC 2022 was adopted on 01 May 2023 by the WA Government with the residential energy efficiency provisions mandatory from 01 May 2025.
- Use of native, low water-use vegetation within planted areas with mulches and ground covers to be used to increase the efficiency of irrigation and conserve water. The associated irrigation system is to be designed to water wise principles.

The proposed conservation measures aim to reduce scheme water consumption in the development area within the constraints of the site.

6. STORMWATER MANAGEMENT

6.1 DESIGN OVERVIEW

Local stormwater management is proposed to be consistent with current water sensitive design practices and to meet key LWMR objectives and criteria as detailed in Table 1 and designed in accordance with the *Decision Process for Stormwater Management in Western Australia* (DWER, 2017a) and the *City of Stirling On Site Stormwater Drainage Criteria* (City of Stirling, 2024).

The stormwater system for the Study Area should be based on the management of the ‘small’, minor and major events.

‘Small’ event management concentrates on the first 15 mm of rainfall (approximately the 1 EY 1 hour event) and represents over 90% of rainfall events. Runoff generated from the first 15 mm of rainfall can mobilise substances such as soluble materials, silts, oils and grease and therefore should be retained and managed at-source (if possible) to prevent transport of pollutants to downstream receiving environments (DWER, 2017a). Stormwater runoff from roofs should be retained within underground storage units (e.g soakwells, StormTrap, GRAF cells, etc.) and stormwater from pavements, bitumen, hardstand, etc. should be retained and infiltrated either in underground storage units or within vegetated treatment structures such as rain gardens or tree pits.

The minor drainage system is designed as a system of pipes, kerbs, gutters, etc. and has the capacity to convey stormwater runoff generated by low frequency storms, typically less than the 10% AEP (10 year ARI) for commercial/industrial areas and 20% AEP (~ 5 year ARI) for residential areas. For the Study Area, the minor event should be considered the 5% AEP (20 year ARI) as the City of Stirling (2024) requires the on-site stormwater retention system be designed to manage the critical 5% AEP storm event.

The major drainage system is designed as the arrangement of stormwater and civil design elements planned to provide a safe passage of stormwater runoff from extreme rainfall events (up to the 1% AEP) to catchment low points. There are existing private stormwater connections to the City of Stirling’s drainage system from the Study Area, Figure 6 right, in the north-west (3) and south-west (1). The north-west outlets discharge to Water Corporation’s Waverley Street CB north of the Study Area and the south-west outlet discharges to the City of Stirling drainage sump on Alexander Drive.

City of Stirling (2024) notes the following: *The onsite retention storage volume is to be designed to cater for a 1 in 20 ARI (5% AEP) critical storm. In the case that the stormwater system for a 1 in 20 ARI (5% AEP) would overflow and runoff from the site could not be safely stored within its boundaries or have a safe overland path where it would not enter other private properties, the development shall be designed to cater for the 1 in 100 ARI (1% AEP) critical storm*, however, City of Stirling (2024) also notes that no private lot connections to the City’s stormwater system are permissible.

Water Corporation has advised that stormwater discharge from the Study Area should be limited to the pre-development flow rate with no overland flow into the Water Corporation drainage system in a minor storm event – this should be managed within the pit-pipe local government drainage system. Overland flows into the Water Corporation system in excess of the minor event were considered by Water Corporation as both likely and permissible.

In this LWMR, Avant Hydro has conservatively assumed all stormwater runoff up to the major event (1% AEP) is retained within the Study Area, either in WSUD structures (‘small’ event), underground storage and/or above-ground in depressions within car park areas. Whilst there are numerous stormwater connection points as detailed above, Avant Hydro does not have any details of the internal Study Area drainage system and its connectivity to the local government drainage system except for drainage pit locations as shown in the feature survey (Jurovich Surveying, 2024; Appendix B). The general grade of land, particularly the eastern half of the Study Area, is towards these connection points and stormwater runoff pre-development likely discharges to the local government piped drainage system as piped flow and possibly overland flow in rarer storm events.

Stirling Libraries – Dianella is owned and operated by the City of Stirling and is connected to the Waverley Street drainage system via a pipe network across the private Dianella Plaza landholding. This connection will need to be maintained post-development with the existing pipe network likely relocated further west through the future Activity Shared Zone.

Connections from the Study Area to the City of Stirling drainage system are to be investigated further as part of detailed design and any future Subdivision and Development Water Management Plan(s), in discussion with the City of Stirling.

Avant Hydro assumes stormwater runoff generated within the Our Lady's Assumption School is retained and infiltrated on-site and is not considered further in this LWMR.

6.2 DRAINAGE CATCHMENTS AND STORMWATER MODELLING PARAMETERS

Preliminary post-development stormwater drainage catchments have been determined from the proposed precinct land use, Table 2 and Figure 1, and are shown on Figure 8.

Indicative storage volumes to be retained within each catchment (up to the 1% AEP) have been estimated based on the following assumptions:

- A runoff coefficient of 95% as the precinct land use zones will comprise predominantly of impervious areas including roofs, pavements, bitumen and hardstand.
- Rainfall was assumed to be both spatially and temporarily uniform. BoM (2016) design rainfalls have been adjusted to 2030 based on climate change factors for the Study Area as shown on the Australian Rainfall and Runoff [ARR] Data Hub.
- The required storage volumes up to the major event (1% AEP) were assumed to be retained and infiltrated within underground storage.
- Underground storage units modelled as 1 m x 1 m x 1 m with 80% of the base of the units open (equivalent infiltration area).
- A constant infiltration rate of 5 m/day was used based on Galt Geotechnics (2024) results for compacted in-situ soils and is approximately equivalent to the Green-Ampt equation.

6.3 STORMWATER MODELLING RESULTS

Catchment areas, equivalent impervious areas [EIA] and indicative storage areas, depths and volumes for each stormwater drainage catchment is summarised in Table 4 and shown on Figure 6.

The calculated critical duration for all catchments was 2 hours for the minor event (5% AEP) and 6 hours for the major event (1% AEP).

Stormwater storage volumes required are indicative only and assume all stormwater generated within each catchment is retained and infiltrated in underground storage. Should stormwater be partially retained above-ground in depressions in parking areas or discharge to the existing City of Stirling drainage system, drainage calculations should be revised to account for potentially smaller underground storage area and associated infiltration area as part of detailed design and documented in any associated future *Subdivision and Development Water Management Report* [SDWMR].

City of Stirling (2024) requires stormwater from roofs to be managed separately to stormwater from other impervious areas including car parks and Avant Hydro assumes this approach will be applied to the Study Area.

Table 4: Indicative Storage Requirements

Catch ID	Catch Area (m ²)	EIA (m ²)	Storage Area (m ²)	Infiltration Area (m ²)	Minor Event (5% AEP)		Major Event (1% AEP)	
					Depth (m)	Volume (m ³)	Depth (m)	Volume (m ³)
AS1	2,255	2,145	125	100	0.60	75	0.95	120
C1	12,000	11,400	650	520	0.60	390	1.00	650
C2	1,815	1,725	100	80	0.60	60	1.00	100
C3	525	500	30	25	0.55	16	0.90	27
C4	465	440	25	20	0.60	15	1.00	25
C5	2,660	2,525	145	115	0.60	85	1.00	145
C6	3,310	3,145	180	145	0.60	110	1.00	180
C7	2,520	2,395	135	110	0.60	80	1.00	135
MU1	3,245	3,085	175	140	0.60	105	1.00	175
MU2	20,050	19,050	1,090	870	0.60	655	1.00	1,090
MU3	4,435	4,215	240	190	0.60	145	1.00	240
MU4	1,845	1,755	100	80	0.60	60	1.00	100
P1	5,375	5,105	290	230	0.60	175	1.00	290
P2	9,315	8,850	510	410	0.60	305	1.00	510
P3	12,435	11,815	680	545	0.60	410	1.00	680

7. GROUNDWATER MANAGEMENT

7.1 DESIGN CRITERIA

Groundwater management for the Study Area has been prepared in line with the design criteria presented in the *Stormwater Management Manual for Western Australia* (DWER, 2022a):

- Protect infrastructure and assets from flooding and inundation by high seasonal groundwater levels and/or soil moisture.
- Protect groundwater-dependent ecosystems from the impacts of urban runoff.
- Manage and minimise changes in groundwater levels and groundwater quality following development.
- Adopt nutrient load reduction design objectives for discharges to groundwater.

7.2 MANAGING GROUNDWATER LEVELS

Groundwater management is generally required to ensure there is a minimum separation of 1.5 m between finished surface level and the design groundwater level [DGL].

In the absence of site-specific monitoring data, the WRC (1997) groundwater contours have been used as the DGL for this LWMR and show there is currently 2 to > 5 m separation to the DGL. As the WRC (1997) groundwater contours typically represent 'Maximum Groundwater Levels', most of which were recorded in the 1970s/80s, it is likely that site-specific groundwater levels will be lower than those inferred from WRC (1997).

Post-development, the landform of the Study Area may be slightly recounted to suit the proposed development but will still likely achieve the minimum separation requirement. Given the separation to groundwater, groundwater level management measures are likely not required across the Study Area but should be reviewed as part of the detailed design process in any *Subdivision and Development Water Management Report* [SDWMR] after review and consideration of any further geotechnical investigations, site-specific monitoring data and detailed site earthworks.

As stormwater retention via infiltration forms a significant component of the proposed stormwater strategy within the Study Area, it is recommended that any underground storage devices (e.g. soakwells, GRAF drainage cells, StormTrap, etc.) have a minimum 1 m clearance from their base to the DGL.

7.3 GROUNDWATER QUALITY

Groundwater quality management will be achieved by infiltrating stormwater runoff treated via non-structural and structural management measures.

8. WATER QUALITY MANAGEMENT

The effective implementation of the structural and non-structural controls as part of the development will enhance water quality infiltrating from the Study Area to the underlying regional groundwater table.

8.1 NON-STRUCTURAL SOURCE CONTROLS

Non-structural source controls to reduce nutrient export from the Study Area will focus on reducing the need for nutrient inputs into the landscape. The following strategies are proposed:

- Local native plants make up a minimum 50% of the planted areas. Any non-local species will be selected for drought tolerance and low fertiliser requirements; and
- Maintenance practices such as sweeping and pit eduction to remove sediment build-up. Future *Subdivision and Development Water Management Reports* [SDWMRs] will outline the schedule and cleaning requirements for sweeping/pit eductions.

8.2 STRUCTURAL SOURCE CONTROLS

The *Stormwater Management Manual for Western Australia* (DWER, 2022) outlines expected pollutant removal efficiencies for detention/retention systems, Table 5.

Structural source controls complement the non-structural source controls and may include flush kerbing, tree pits and rain gardens within circulation and parking areas.

Table 5: BMP Water Quality Performance

Parameter	Structural Controls Nutrient Output Reduction ¹
	Detention/Retention Measures
Total Suspended Solids	65-99%
Total Phosphorus	40-80%
Total Nitrogen	50-70%
Gross Pollutants	> 90%

Note 1. Typical Performance Efficiencies via DWER (2022)

In areas such as the Study Area with sandy soils and depth to groundwater, most rainfall is infiltrated at-source and treated by current best management practices (ie. Tree pits / rain gardens) and achieve modest pollutant removal efficiencies which may be lower than the typical performance efficiencies in DWER (2022).

Tree pits and/or rain gardens with flush kerbing can be utilised as an alternative to traditional soakwells or underground storage to capture, treat and infiltrate the small event rainfall (first 15 mm) in circulation and parking areas. These structural controls should be considered as part of detailed design and documented in an future SDWMRs. Tree pits / Rain gardens, if implemented, should be planted with suitable water tolerant vegetation to provide water quality treatment and should dry out in less than a day after rain ceases. Typical details on plant selection, density and distribution for south-west Western Australia are detailed in Monash University (2014).

8.3 DISEASE VECTOR AND NUISANCE INSECT MANAGEMENT

Structural stormwater management systems are designed to minimise the risk of chironomid midge and mosquito breeding. Infiltration and evapotranspiration will prevent stormwater pooling for longer than four days (96 hours) in late spring to early autumn will prevent completion of the larval stages of the mosquito life cycle (DWER, 2022a), as per requirement of the Department of Health.

9. IMPLEMENTATION

Implementation of this Local Water Management Report involves defining the roles and responsibilities of the developer and local authority, outlining future documentation required to support the development and defining operation, monitoring and maintenance of the stormwater system.

9.1 ROLES AND RESPONSIBILITIES

The entirety of the Study Area will remain in private ownership. The construction and initial operation of the stormwater management system will be the responsibility of the developer(s). Thereafter, the ongoing maintenance will either remain with the developer or will be relegated to the lessor or an appointed development manager.

Preparation of any future *Subdivision and Development Water Management Report(s)* [SDWMR] will be the responsibility of the developer(s).

9.2 CONSTRUCTION MANAGEMENT

9.2.1 Dewatering

Dewatering may be required for sewer installation but is to be confirmed by the civil engineer and contractor. Given the potential depth of constructions, dewatering, if to occur, would only be in the superficial aquifer.

Prior to commencement of any dewatering, the construction contractor may need to apply for and obtain from DWER a "Licence to Take Water". A licence is not required for dewatering if the pump rate does not exceed 10 L/s over a period of less than 30 days and the volume of water taken over the period does not exceed 25,000 kL.

Dewatering will need be carried out in accordance with the licence conditions should a licence to take water be required. Where possible, construction will be timed to minimise impacts on groundwater and any dewatering requirement.

9.2.2 Acid Sulphate Soils

Figure 3 generally shows a moderate to low risk of A.S.S. occurring within 3 m of natural surface.

A.S.S., if encountered, will need to be investigated and managed in accordance with the applicable DWER *Acid Sulphate Guidelines for Identification and Investigation* (DER, 2015a) and *Treatment and Management* (DER, 2015b) of Disturbed Acid Sulphate Soils. Specific methods for treatment and holding times for A.S.S. are specified in these guidelines.

9.3 STORMWATER SYSTEM OPERATION AND MAINTENANCE

The stormwater drainage system within the proposed development will require maintenance to ensure correct operation and minimise risk of inundation of the Study Area and surrounding properties. It is considered the following operating and maintenance practices will be required periodically:

- Inspection and removal of debris, litter and sediments surrounding pipe inlets/outlets to prevent blockages.
- Regular sweeping of circulation and parking areas to reduce particulate build-up on impervious surfaces.
- Maintenance of planted areas including plant condition and weeds and cleaning of sediment at base.

The operating and maintenance schedule required is presented in Table 6.

Table 6: Maintenance Schedule for Drainage Infrastructure

Item	Maintenance Interval		
	Quarterly	Bi-annually	As required
Underground Storage / Pit-Pipe Drainage			
Street sweeping to reduce particulate build-up			✓
Removal of debris to prevent blockages	✓		
Inspection of sediment and rubbish in manholes	✓		
Planted Areas (Tree Pits/Rain Gardens)			
Inspect for erosion + sediment accumulation		✓	
Assess health of vegetation. Remove dead plants and replace where necessary.		✓	
Inspect for standing water 1 day after rainfall events			✓
Removal of sediment and leaf litter layer build up.			✓

9.4 MONITORING PROGRAM

Given the minimal changes to the overall land use across the Study Area post-development compared to pre-development, there is likely to be minimal changes to the overall groundwater quantity and quality and therefore no post-development monitoring is proposed.

9.5 FUTURE WATER MANAGEMENT REPORTING

A *Subdivision and Development Water Management Report* [SDWMR] forms part of the planning process outlined in *State Planning Policy 2.9 – Water* (WAPC, 2025a&b). Any future SDWMR(s) will build on the water management strategies presented in this LWMR and provide further detail on the following areas:

- Design of water quality treatment structures and underground storage devices as outlined in the *Stormwater Management Manual* (DWER, 2022);
- Refinement of catchment areas and treatment/storage locations, dependent on final site earthworks.
- Confirmation of post-development discharge to existing external drainage based on detailed existing drainage design detail and final post-development site earthworks following discussions with the City of Stirling.
- Confirmation of water source for irrigation of planted areas.

Any SDWMR(s) are to be prepared consistent with the requirements outlined in Table E.1 of SPP 2.9 design guidelines (WAPC, 2025b).

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Water Corporation (2025) *Drainage Gravity Pipe (WCORP-080), Drain Inlet (WCORP-290), Drainage Compensating Basi (WCORP-079) and Drain Open Channel (WCORP-083)*. Data Extracted 01 December 2025.

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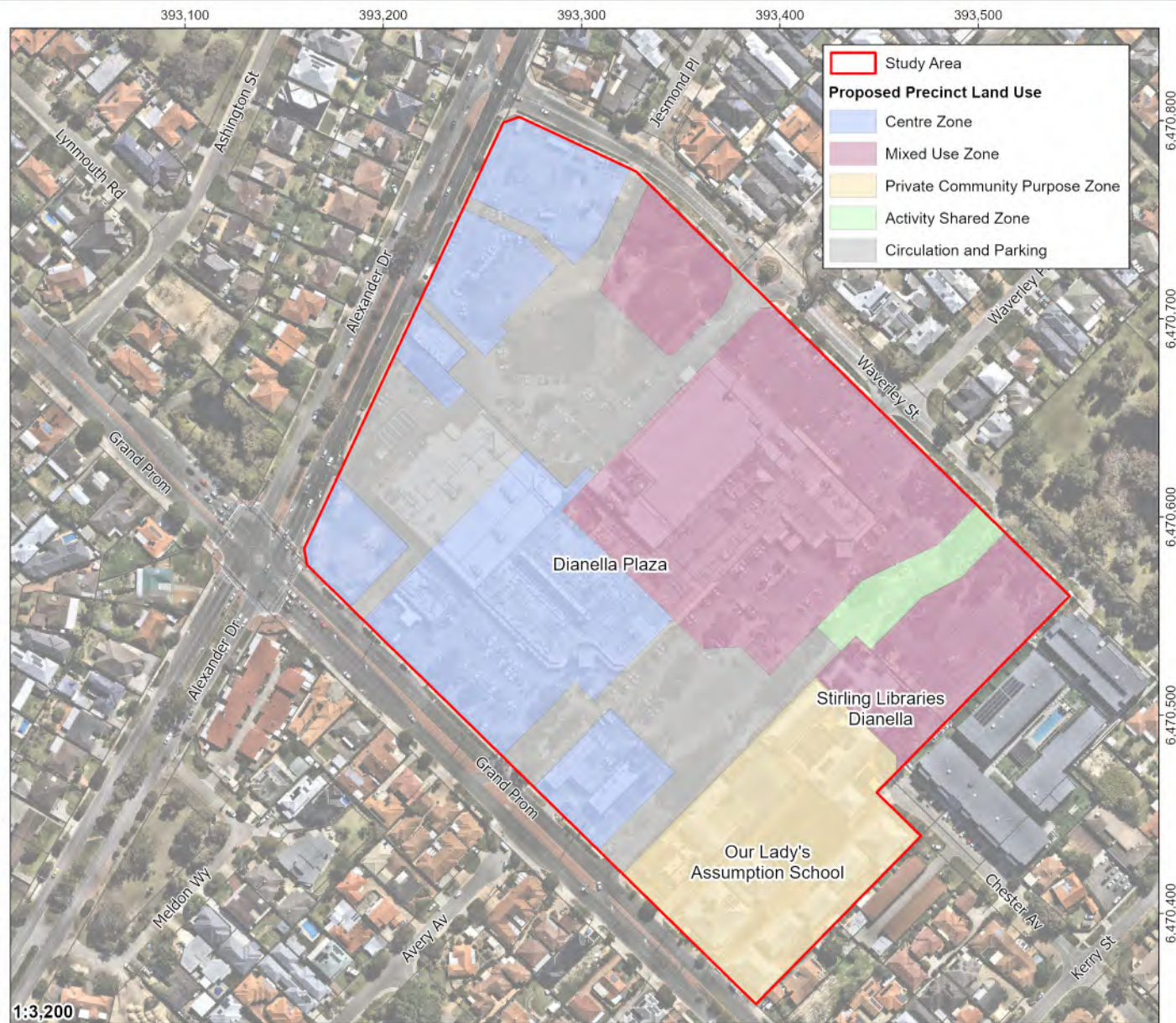
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FIGURES

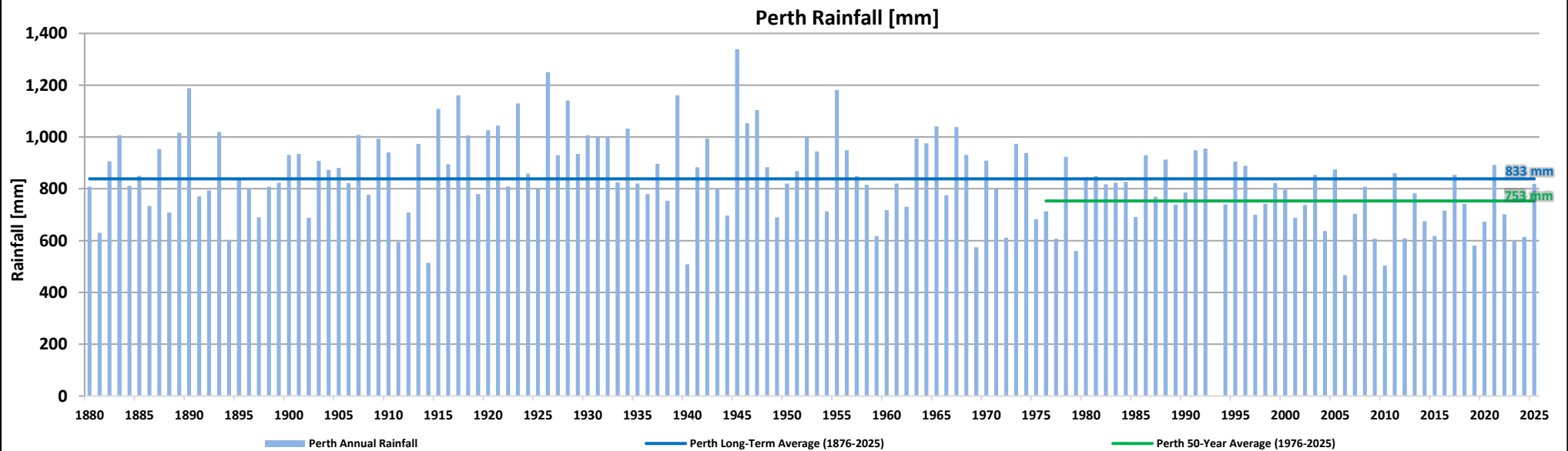
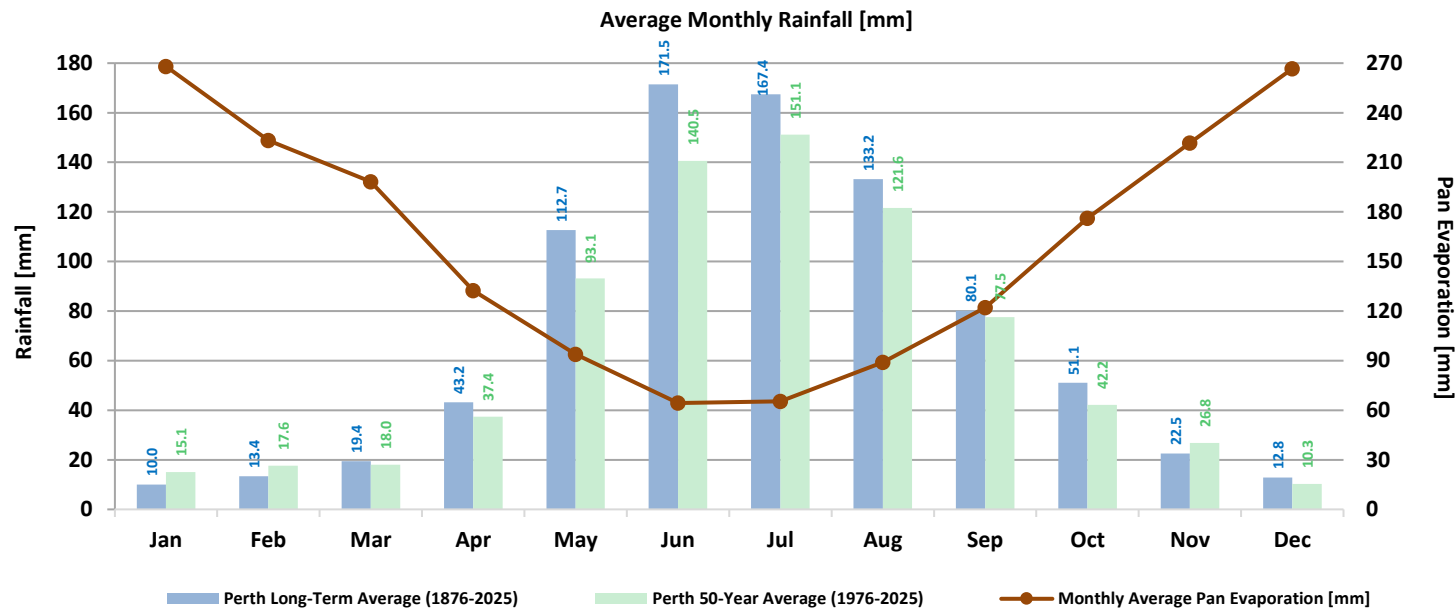




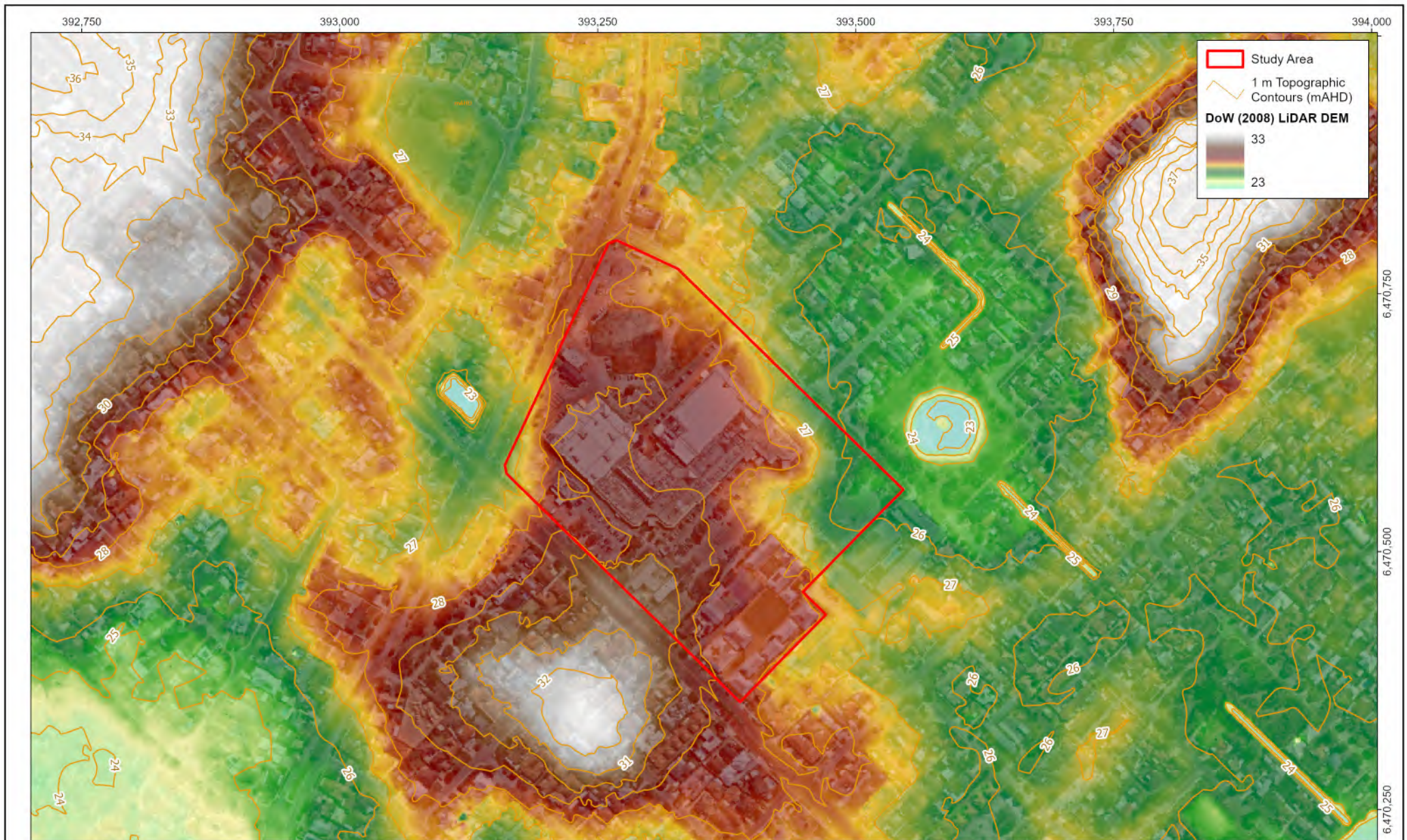
Data Source: Street Express (2012); NearMaps (2025) 21 September 2025; URBIS (2026).

GDA2020 MGA Zone 50



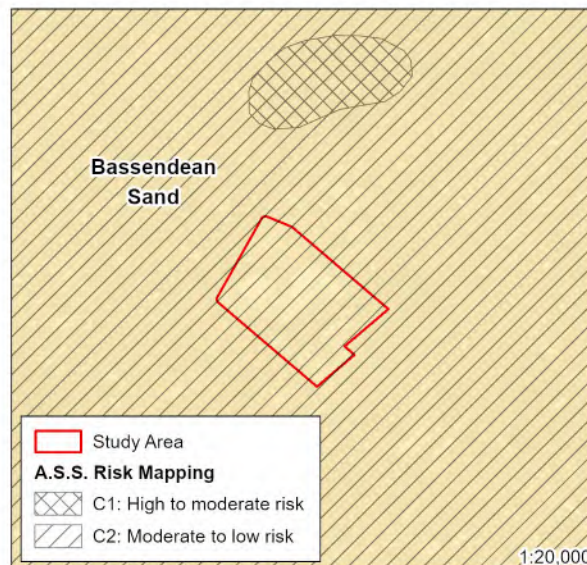


Data Source: BoM (2026) Climate Data Online - Perth Regional Office (009034) & Perth Metro WA (009225); DPIRD (2026) Floreat Park (FL) Pan Evaporation



Data Source: DoW (2008); NearMaps (2025).

GDA2020 MGA Zone 50



Lithological Classification

S8 Sand - very light grey at surface, yellow at depth, fine to medium-grained, sub-rounded quartz, moderately well sorted, of aeolian origin.

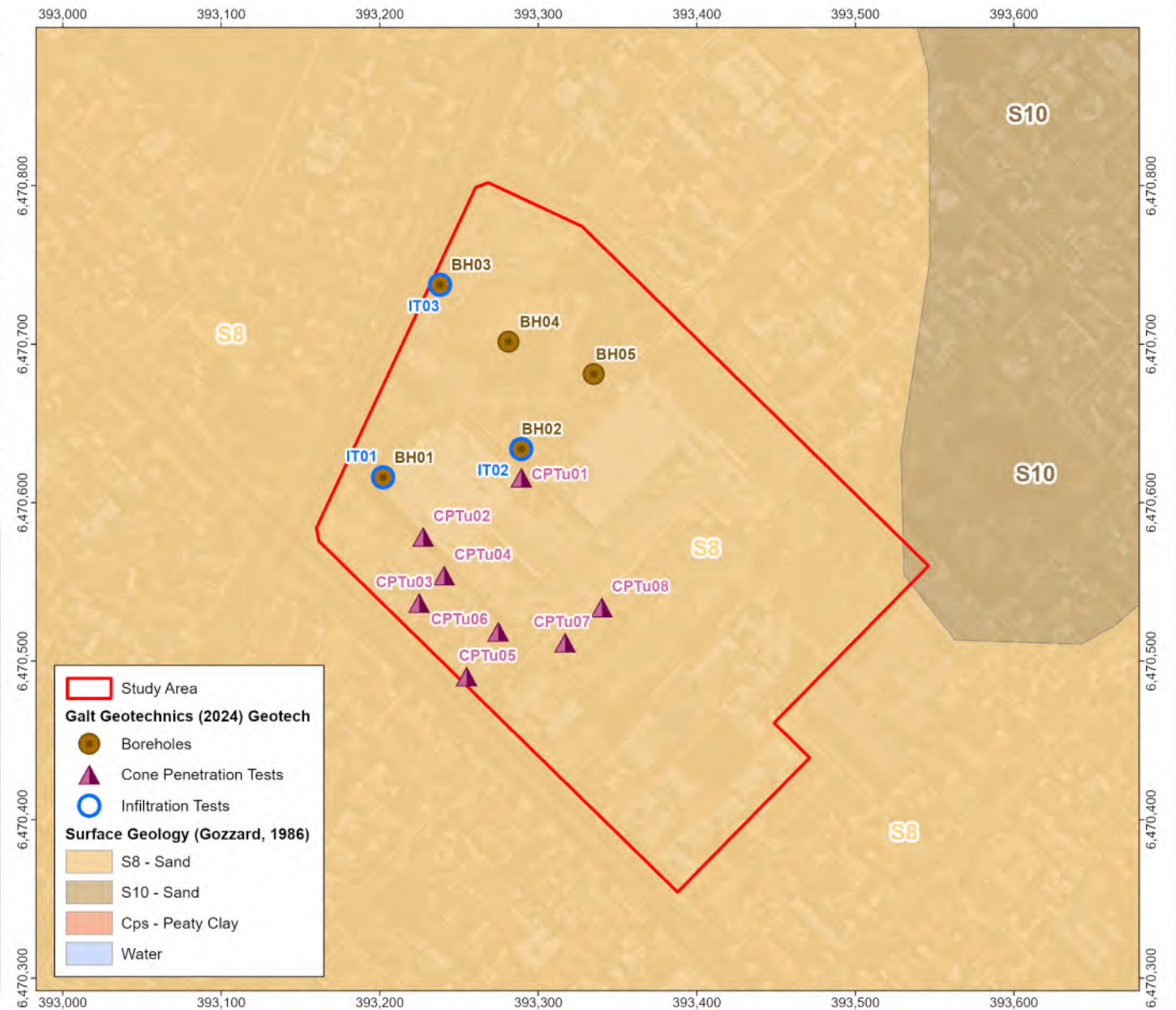
S10 Sand - as S8 (Thin Bassendean Sand over Guildford Formation).

Bassendean Sand

Basal conglomerate overlain by dune quartz sand with heavy mineral concentrations.

Acid Sulphate Soils

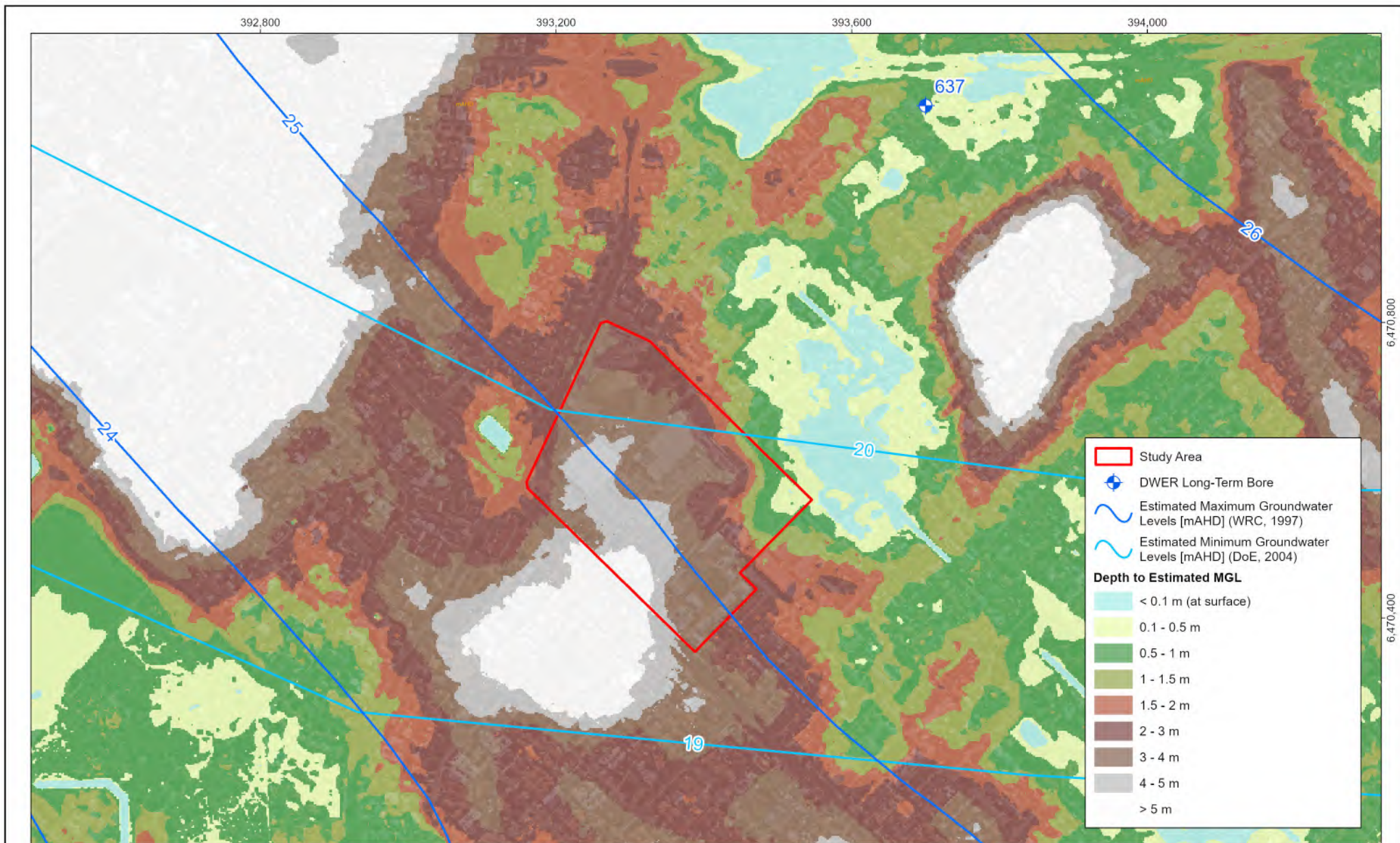
Class 2 - Moderate to low risk of A.S.S. occurring within 3 m of natural soil surface that could be disturbed by most land development activities (activities disturbing soils at depths greater than 3 m carry a high to moderate risk of disturbing A.S.S.).



Data Source: Gozzard (1986) Environmental Geology Series *Perth*; A.S.S. Risk Mapping (DWER, 2017b); NearMaps (2025).

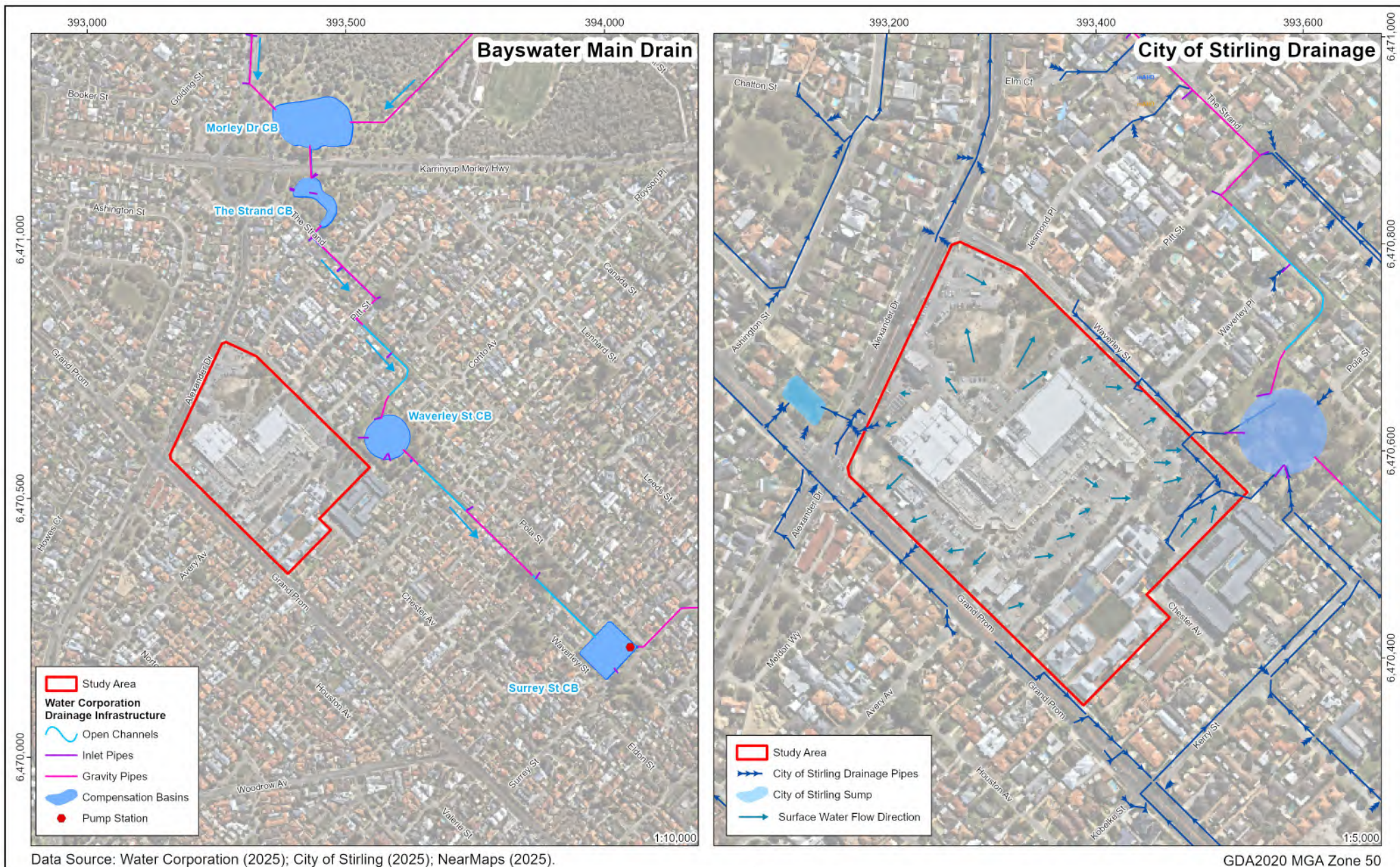
GDA2020 MGA Zone 50

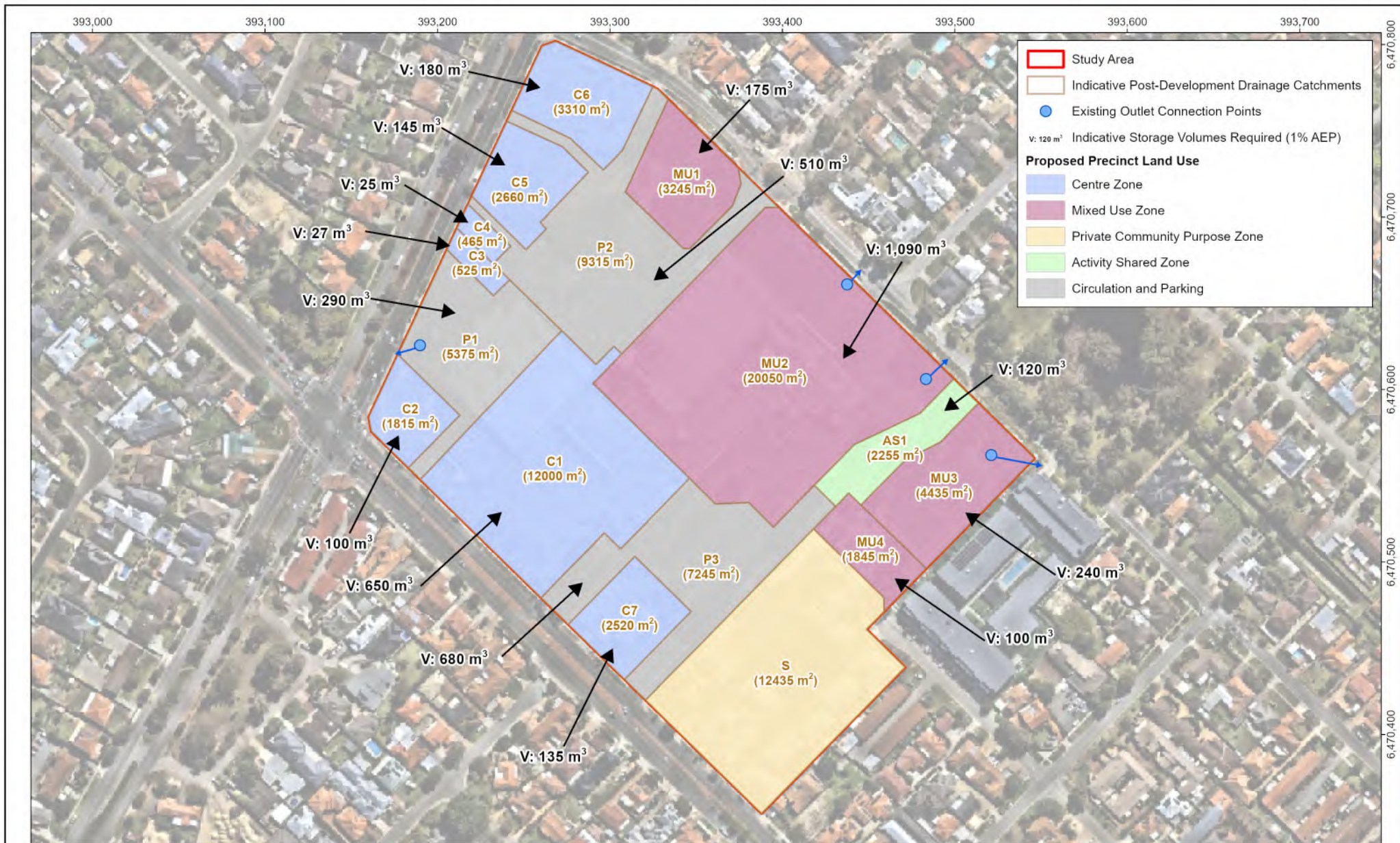




Data Source: DoW (2008); WRC (1997); DoE (2014); NearMaps (2025).

GDA2020 MGA Zone 50





Data Source: NearMaps (2025); URBIS (2026).

GDA2020 MGA Zone 50

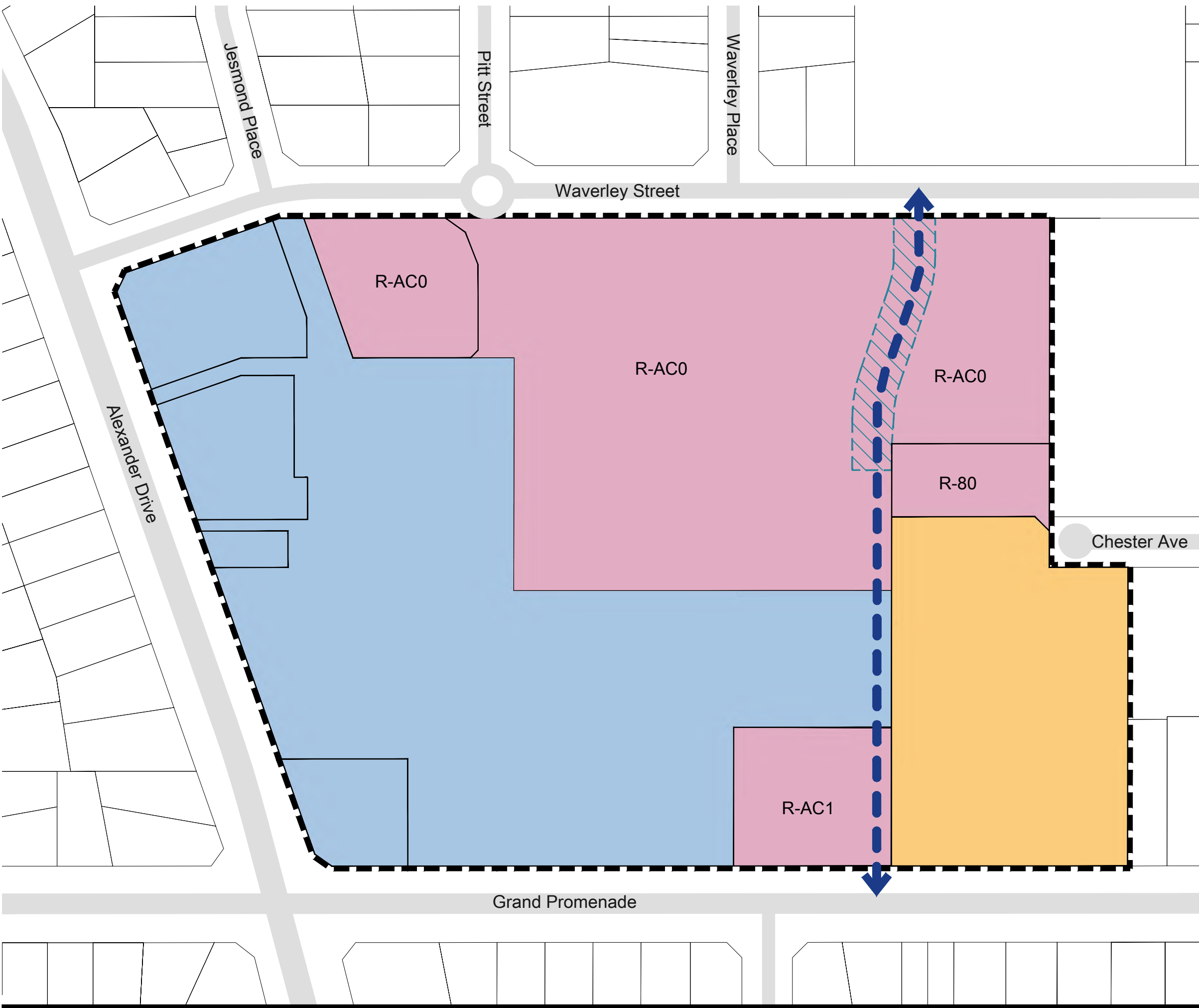
APPENDICES



APPENDIX A

Precinct Structure Plan (URBIS, 2026)





- Legend**
- Precinct Structure Plan Area
 - Centre Zone
 - Mixed Use Zone
 - Private Community Purpose Zone
 - Lowick Street Private Access Road
 - Shared Zone



Precinct Structure Plan Map - Part 1
Dianella Plaza Precinct Structure Plan

Level 8, 1 William Street | Perth WA 6000 Australia | +61 8 9346 0500 | URBIS Ltd | ABN 50 105 256 228

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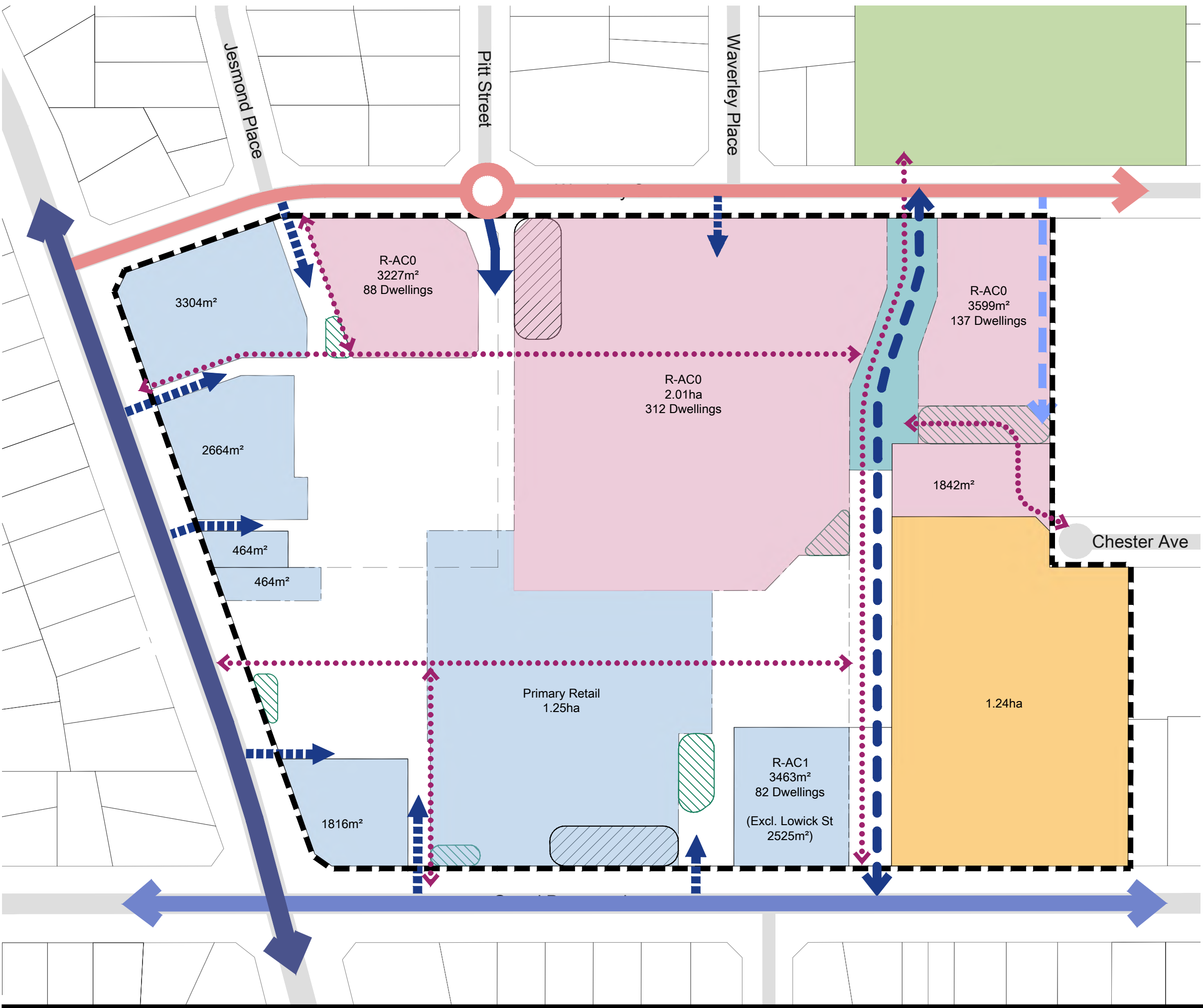
CLIENT
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PROJECT NO.
P0063129
DRAWING NO.
03.1

DATE
07.05.2026
REVISION
.



Legend

Precinct Structure Plan Area

Centre Zone

Mixed Use Zone

Private Community Purpose Zone

Circulation and Parking

Lowick Street Private Access Road

Activated Shared Zone

Indicative Landscape Node

Access Easement

Access - Full Movement

Access Left-In Left-Out

Service Areas

Key Pedestrian Links

Surrounding Reseves

Other Regional Road (MRS)

District Distributor Road

Local Distributor Road

Public Open Space

Land Use Summary

Total Site:

8.95ha

Land Use	Area
Centre	2.38ha
Mixed Use	2.96ha
Private Community Purpose	1.24ha
Circulation and Parking	2.15ha
Activated Shared Zone	0.22ha

Total Dwellings:

619

Commercial GFA:
(excl. PAD Sites)

30,245m²

Parking Bays

1,753 total

Commercial:

1,035 bays

Residential:

718 bays

APPENDIX B

Feature Survey (Jurovich Surveying, 2024)





APPENDIX C

Geotechnical Investigation (Galt Geotechnics, 2024)



Report on:

**GEOTECHNICAL STUDY
PROPOSED DIANELLA PLAZA SHOPPING
CENTRE REDEVELOPMENT – PHASE 1
ALEXANDER DRIVE
DIANELLA**

WAE200102-02 002 R Rev0

Submitted to:

Projective DM Pty Ltd

16 April 2024

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2. KEY FINDINGS	3
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4. PROPOSED DEVELOPMENT	4
5. PROJECT OBJECTIVES	4
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Figure 1: Site and Location Plan

- Appendix A: Supplied Information
- Appendix B: Site Photographs
- Appendix C: Cone Penetration Test Results
- Appendix D: Borehole Reports
- Appendix E: Infiltration Test Results

Standard Geotechnical Definitions, Recommendations, Requirements and Limitations

1. INTRODUCTION

This report presents the outcomes of Galt Geotechnics' (Galt's) geotechnical study for the proposed Stage 1 of the Dianella Plaza Shopping Centre redevelopment on Alexander Drive, Dianella ("the site").

This report is to be read in conjunction with the appended "Geotechnical Definitions, Recommendations, Requirements and Limitations", 'Clause GDR1', etc. found at the back of this report.

2. KEY FINDINGS

The site is underlain by Sand to the maximum investigated depth of 8 m. The sand is typically medium dense to dense with some near surface loose sand present in some test locations.

Groundwater was recorded at depths ranging from 6.5 m to 7.7 m.

An unsaturated hydraulic conductivity (k) of 5 m/day may be adopted for the design of soakwells.

3. SITE DESCRIPTION

Table 1: Summary of Site

Item	Comment
Site Extent	Refer Figure 1
Site Area	Around 7.7 ha
Current Site Surface Levels ¹	Typically RL 26 m AHD to RL 30 m AHD in middle of site
Vegetation	Mature trees within car park and near northern boundary. Typically paved across balance of the site.
Current Land Use	Commercial.
Existing Infrastructure	Dianella Plaza Shopping Centre and associated car parking
Site History ²	1953 to 1965: Bushland 1965 to 1995: Construction of Dianella Plaza and associated car parks 1995 to present: Relatively unchanged. Northern-most building demolished in 2015 and area remains vacant.

- NOTES:**
1. Site levels based on publicly available data (Landgate).
 2. Site history based on aerial imagery (Landgate).

4. PROPOSED DEVELOPMENT

Table 2: Summary of Proposed Development

Item	Comment
Proposed Development	Demolition of the existing Coles building, followed by construction of new Coles building further south (fronting Grand Promenade). The footprint of the existing Coles building will be occupied by several smaller commercial tenancies and car parking areas.
Basements Proposed	Assumed none
Proposed Finished Level	Assumed near current surface level
Cut/Fill	Minor to facilitate earthworks.
Assumed Foundation Type	Shallow footings and ground slabs
Assumed Retaining Walls	Minor if any
Assumed Stormwater Disposal	On-site via soakwells
Assumed Sewage Disposal	Off-site via sewer network

NOTES: 1. Proposed development details based on supplied information presented in Appendix A.

5. PROJECT OBJECTIVES

The objectives of the study were to:

- assess subsurface soil and groundwater conditions across the site;
- provide recommendations on suitable footing systems for the proposed development;
- provide allowable bearing pressure and settlement estimates for shallow foundations;
- provide a site classification(s) in accordance with AS 2870-2011 "Residential Slabs and Footings";
- provide recommendations and geotechnical design parameters for earth retaining structures;
- recommend appropriate site preparation procedures including compaction criteria;
- assess the permeability of the soils at the site for potential on-site disposal of stormwater by infiltration; and
- provide a subgrade California bearing ratio (CBR) value for pavement thickness design by others.

6. FIELDWORK

Fieldwork was carried out in the presence of a representative from Galt on 2 April 2024 and comprised:

Table 3: Summary of Field Data

Type	Results Appendix	Summary	GDR Clause	Equipment Used	No. Tests	Depth Range (m)
Site Plan	Figure 1	-	-	Hand held GPS ¹	-	-
Photographs	B	-	-	-	-	-
Cone Penetration Tests (CPTs)	C	Section 8	GDR3.2	22-tonne truck	8	8
Machine Auger Boreholes (BH)	D	Section 8	GDR3.3	EVH Scout on utility	5	1.5
Perth Sand Penetrometer (PSP)			GDR3.5	Hand operated PSP	5	1.05-2.1
Infiltration Tests (IT)	-	Section 6.1	GDR3.7	Inverse auger hole	3	0.91

NOTES: 1. Hand held GPS is accurate to ± 5 m.

6.1. Infiltration Test Results

Table 4: Infiltration Test Results

Test Location	Soil Description	Depth (m)	Minimum Unsaturated Hydraulic Conductivity, k_{unsat} (m/day)
IT01	SAND (SP)	0.91	8.5
IT02			8.7
IT03			7.4

NOTES: 1. Infiltration test method using inverse auger is explained in GDR3.7

7. SITE CONDITIONS

7.1. Geology

Table 5: Summary of Geology Mapping

Map Sheet	Map Scale	Mapped Soils	Site Findings
Perth	1:50,000	Bassendean Sand	FILL: SAND (SP-SM); over SAND (SP)

7.2. Groundwater

Table 6: Summary of Groundwater Levels

Item	Date	Depth (m)	Elevation (m AHD)	Comment
Perth Groundwater Atlas	1997	1-5	25	
Site observations	2024	5.2-6.2	~23 ²	Groundwater depths inferred from pore pressure measurements

NOTES: 1. Perth Groundwater Atlas 1997 shows the historical maximum groundwater elevations.
2. Groundwater elevation estimated from assumed surface elevation of RL 28 m AHD.

8. GROUND MODEL

The subsurface conditions are generalised in the inline image and table below. The generalised subsurface units are described in the table with geotechnical design parameters.

Inline Image 1 – Idealised cross section of subsurface conditions on site.

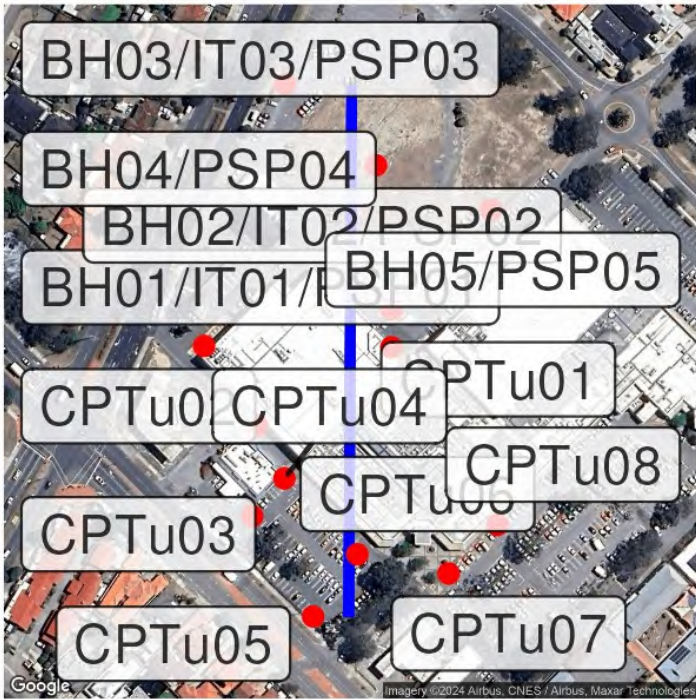
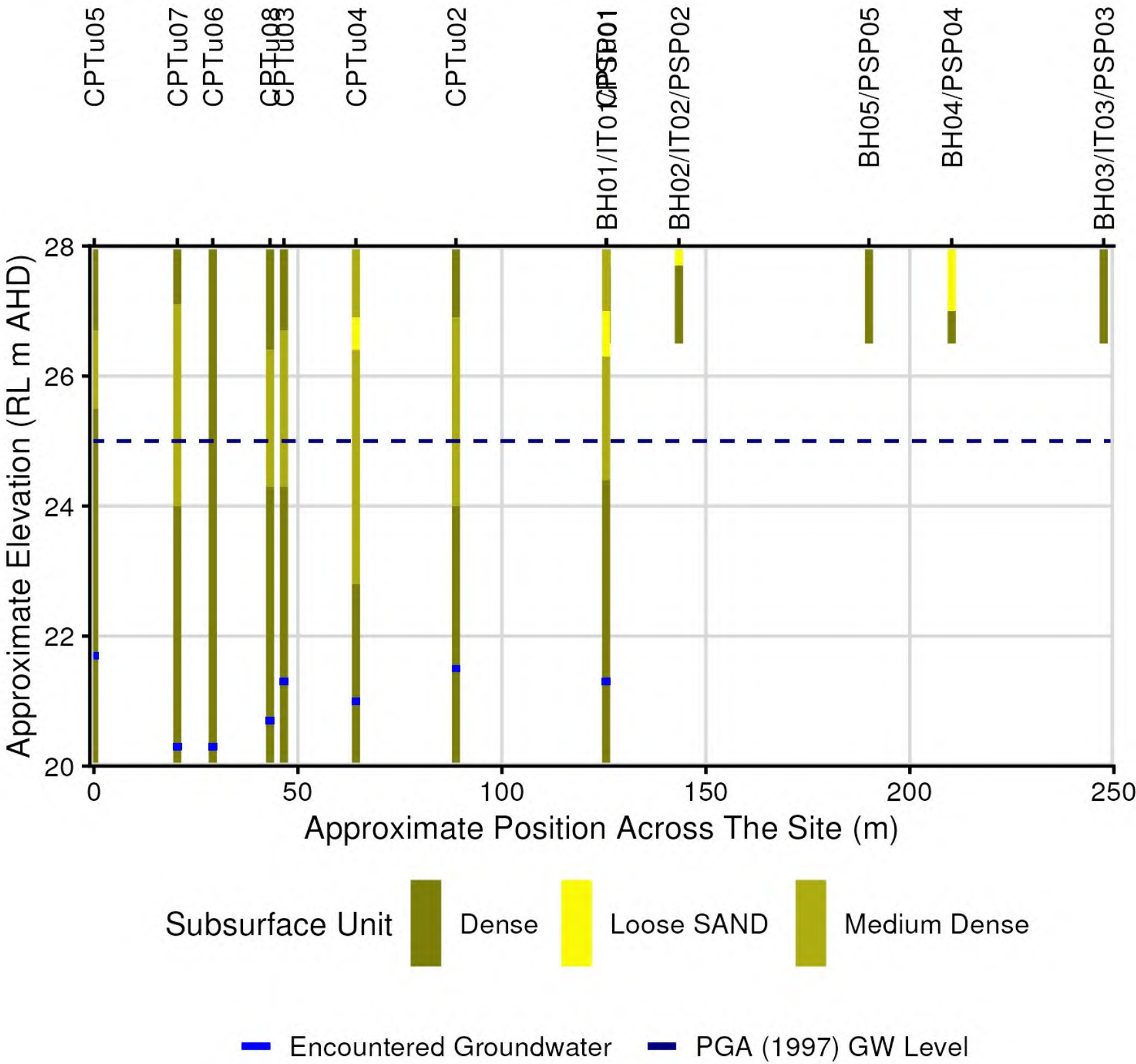


Table 7: Geotechnical Model Units and Design Parameters

Unit Name	Material Type	Where Found	Description	Comment	γ_{bulk} (kN/m ³)	ϕ' (°)	c' (kPa)	S_u (kPa)	E_v (MPa)	ν	k_0	Wall Friction=0		Wall Friction=0.5 ϕ	
												k_a	k_p	k_a	k_p
A	Loose SAND	Within the upper 2 m of soil profile, typically toward the north of the site.	Fine to medium grained, grey, brown, yellow.	Local fill similar to in situ material as noted on ground model.	17	32	-	-	5	0.3	0.42	0.31	3.25	0.27	5.55
B	Medium Dense SAND	Typically between RL 27 m AHD and RL 23 m AHD.	Near surface FILL typically comprises gravelly SAND, fine to medium grained, fine to medium sized gravel.		18	34	-	-	20	0.25	0.39	0.28	3.54	0.25	6.47
C	Dense SAND	At the surface and typically below RL 24 m AHD.			18	36	-	-	40	0.25	0.36	0.26	3.85	0.22	7.63

- NOTES:**
1. These units are a generalization of results from individual tests, which should be referred to for more information.
 2. Conditions at CPT locations below depth of soil sample recovery are inferred (refer to clause GDR3.2)
 3. Topsoil is not included as a discrete unit.
 4. For all earth pressure coefficients (retaining wall design) refer to clause GDR11.2 for more detail and interpretation. Unit weights for retaining structure design should be as per GDR11.2 or 1 kN/m³ greater than the values in the table above.
- γ_{bulk} – bulk unit weight
 ϕ' – effective friction angle
 S_u – undrained shear strength
 c' – effective cohesion
 E_v – vertical elastic modulus
 ν – Poisson's Ratio
 k_a – coefficient of active earth pressure (Coulomb – AS4678-2002, Appendix E)
 k_p – coefficient of passive earth pressure (Coulomb – AS4678-2002, Appendix E)
 k_0 – coefficient of at-rest earth pressure (Jaky)

9. GEOTECHNICAL ASSESSMENT

9.1. Summary

Table 8: Summary of Geotechnical Assessment

Type	Clause	Parameter	Comment
Site Suitability	-	-	We consider the site to be geotechnically suitable for the proposed development. Standard site preparation measures will apply.
Construction Methodology and Suitability	-	-	Shallow footings in accordance with AS2870-2011 will be suitable for this site. Mass retaining will be suitable for retaining above groundwater. Stormwater disposal via infiltration is suitable.
Site Classification (AS2870)	GDR5	A	$y_s < 5 \text{ mm}$
Site Preparation	GDR6	-	GDR6.2.1 Common Measures followed by GDR6.2.2 Sand Sites .
Approved Fill	GDR8	-	Approved Fill for this site is to comprise Permeable Sand . All <u>natural</u> and <u>existing fill</u> sand may be assumed to be Permeable Sand .
Compaction Control	GDR7	-	A PSP may be used for compaction control on site-derived Permeable Sand . Deemed to comply values for 'Bassendean Sand' in GDR7.4 are applicable.
Shallow Footings	GDR9	$q_{all} = 250 \text{ kPa}$	Design tables for shallow footings are presented in Section 9.2. 70% of the settlement is expected to occur during construction.
Earth Pressure Coefficients	GDR11	Section 8	Earth pressure coefficients can be used for the generalised subsurface unit presented. Any Permeable Sand fill may be assumed to be Unit B – Medium Dense SAND.
Unsaturated Hydraulic Conductivity	GDR13	$k_{unsat} = 5 \text{ m/day}$	k_{unsat} values apply where disposing into Approved Fill (Permeable Sand) or natural sand, minimum 0.5 m above the groundwater table GDR13.4.
Pavement Subgrade CBR	GDR16	CBR = 10%	Subgrade to comprise compacted in-situ sand or compacted Approved Fill

NOTES: 1. q_{all} – allowable bearing pressure (maximum for all footings, refer to footing tables for further details)

9.2. Shallow Footings

Table 9: Isolated Pad - Footing Allowable Bearing Pressures and Estimated Settlements

d_e (m)	b (m)	q_{all} (kPa)	s (mm)
0.5	0.5	160	<5
	1.0	180	5-10
	1.5	200	10-15
	2.0	200	15-20
	3.0	200	20-25
1.0	1.0	200	5-10
	2.0	200	10-15
	3.0	200	15-20
	4.0	200	20-25

- NOTES:**
1. d_e – minimum embedment depth (below finished ground level or floor slab)
 2. b – Footing breadth (footings assumed approximately square)
 3. q_{all} – allowable bearing pressure (peak).
 4. s – estimated settlement (excludes shrink/swell from site class)
 5. Refer to GDR9

Table 10: Isolated Strip Footing - Allowable Bearing Pressures and Estimated Settlements

d_e (m)	b (m)	q_{all} (kPa)	s (mm)
0.5	0.5	140	<5
	1.0	140	5-10
	1.5	150	10-15
	2.0	160	15-20
	3.0	160	20-25
1.0	1.0	160	5-10
	2.0	160	10-15
	3.0	160	15-20

- NOTES:**
1. d_e – minimum embedment depth (below finished ground level or floor slab)
 2. b – Footing width (footings assumed long relative to width)
 3. q_{all} – allowable bearing pressure (peak).
 4. s – estimated settlement (excludes shrink/swell from site class)
 5. Refer to GDR9

10. CLOSURE

GALT GEOTECHNICS



Timothy Dunton
Engineering Geologist



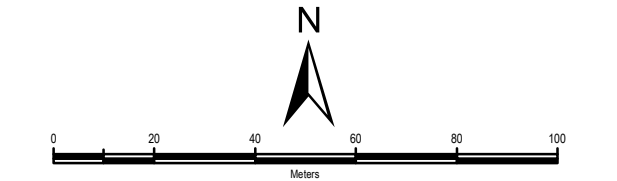
Rick Piovesan CPEng
Geotechnical Engineer

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Figures



- Legend**
- Site Boundary
 - Borehole / Infiltration Test / Perth Sand Penetrometer
 - Borehole / Perth Sand Penetrometer
 - Cone Penetration Test with Pore Pressure Measurement



NOTES
Aerial Imagery and Cadastre sourced from Landgate/SLIP

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	DRAWN	CED	
	DATE DRAWN	5/4/2024	
	CHECKED	RP	
	DATE CHECKED	16/4/2024	
	PROJECTION	GDA 1994 MGA Zone 50	

Galt Geotechnics Pty Ltd
ACN : 138 490 865
Tel : +61 (0)8 6272-0200
Address : 50 Edward Street
Osborne Park WA 6017

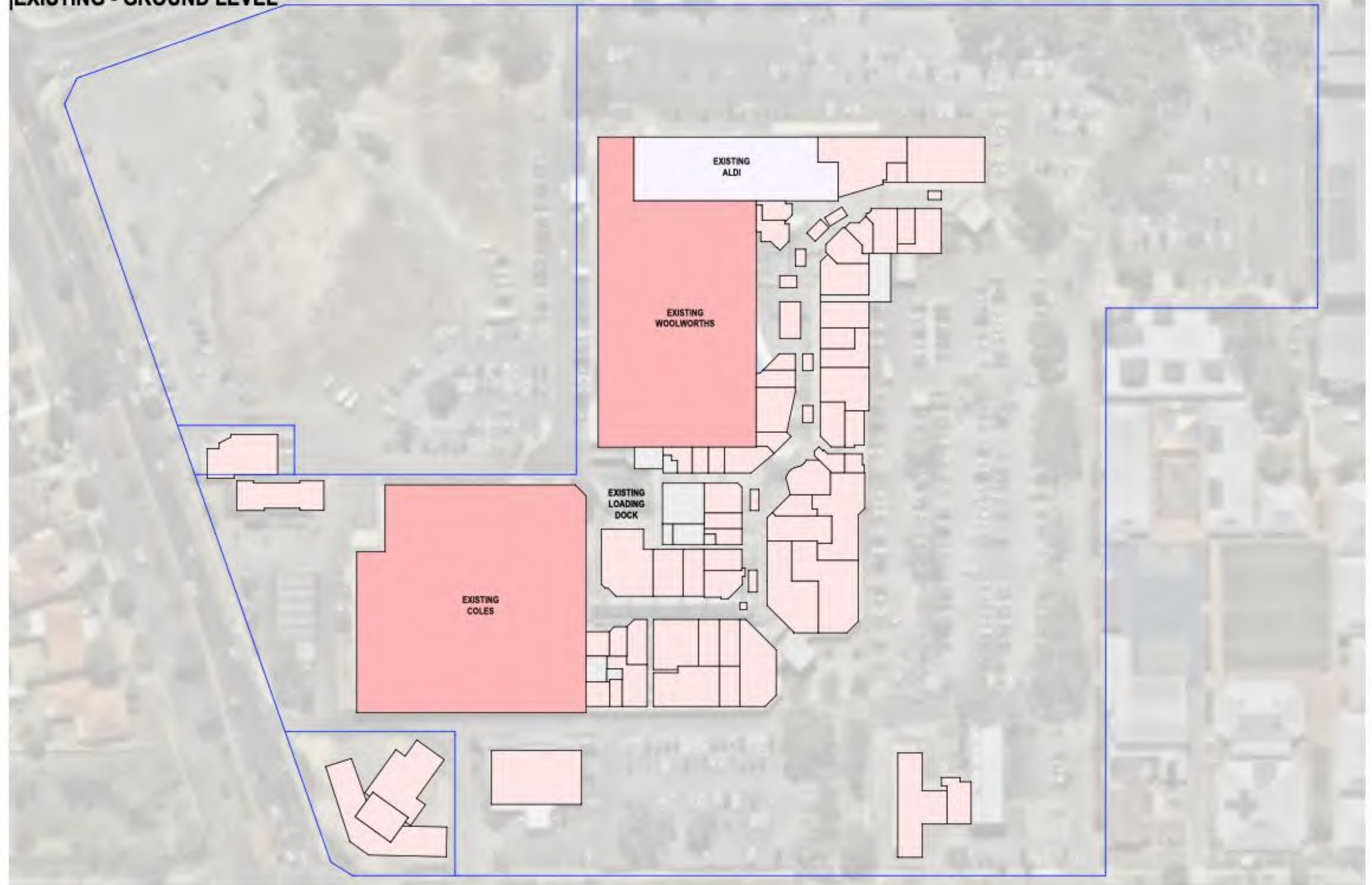
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CLIENT	PROJECTIVE DM PTY LTD		
PROJECT	PROPOSED PHASE 1 REDEVELOPMENT		
LOCATION	DIANELLA PLAZA SHOPPING CENTRE ALEXANDER DRIVE, DIANELLA		
TITLE	SITE & LOCATION PLAN		
Job No	WAE200102-02	Fig No	FIGURE 1
		Rev	A

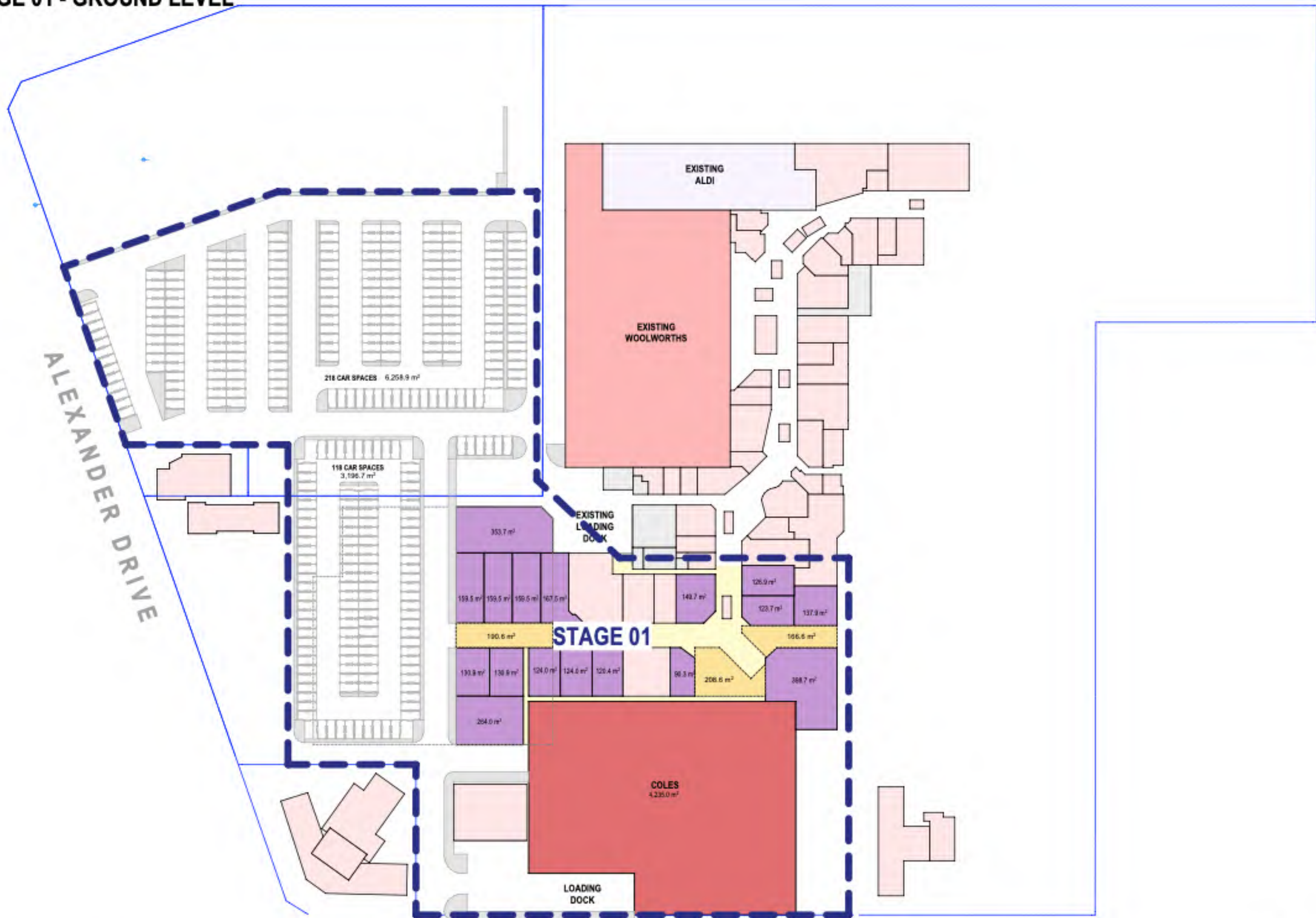
Appendices

Appendix A: Supplied Information

EXISTING - GROUND LEVEL



|STAGE 01 - GROUND LEVEL



Appendix B: Site Photographs

Photograph 1: Facing northeast at BH01 location.



Photograph 2: Facing southeast at BH01 location.



Photograph 3: Facing southwest at BH01 location. IT01 in progress.



Photograph 4: Facing southeast at BH02 location.



Photograph 5: Facing northeast at BH03 location.



Photograph 6: Facing southeast at BH03 location.



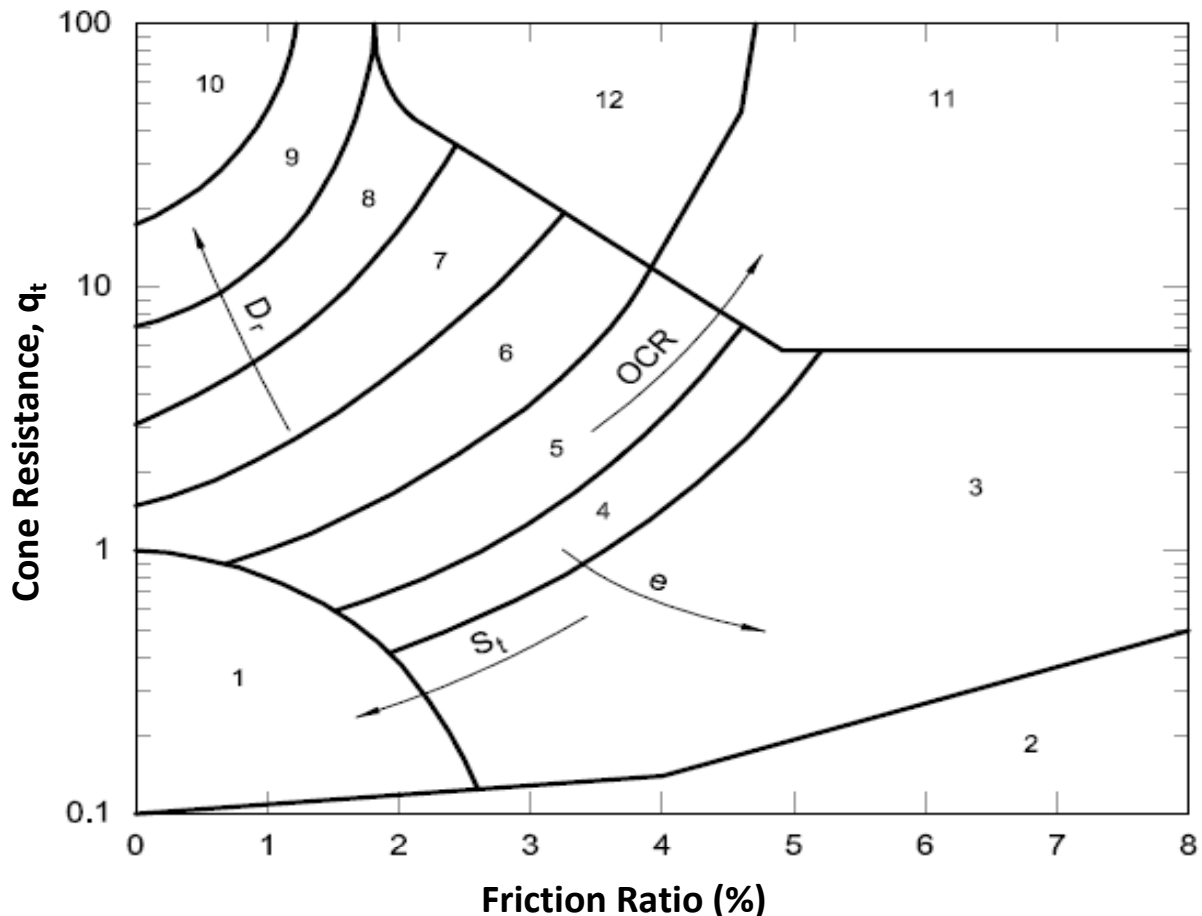
Photograph 7: Facing southwest at BH05 location.



Photograph 8: Facing south at CPT01 location.



Appendix C: Cone Penetration Test Results



DEFINITIONS

- q_t : Cone tip resistance corrected for pore water pressure
 S_t : Sensitivity
 e : Void ratio
 D_r : Relative density
 OCR : Overconsolidation ratio
 OC : Overconsolidated

SOIL BEHAVIOUR TYPE ZONES

- | | |
|------------------------------|--|
| 1. Sensitive fine grained | 7. Silty sand to sandy silt |
| 2. Organic material | 8. Sand to silty sand |
| 3. Clay | 9. Sand |
| 4. Silty clay to clay | 10. Gravelly sand to sand |
| 5. Clayey silt to silty clay | 11. Very stiff fine grained material (OC/cemented) |
| 6. Sandy silt to clayey silt | 12. Sand to clayey sand (OC/cemented) |

NOTES

- A. Some overlap in type zones is expected
 B. Local correlations are preferred and may indicate soil type boundaries that are different from those shown above

Reference: Robertson, P.K., Campanella, R.G., Gillespie, D. and Grieg, J. (1986) "Use of Piezometer Cone Data". Proceedings of the ASCE Speciality Conference In Situ '86: Use of In Situ Tests in Geotechnical Engineering, Blacksburg, pp 1263-80, American Society of Civil Engineers (ASCE)



CONE PENETRATION TESTING (CPT) SOIL TYPE INTERPRETATION

CONE PENETRATION TEST

ALL TESTS

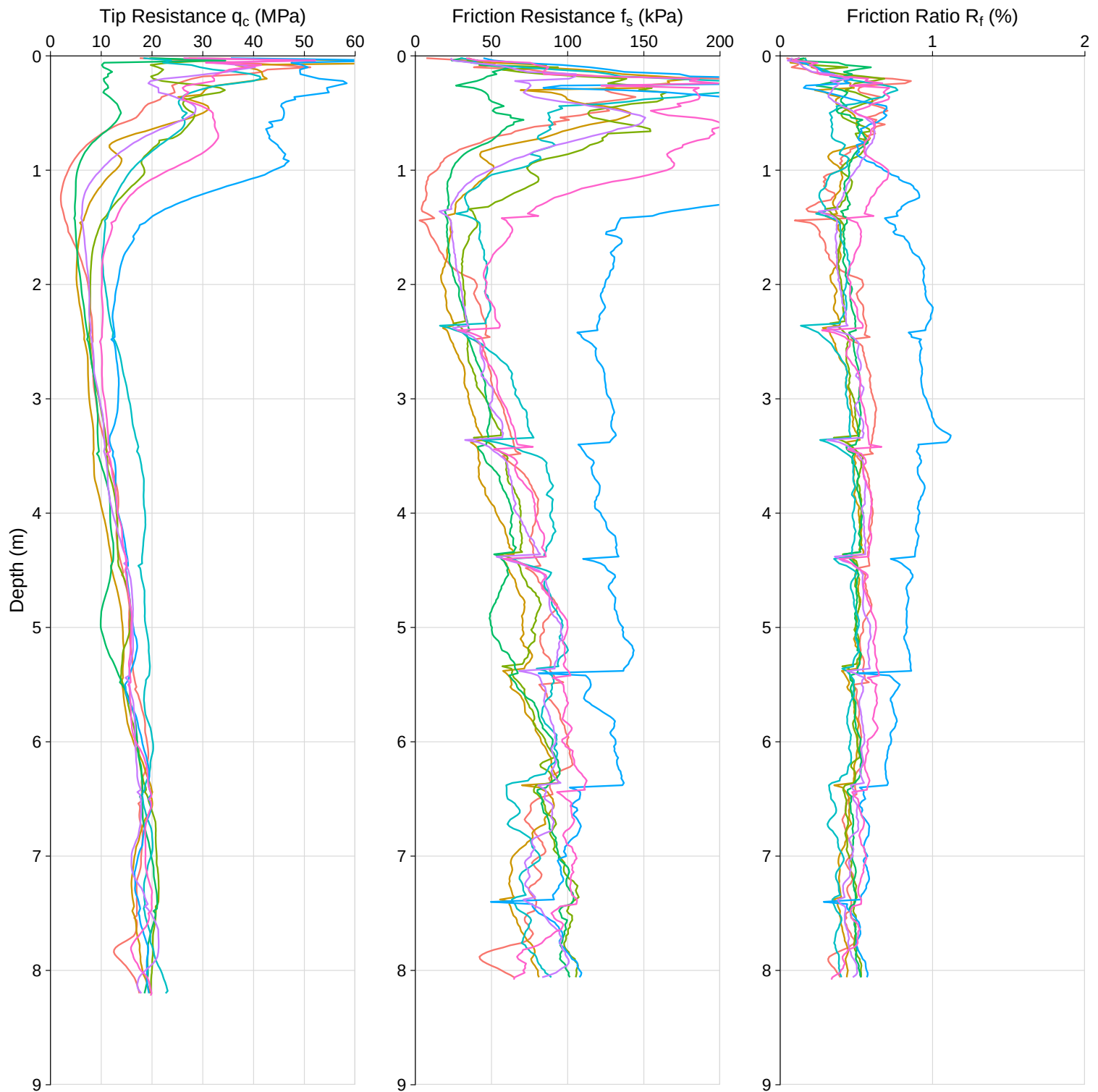
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DATE: 02/04/2024 - 03/04/2024

CLIENT: Projective DM PTY LTD

PROJECT: Proposed Phase One Redevelopment

LOCATION: Dianella Plaza Shopping Centre

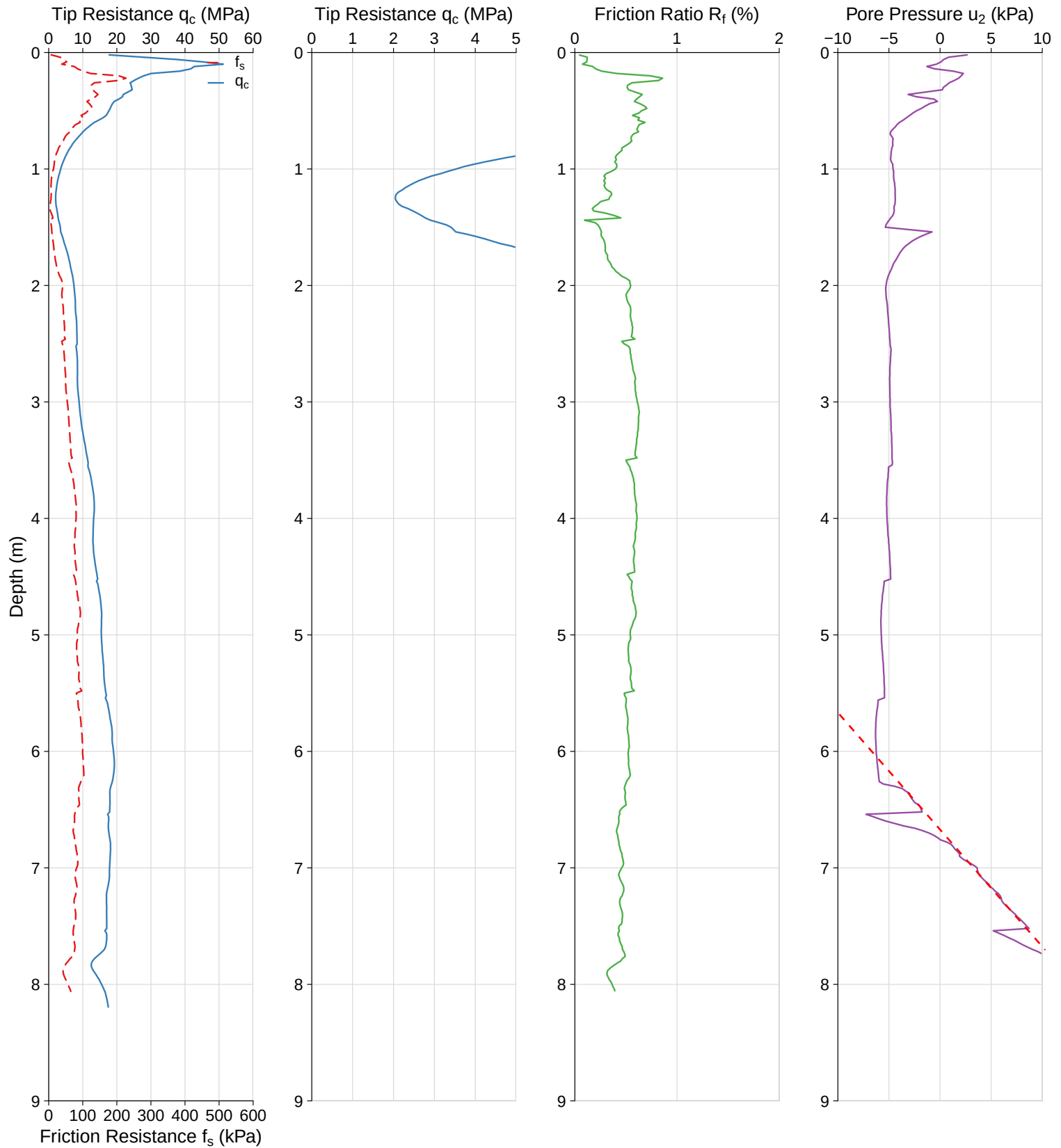


RIG: AP van den Berg Hyson 200kN 14T Truck

CONE PENETRATION TEST

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JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



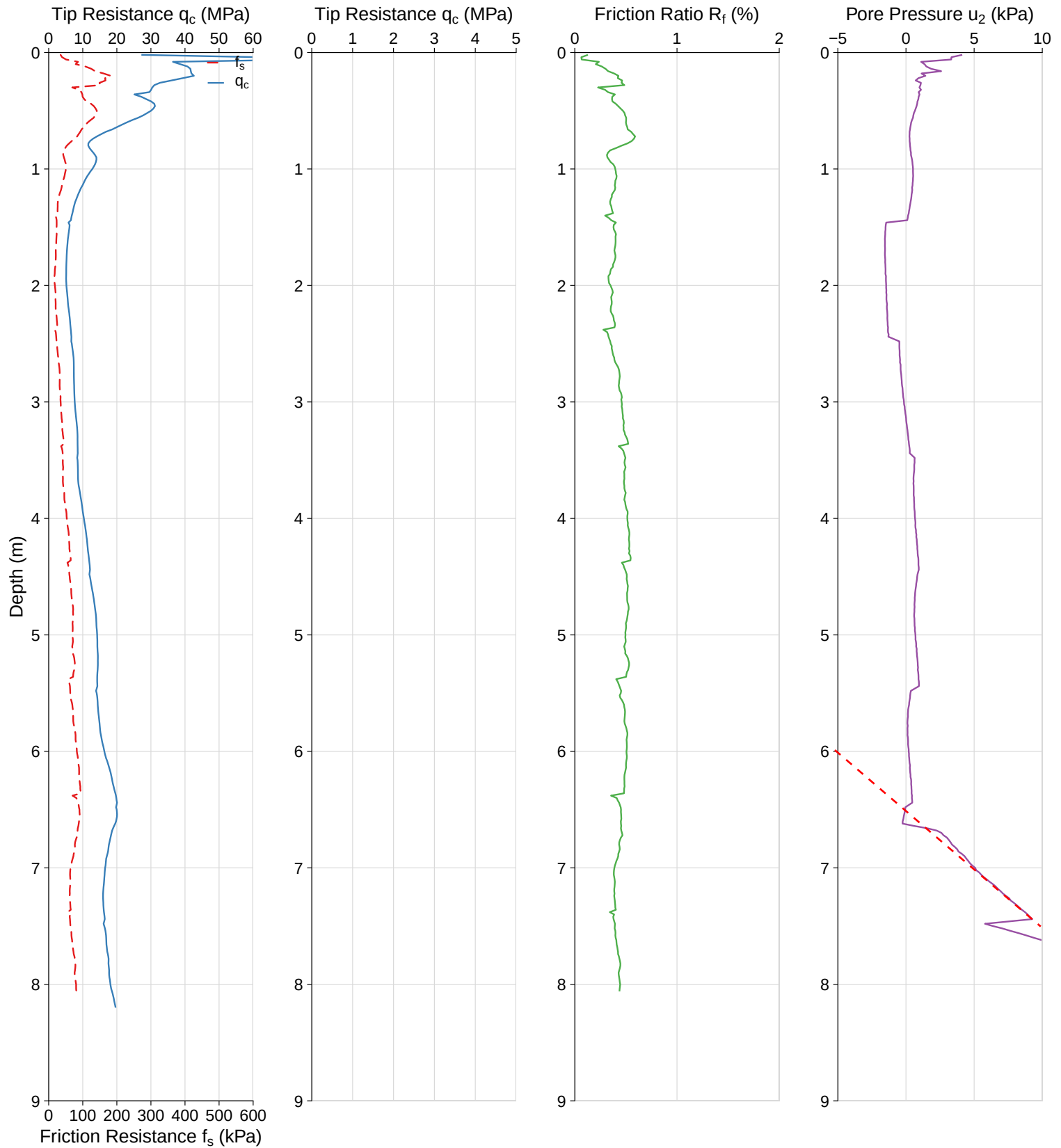
WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU02
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



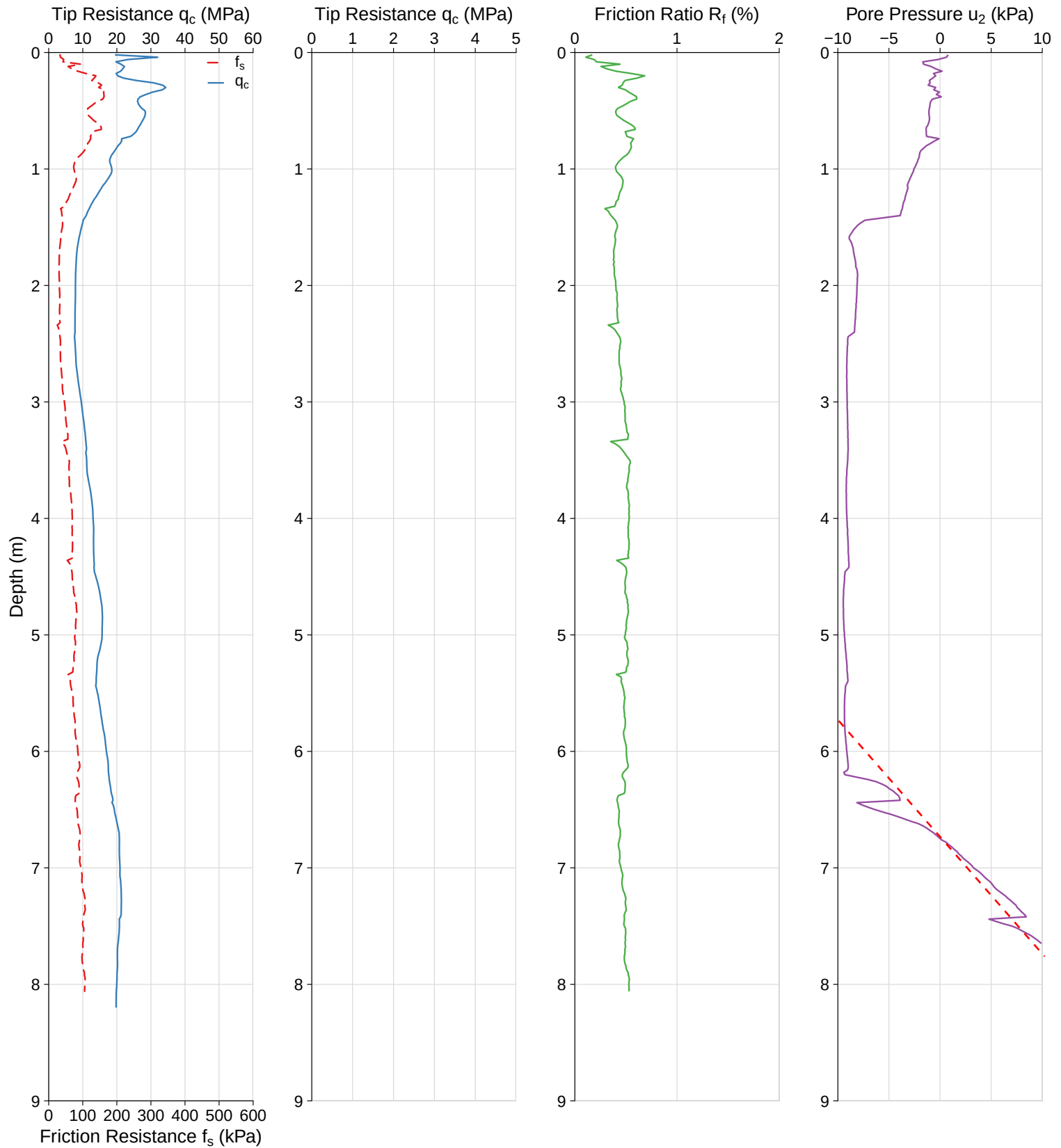
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TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU03
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



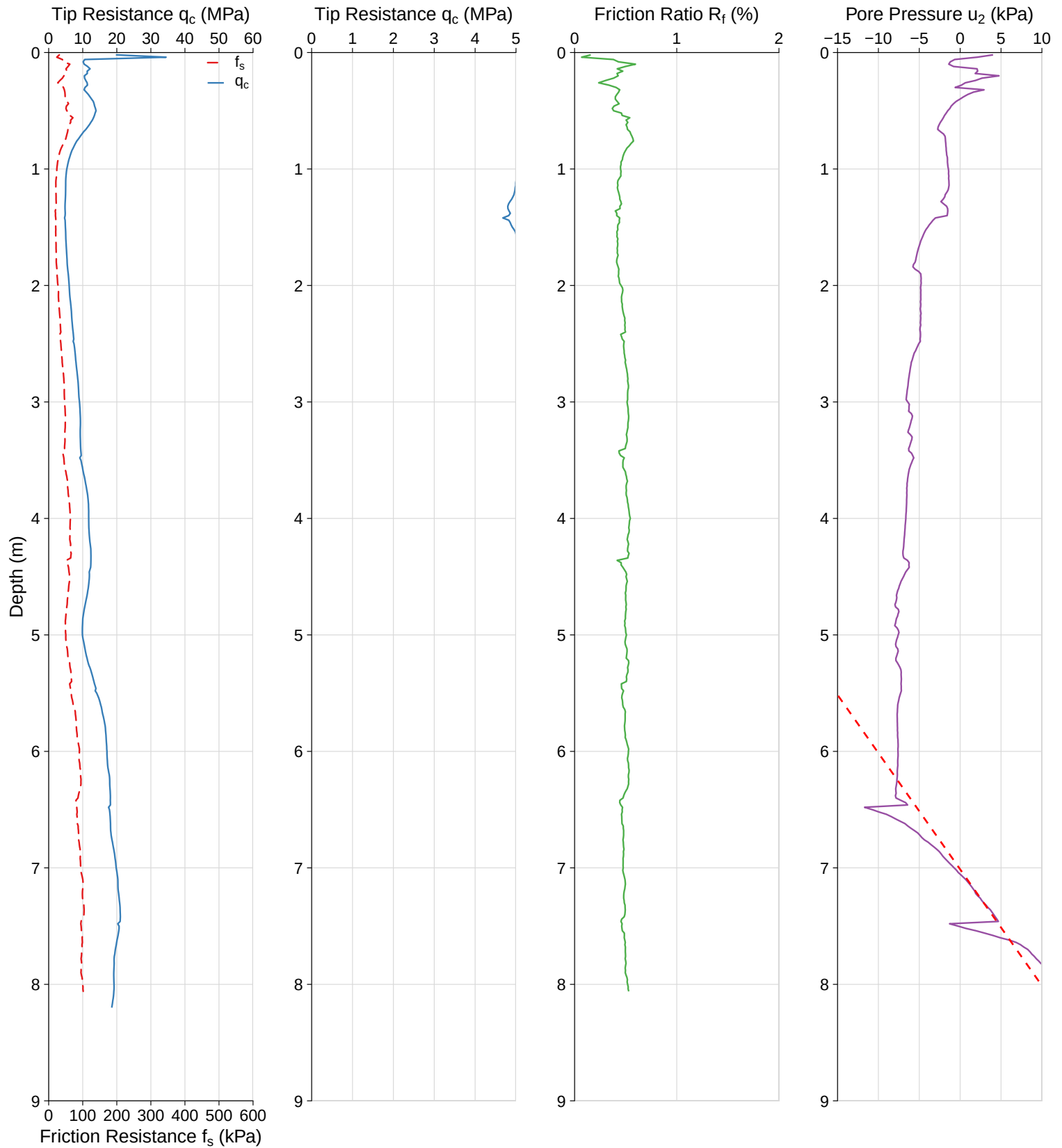
WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU04
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



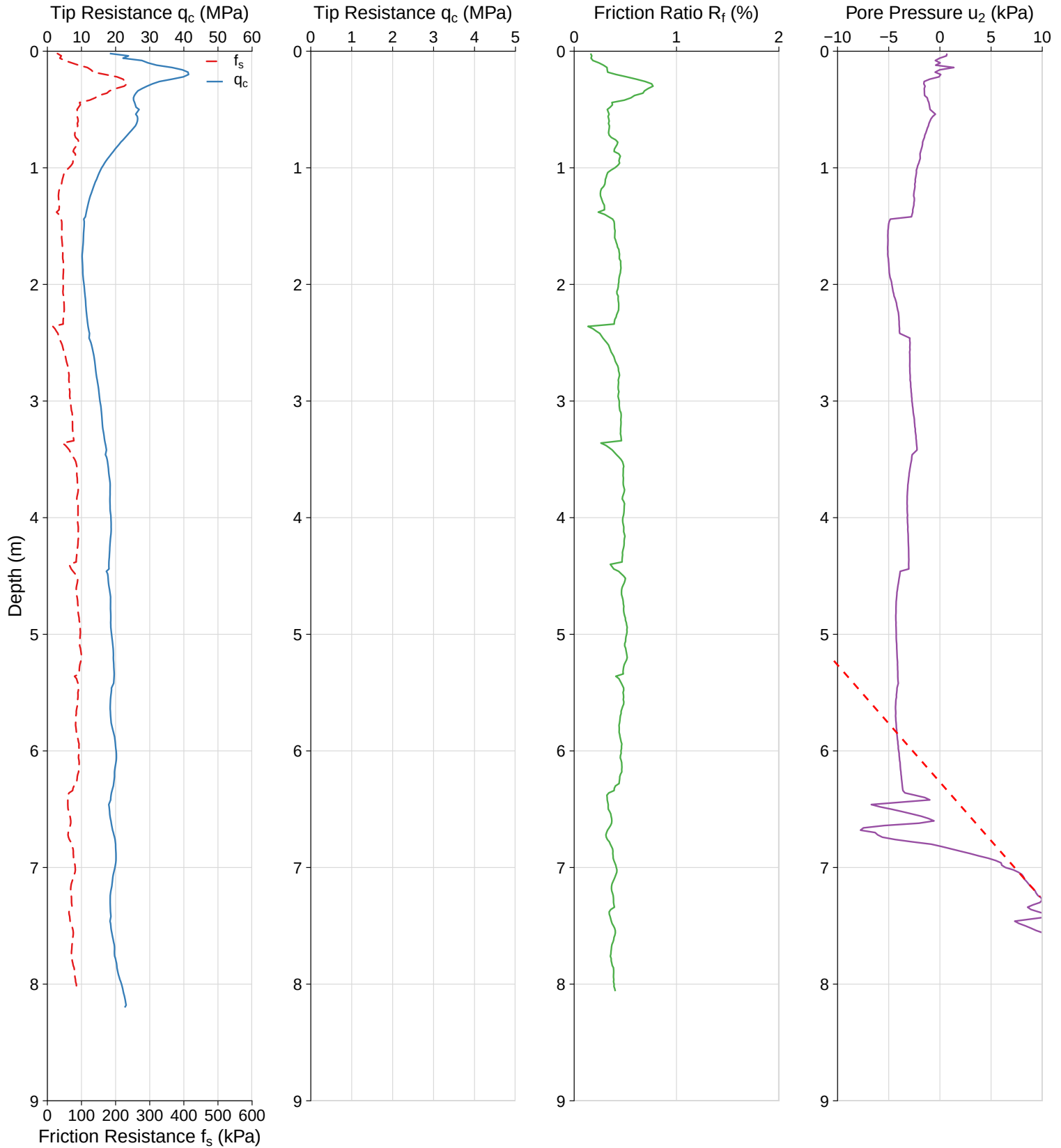
WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU05
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



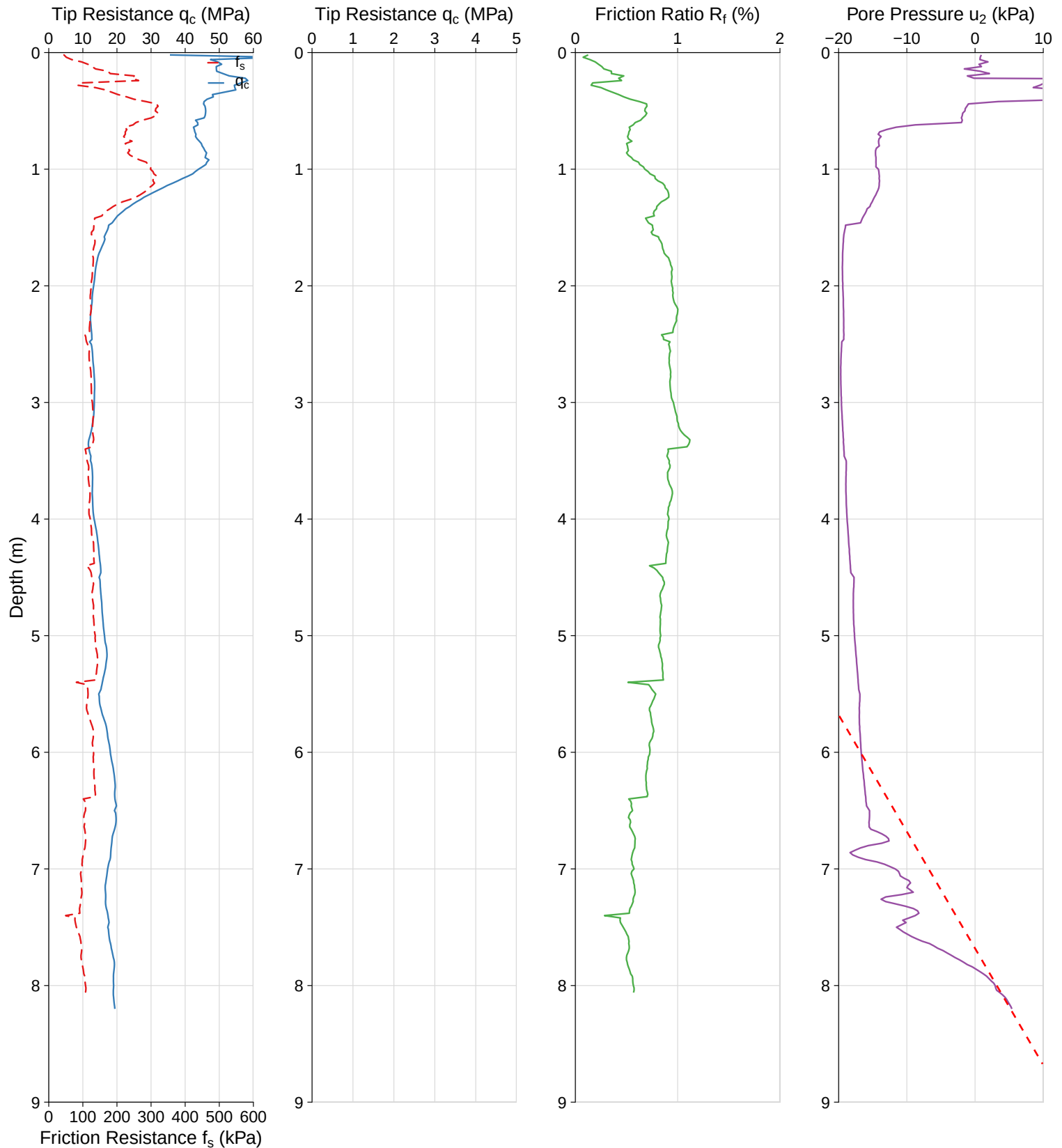
WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU06B
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



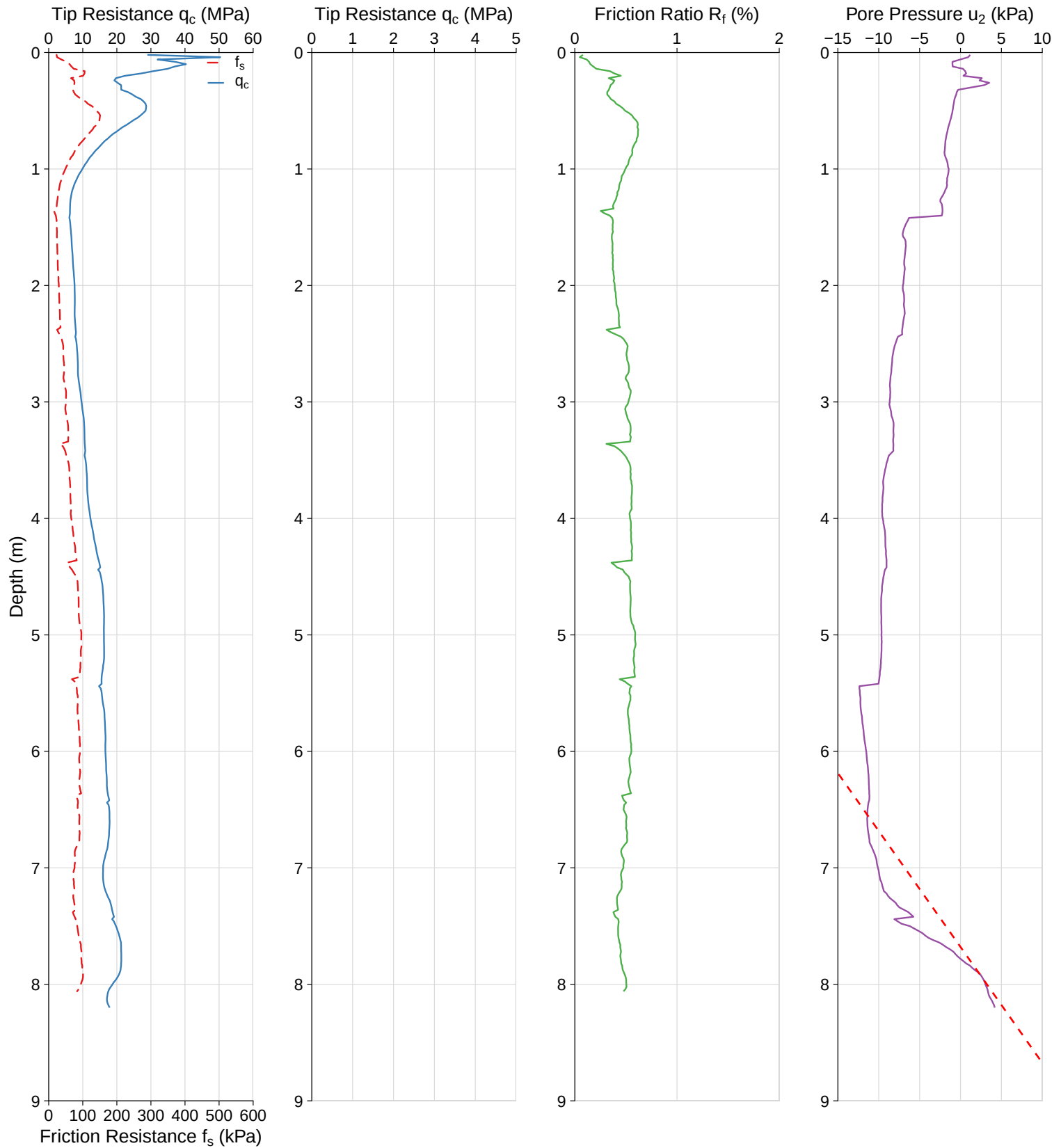
WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU07
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



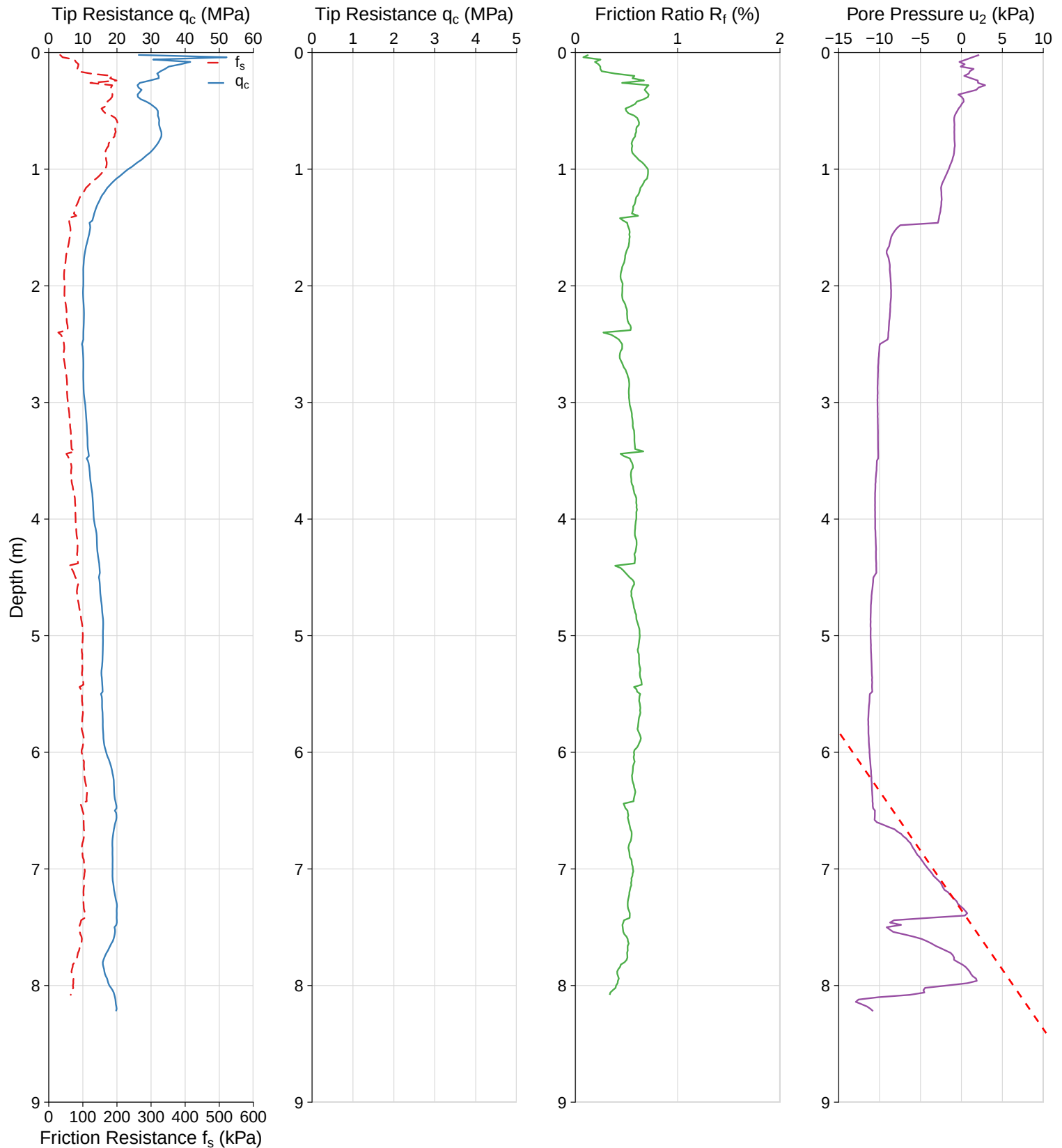
WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous

CONE PENETRATION TEST

CPT ID: WAE200102-02_CPTU08
JOB NUMBER: WAE200102-02
DATE: 02/04/2024

CLIENT: Projective DM PTY LTD
PROJECT: Proposed Phase One Redevelopment
LOCATION: Dianella Plaza Shopping Centre



WATER:
TERMINATION:
DUMMY PROBE:
RIG: AP van den Berg Hyson 200kN 14T Truck

CO-ORDS:
ELEVATION:
PRE-DRILL:
WASHER/DISC: Porous



Appendix D: Borehole Reports

EXPLANATORY NOTES TO BE READ WITH BOREHOLE AND TEST PIT REPORTS



METHOD OF DRILLING OR EXCAVATION

AC	Air Core	E	Excavator	PQ3	PQ3 Core Barrel
AD/T	Auger Drilling with TC-Bit	EH	Excavator with Hammer	PT	Push Tube
AD/V	Auger Drilling with V-Bit	HA	Hand Auger	R	Ripper
AT	Air Track	HMLC	HMLC Core Barrel	RR	Rock Roller
B	Bulldozer Blade	HQ3	HQ3 Core Barrel	SON	Sonic Rig
BH	Backhoe Bucket	N	Natural Exposure	SPT	Driven SPT
CT	Cable Tool	NMLC	NMLC Core Barrel	WB	Washbore
DT	Diatube	PP	Push Probe	X	Existing Excavation

SUPPORT

T	Timbering
---	-----------

PENETRATION EFFORT (RELATIVE TO THE EQUIPMENT USED)

VE	Very Easy	E	Easy	F	Firm
H	Hard	VH	Very Hard		

WATER

►	Water Inflow	▼	Water Level
◄	Water Loss (complete)		
◄	Water Loss (partial)		

SAMPLING AND TESTING

B	Bulk Disturbed Sample	P	Piston Sample
BLK	Block Sample	PBT	Plate Bearing Test
C	Core Sample	U	Undisturbed Push-in Sample
CBR	CBR Mould Sample		U50: 50 mm diameter
D	Small Disturbed Sample	SPT	Standard Penetration Test
ES	Environmental Soil Sample		Example: 3, 4, 5 N=9
EW	Environmental Water Sample		3,4,5: Blows per 150 mm
G	Gas Sample		N=9: Blows per 300 mm after
HP	Hand Penetrometer		150 mm seating interval
LB	Large Bulk Disturbed Sample	VS	Vane Shear; P = Peak
M	Mazier Type Sample		R = Remoulded (kPa)
MC	Moisture Content Sample	W	Water Sample

ROCK CORE RECOVERY

$$\text{TCR} = \text{Total Core Recovery (\%)} = \frac{\text{CRL}}{\text{TCL}} \times 100$$

$$\text{RQD} = \text{Rock Quality Designation (\%)} = \frac{\text{ALC} > 100}{\text{TCL}} \times 100$$

TCL Length of Core Run

CRL Length of Core Recovered

ALC>100 Total Length of Axial Lengths of Core Greater than 100 mm Long

METHOD OF SOIL DESCRIPTION BOREHOLE AND TEST PIT REPORTS



GRAPHIC LOG & SOIL CLASSIFICATION SYMBOLS

Graphic	USCS	Soil Name
		FILL (various types)
		COBBLES / BOULDERS
	GP	GRAVEL (poorly graded)
	GW	GRAVEL (well graded)
	GC	Clayey GRAVEL
	GM	Silty GRAVEL
	SP	SAND (poorly graded)
	SW	SAND (well graded)
	SC	Clayey SAND

Graphic	USCS	Soil Name
	SM	Silty SAND
	ML	SILT (low liquid limit)
	MH	SILT (high liquid limit)
	CL	CLAY (low plasticity)
	CI	CLAY (medium plasticity)
	CH	CLAY (high plasticity)
	OL	Organic SILT (low liquid limit)
	OH	Organic SILT (high liquid limit)
	Pt	PEAT

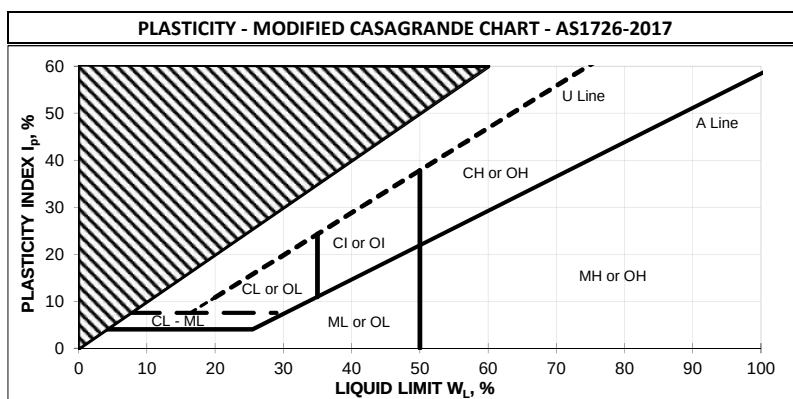
NOTE: Dual classification given for soils with a fines content between 5% and 12%.

SOIL CLASSIFICATION AND INFERRED STRATIGRAPHY

Soil descriptions are based on AS1726-2017. Material properties are assessed in the field by visual/tactile methods in combination with field and laboratory testing techniques (where used).

NOTE: AS 1726-2017 defines a fine grained soil where the total dry mass of fine fractions (<0.075 mm particle size) exceeds 35%.

PARTICLE SIZE		
Soil Name	Particle Size (mm)	
BOULDERS	>200	
COBBLES	63 to 200	
GRAVEL	Coarse	19 to 63
	Medium	6.7 to 19
	Fine	2.3 to 6.7
SAND	Coarse	0.6 to 2.36
	Medium	0.21 to 0.6
	Fine	0.075 to 0.21
FINES	SILT	0.002 to 0.075
	CLAY	<0.002



RESISTANCE TO EXCAVATION		
Symbol	Term	Description
VE	Very easy	All resistances are relative to the selected method of excavation
E	Easy	
F	Firm	
H	Hard	
VH	Very hard	

MOISTURE CONDITION	
Symbol	Term
D	Dry
M	Moist
W	Wet

CEMENTATION	
Cementation	Description
Weakly cemented	Soil may be easily disaggregated by hand in air or water
Moderately cemented	Effort is required to disaggregate the soil by hand in air or water

CONSISTENCY		
Symbol	Term	Undrained Shear Strength (kPa)
VS	Very Soft	0 to 12
S	Soft	12 to 25
F	Firm	25 to 50
St	Stiff	50 to 100
VSt	Very Stiff	100 to 200
H	Hard	>200

ORGANIC SOILS	
Material	Organic Content % of dry mass
Inorganic soil	<2%
Organic soil	2% to 25%
Peat	>25%

DENSITY		
Symbol	Term	Density Index (%)
VL	Very Loose	<15
L	Loose	15 to 35
MD	Medium Dense	35 to 65
D	Dense	65 to 85
VD	Very Dense	>85



REPORT OF BOREHOLE: BH01

Job No : WAE200102-02
Client : Projective DM Pty Ltd
Project : Proposed Phase 1 Redevelopment
Location : Dianella Plaza, Grand Promenade, Dianella WA
Contractor : Galt Geotechnics

Easting : 0.00
Northing : 0.00
UTM : 50J
Drill Rig : EVH Scout 1750
Inclination : -90 deg

Sheet : 1 OF 1
Logged : Alex Mathew
Logged Date : 02/04/2024
Checked : TD
Checked Date : 09/04/2024

Drilling Method	Excavation Resistance	PSP	DCP graph	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Moisture	Consistency/Density	Remarks	Sample
AD/V		SET			0.04	Nat Soil		ASP	Asphalt	D			
	4						SP-SM	Fill Gravelly SAND: brown, medium dense to dense, fine to medium grained, fine to coarse sized gravel, with fines.		MD-D			
	5			0.3	Fill		SP	Fill SAND: brown grey, dense to very dense, fine to medium grained, trace fines, trace gravel.		D-VD			
	6												
	8												
	13												
	16												
					1	Natural		SP	Natural SAND: yellow, fine to medium grained, trace fines .				
								BH01 Terminated at 1.5m (Target Depth. Groundwater not encountered)					
													



Easting : 0.00
Northing : 0.00
UTM : 50J
Drill Rig : EVH Scout 1750
Inclination : -90 deg

Sheet : 1 OF 1
 Logged : Alex Mathew
 Logged Date : 02/04/2024
 Checked : TD
 Checked Date : 09/04/2024



REPORT OF BOREHOLE: BH03

Job No	: WAE200102-02	Easting	: 0.00	Sheet	: 1 OF 1
Client	: Projective DM Pty Ltd	Northing	: 0.00	Logged	: Alex Mathew
Project	: Proposed Phase 1 Redevelopment	UTM	: 50J	Logged Date	: 02/04/2024
Location	: Dianella Plaza, Grand Promenade, Dianella WA	Drill Rig	: EVH Scout 1750	Checked	: TD
Contractor	: Galt Geotechnics	Inclination	: -90 deg	Checked Date	: 09/04/2024

Drilling Method	Excavation Resistance	PSP	DCP graph	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Moisture	Consistency/Density	Remarks	Sample
AD/V		SET			0.02	Not Soil		ASP	Asphalt	D	D-VD		
		17						SP -SM	Fill Gravelly SAND: pale yellow brown, dense to very dense, fine to medium grained, fine to coarse sized gravel, with fines.				
		17			0.3	Fill		SP	Fill SAND: brown, dense to very dense, fine to medium grained, with fine to medium sized gravel, trace fines.				
		20											
		19 R											
					0.8	Natural		SP	Natural SAND: yellow, fine to medium grained, trace fines.				
					1								
									BH03 Terminated at 1.5m (Target Depth. Groundwater not encountered)				
													



REPORT OF BOREHOLE: BH04

Job No : WAE200102-02

Client : Projective DM Pty Ltd

Project : Proposed Phase 1 Redevelopment

Location : Dianella Plaza, Grand Promenade, Dianella WA

Contractor : Galt Geotechnics

Easting : 0.00

Northing : 0.00

UTM : 50J

Drill Rig : EVH Scout 1750

Inclination : -90 deg

Sheet : 1 OF 1

Logged : Alex Mathew

Logged Date : 02/04/2024

Checked : TD

Checked Date : 09/04/2024

Drilling Method	Excavation Resistance	PSP	DCP graph	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Moisture	Consistency/Density	Remarks	Sample
ADV		SET				Fill		SP-SM	Fill SAND: grey, loose, fine to medium grained, with fines, trace rootlets within top 0.2 m.	D	L		
	1												
	3												
	2												
	2												
	2												
	2												
	1	1	Natural		SP	Natural SAND: yellow brown, fine to medium grained, trace fines .		D-VD					
	8												
	9												
	10												
	9						BH04 Terminated at 1.5m (Target Depth. Groundwater not encountered)						
	11												
	11												



REPORT OF BOREHOLE: BH05

Job No : WAE200102-02
Client : Projective DM Pty Ltd
Project : Proposed Phase 1 Redevelopment
Location : Dianella Plaza, Grand Promenade, Dianella WA
Contractor : Galt Geotechnics

Easting : 0.00
Northing : 0.00
UTM : 50J
Drill Rig : EVH Scout 1750
Inclination : -90 deg

Sheet : 1 OF 1
Logged : Alex Mathew
Logged Date : 02/04/2024
Checked : TD
Checked Date : 09/04/2024

Drilling Method	Excavation Resistance	PSP	DCP graph	Water	Depth (m)	Soil Origin	Graphic Log	Classification Code	Material Description	Moisture	Consistency/Density	Remarks	Sample
AD/V		SET				Fill		SP-SM	Fill Gravelly SAND: pale yellow, dense to very dense, fine to medium grained, fine to medium sized gravel, with fines.	D	D-VD		
		13			0.2	Fill		SP-SM	Fill SAND: brown, dense to very dense, fine to medium grained, with gravel, with fines.				
		5 HB			0.3	Fill		SP	As above, pale brown, trace gravel, trace fines.				
					1	Natural		SP	Natural SAND: yellow, fine to medium grained, trace fines .				
									BH05 Terminated at 1.5m (Target Depth. Groundwater not encountered)				
													

Appendix E: Infiltration Test Results

Hydraulic Conductivity Calculation - Inverse Auger Hole Method

Galt Geotechnics

Spreadsheet author:

ORW

17-Oct-09

REFERENCE: Cocks, G. *Disposal of Stormwater Runoff by Soakage in Perth, Western Australia*, Journal and News of the Australian Geomechanics Society, Volume 42 No 3 September 2007, pp101-114

Job No: WAE200102-02

Client: Projective DM Pty Ltd

Project: Proposed Phase 1

Redevelopment

Location: Dianella Plaza

Shopping Centre

BH Name: BH01/IT01

Test Depth: 0.91 m

Spreadsheet Legend

Required input

Calculated field

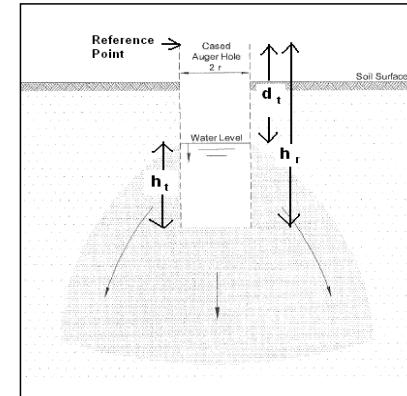
Comment field

Field not used

Fixed field

$$K = 1.15r \frac{\log_{10}(h_0 + \frac{1}{2}r) - \log_{10}(h_t + \frac{1}{2}r)}{t - t_0}$$

Parameter	Description	Value	Units
K	Hydraulic Conductivity		m/s
r	radius of test hole	0.045	m
t	time since start of measurement		s
h_r	reference point height above base	0.91	m
d_t	depth from reference point to water at time t		m
h_t	Water column height at time t		m
h_0	h_t at t=0		m



Test 1

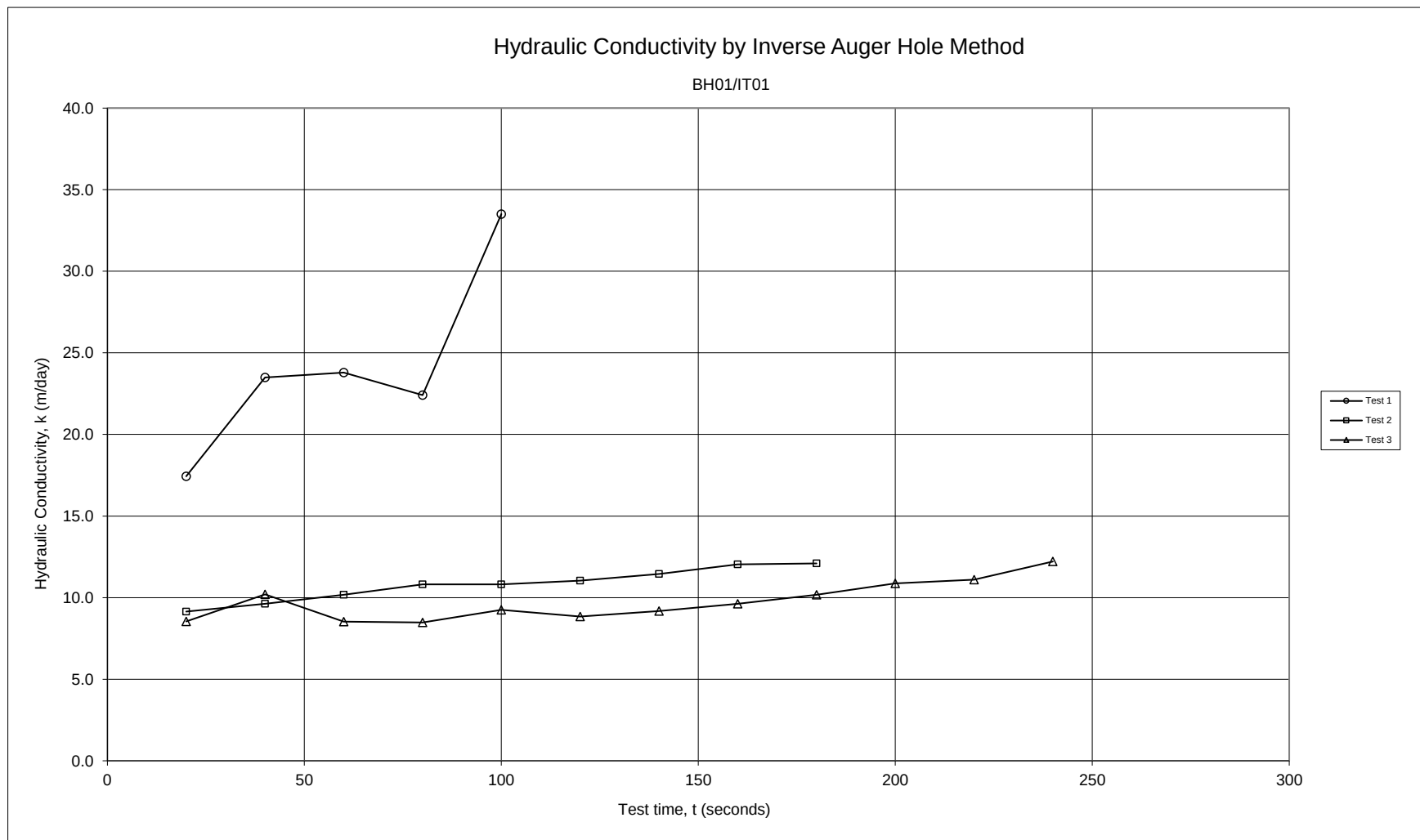
t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.75	0.16		
20	0.78	0.13	2.0E-04	17.4
40	0.82	0.09	2.7E-04	23.5
60	0.845	0.065	2.8E-04	23.8
80	0.86	0.05	2.6E-04	22.4
100	0.9	0.01	3.9E-04	33.5
AVERAGE			2.8E-04	24.1

Test 2

t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.71	0.2		
20	0.73	0.18	1.1E-04	9.1
40	0.75	0.16	1.1E-04	9.6
60	0.77	0.14	1.2E-04	10.2
80	0.79	0.12	1.3E-04	10.8
100	0.805	0.105	1.3E-04	10.8
120	0.82	0.09	1.3E-04	11.0
140	0.835	0.075	1.3E-04	11.4
160	0.85	0.06	1.4E-04	12.0
180	0.86	0.05	1.4E-04	12.1
AVERAGE			1.2E-04	10.8

Test 3

t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.695	0.215		
20	0.715	0.195	9.9E-05	8.5
40	0.74	0.17	1.2E-04	10.2
60	0.75	0.16	9.9E-05	8.5
80	0.765	0.145	9.8E-05	8.5
100	0.785	0.125	1.1E-04	9.2
120	0.795	0.115	1.0E-04	8.8
140	0.81	0.1	1.1E-04	9.2
160	0.825	0.085	1.1E-04	9.6
180	0.84	0.07	1.2E-04	10.2
200	0.855	0.055	1.3E-04	10.9
220	0.865	0.045	1.3E-04	11.1
240	0.88	0.03	1.4E-04	12.2
AVERAGE			1.1E-04	9.7



Hydraulic Conductivity Calculation - Inverse Auger Hole Method

Galt Geotechnics

Spreadsheet author:

ORW

17-Oct-09

REFERENCE: Cocks, G. *Disposal of Stormwater Runoff by Soakage in Perth, Western Australia*, Journal and News of the Australian Geomechanics Society, Volume 42 No 3 September 2007, pp101-114

Job No: WAE200102-02

Client: Projective DM Pty Ltd

Project: Proposed Phase 1

Redevelopment

Location: Dianella Plaza

Shopping Centre

BH Name: BH02/IT02

Test Depth: 0.91 m

Spreadsheet Legend

Required input

Calculated field

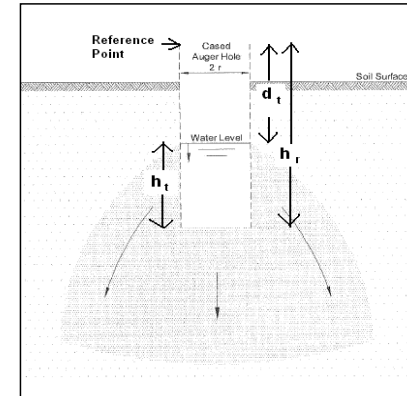
Comment field

Field not used

Fixed field

$$K = 1.15r \frac{\log_{10}(h_0 + \frac{1}{2}r) - \log_{10}(h_t + \frac{1}{2}r)}{t - t_0}$$

Parameter	Description	Value	Units
K	Hydraulic Conductivity		m/s
r	radius of test hole	0.045	m
t	time since start of measurement		s
h_r	reference point height above base	0.91	m
d_t	depth from reference point to water at time t		m
h_t	Water column height at time t		m
h_0	h_t at t=0		m



Test 1

t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.7	0.21		
20	0.765	0.145	3.7E-04	31.8
40	0.79	0.12	2.8E-04	23.8
60	0.82	0.09	2.7E-04	23.5
80	0.84	0.07	2.6E-04	22.4
100	0.86	0.05	2.6E-04	22.6
120	0.89	0.02	3.2E-04	27.5
AVERAGE			2.9E-04	25.3

Test 2

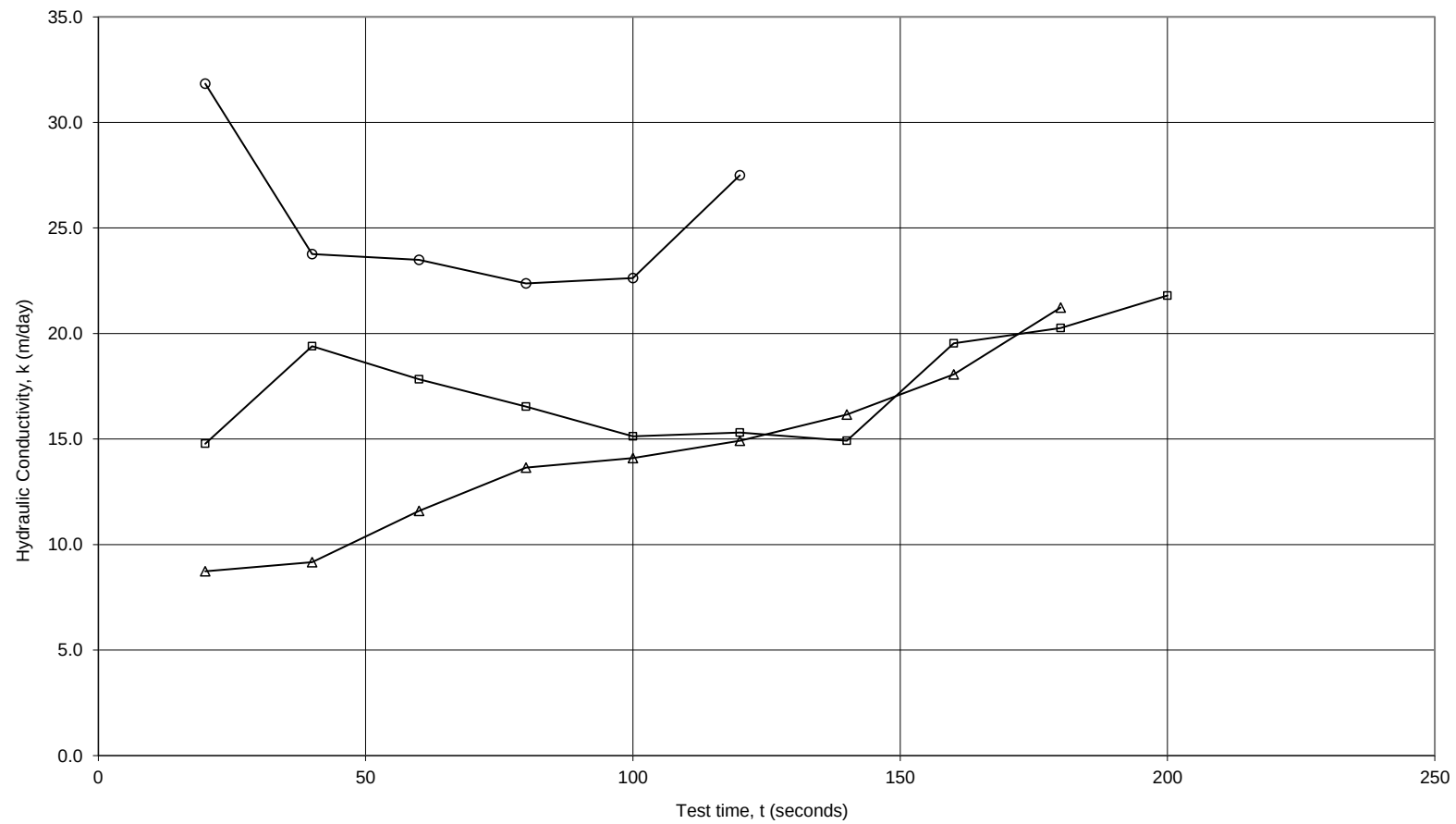
t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.72	0.19		
20	0.75	0.16	1.7E-04	14.8
40	0.79	0.12	2.2E-04	19.4
60	0.81	0.1	2.1E-04	17.8
80	0.825	0.085	1.9E-04	16.5
100	0.835	0.075	1.8E-04	15.1
120	0.85	0.06	1.8E-04	15.3
140	0.86	0.05	1.7E-04	14.9
160	0.89	0.02	2.3E-04	19.5
180	0.9	0.01	2.3E-04	20.3
200	0.91	0	2.5E-04	21.8
AVERAGE			2.0E-04	17.5

Test 3

t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.7	0.21		
20	0.72	0.19	1.0E-04	8.7
40	0.74	0.17	1.1E-04	9.2
60	0.77	0.14	1.3E-04	11.6
80	0.8	0.11	1.6E-04	13.6
100	0.82	0.09	1.6E-04	14.1
120	0.84	0.07	1.7E-04	14.9
140	0.86	0.05	1.9E-04	16.2
160	0.88	0.03	2.1E-04	18.1
180	0.9	0.01	2.5E-04	21.2
AVERAGE			1.6E-04	14.2

Hydraulic Conductivity by Inverse Auger Hole Method

BH02/IT02



Hydraulic Conductivity Calculation - Inverse Auger Hole Method

Galt Geotechnics

Spreadsheet author:

ORW

17-Oct-09

REFERENCE: Cocks, G. *Disposal of Stormwater Runoff by Soakage in Perth, Western Australia*, Journal and News of the Australian Geomechanics Society, Volume 42 No 3 September 2007, pp101-114

Job No: WAE200102-02

Client: Projective DM Pty Ltd

Project: Proposed Phase 1

Redevelopment

Location: Dianella Plaza

Shopping Centre

BH Name: BH03/IT03

Test Depth: 0.91 m

Spreadsheet Legend

Required input

Calculated field

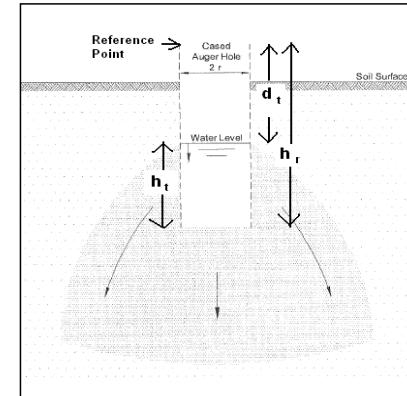
Comment field

Field not used

Fixed field

$$K = 1.15r \frac{\log_{10}(h_0 + \frac{1}{2}r) - \log_{10}(h_t + \frac{1}{2}r)}{t - t_0}$$

Parameter	Description	Value	Units
K	Hydraulic Conductivity		m/s
r	radius of test hole	0.045	m
t	time since start of measurement		s
h_r	reference point height above base	0.91	m
d_t	depth from reference point to water at time t		m
h_t	Water column height at time t		m
h_0	h_t at t=0		m



Test 1

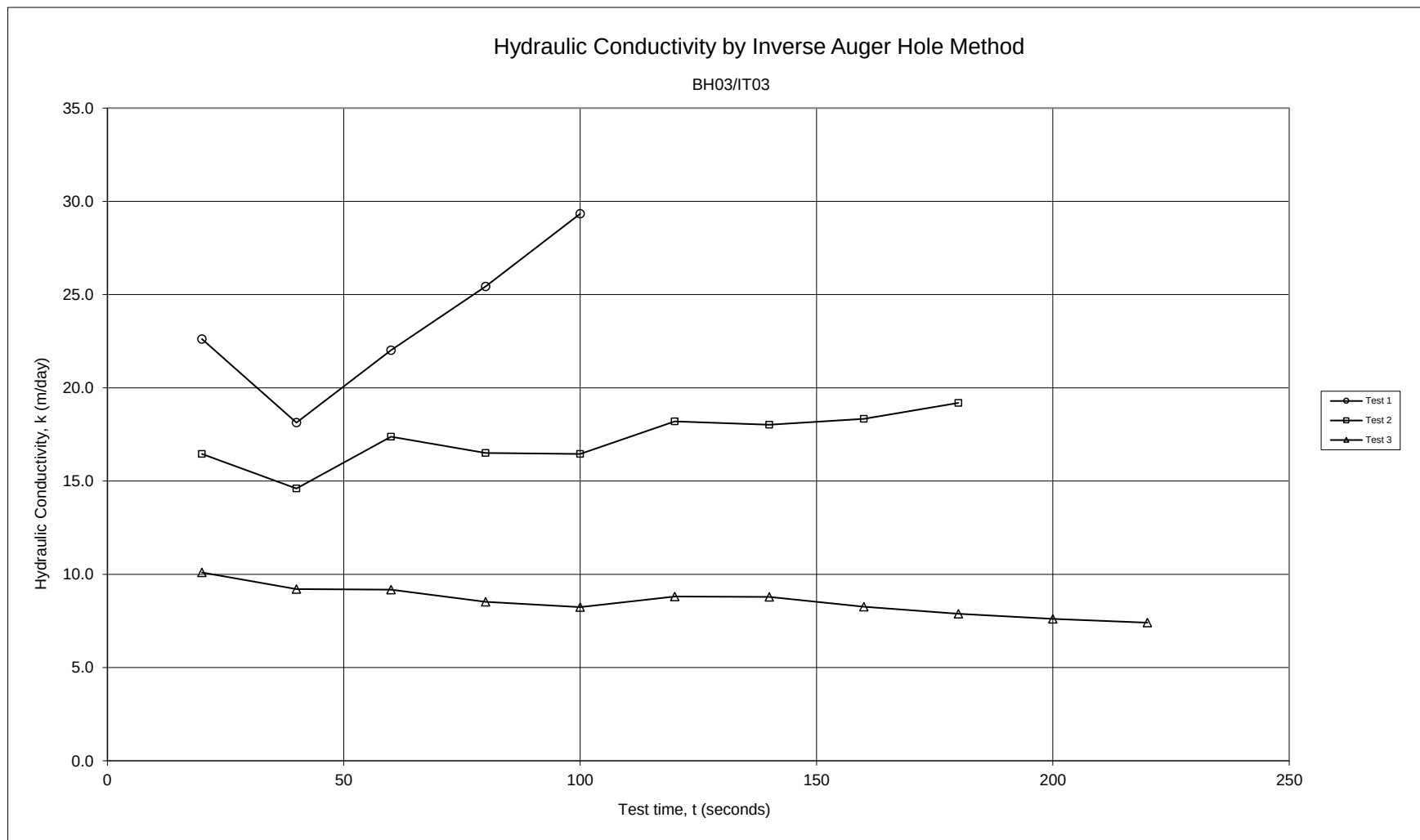
t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.74	0.17		
20	0.78	0.13	2.6E-04	22.6
40	0.8	0.11	2.1E-04	18.1
60	0.835	0.075	2.5E-04	22.0
80	0.865	0.045	2.9E-04	25.4
100	0.89	0.02	3.4E-04	29.3
AVERAGE			2.7E-04	23.5

Test 2

t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.74	0.17		
20	0.77	0.14	1.9E-04	16.4
40	0.79	0.12	1.7E-04	14.6
60	0.82	0.09	2.0E-04	17.4
80	0.835	0.075	1.9E-04	16.5
100	0.85	0.06	1.9E-04	16.5
120	0.87	0.04	2.1E-04	18.2
140	0.88	0.03	2.1E-04	18.0
160	0.89	0.02	2.1E-04	18.3
180	0.9	0.01	2.2E-04	19.2
AVERAGE			2.0E-04	17.2

Test 3

t (s)	d_w (m)	h_t (m)	K (m/s)	K (m/day)
0	0.73	0.18		
20	0.75	0.16	1.2E-04	10.1
40	0.765	0.145	1.1E-04	9.2
60	0.78	0.13	1.1E-04	9.2
80	0.79	0.12	9.9E-05	8.5
100	0.8	0.11	9.5E-05	8.2
120	0.815	0.095	1.0E-04	8.8
140	0.825	0.085	1.0E-04	8.8
160	0.83	0.08	9.6E-05	8.3
180	0.835	0.075	9.1E-05	7.9
200	0.84	0.07	8.8E-05	7.6
220	0.845	0.065	8.6E-05	7.4
AVERAGE			9.9E-05	8.5





Standard Geotechnical Definitions, Recommendations, Requirements and Limitations

GDR1 ABOUT THIS APPENDIX

These technical notes are to be read with the attached report. These notes contain important information regarding the study in the attached report, and the report cannot be considered in isolation without full reading of these notes.

Where there are conflicts between this appendix and the report text, the report text takes precedence.

Unless noted otherwise, geotechnical investigations are conducted in accordance with AS1726-2017, "Geotechnical site investigations".

Unless noted otherwise, the report does not include any assessment (or implied assessment) of karst risk.

GDR2 DEFINITIONS

The following definitions apply:

- **Approved Fill** – fill that has been assessed and approved by the geotechnical engineer or civil designer for a particular purpose.
- **Bulk Fill** – Controlled fill intended to support future infrastructure, but potentially lacking some engineering properties required for upper fill layers or adjacent to structures, where fill with specific properties may be required. Contrast with Select Fill.
- **Civil Design** – the engineering design of the earthworks including surface water and erosion control and subsurface drainage control (where required) to achieve an earthworked, drained site which is capable of supporting the proposed development (including target site classification to AS2870, where relevant). This design is separate to this geotechnical investigation and is a required element of a site development.
- **Clay** – A component of a soil with particles smaller than 0.002 mm in size.
- **Cohesionless (Non-cohesive) Soil** – A soil mass that has does not hold together at low applied stress levels. The strength of the soil depends solely on friction between particles.
- **Cohesive Soil** – A soil mass that has holds together and can adhere to itself.
- **Collapsible Soil** – a soil with high void ratio that is typically strong when dry but loses strength and consolidates under constant stress when wetted, usually due to loss of soil matric suction or dissolving of a chemical cementing agent.
- **Compaction** – The process of increasing the soil density, typically be mechanical means.
- **Competent Person** – A person who has, through a combination of training, education and experience, acquired knowledge and skills enabling that person to correctly perform a specified task.
- **Consistency** – The stiffness of a cohesive soil, at specific moisture contents, to resist mechanical stress or manipulation (remoulding).
- **Controlled (or engineered) Fill** – Any fill for which engineering properties are controlled during placement. Also referred to as structural fill.
- **Dense** – with respect to sandy soils, at a relatively high density index or dry density ratio, exhibiting better engineering parameters with respect to strength and stiffness than the same material at a lower density index.
- **Density** – A measure of the mass of material per unit volume.
- **Eccentric Load** – a load incorporating either a varying vertical load and/or a horizontal load such that the peak vertical stress exceeds the average vertical stress.
- **Fill** – Any material that has been placed by anthropogenic processes.
- **Fines** – A component of a soil with particles smaller than 0.075 mm in size.
- **Groundwater** – Water located beneath the earth's surface in pore spaces, fractures and voids in soil or rock.
- **Gravel** – A component of a soil with particles between 2.36 mm and 63 mm in size.

- **Heavily Loaded** – in reference to mobile plant, particularly intended for equipment where ground bearing pressures exceed 50 kPa and/or equipment has a high centre of gravity and could be prone to toppling. In reference to buildings/structures, where footing pressures exceed 100 kPa and/or footing dimensions exceed 1 m wide.
- **Hydraulic Conductivity** – ratio of volume flux to hydraulic gradient – a quantitative measure of soil's ability to transmit water when subjected to a hydraulic gradient. k_{sat} – saturated hydraulic conductivity, intended for dewatering assessment, subsoil drainage design and other engineering assessments where saturated soils are relevant. k_{unsat} – unsaturated hydraulic conductivity, intended for design of stormwater disposal elements such as soakwells and infiltration basins, where the base of disposal elements is above the groundwater level.
- **In situ** – In the place and condition in which it exists naturally. May also refer to fill that is present at any site prior to an investigation taking place.
- **Limestone** – A sedimentary carbonate rock. The use of the term does not infer a specific strength, carbonate content or grain size. Refer to GDR4.1 for further detail.
- **Loose** – with respect to sand soils, at a relatively low density index or dry density ratio, typically indicating poorer engineering parameters with respect to strength and stiffness than the same material at a higher density index.
- **Material** – Matter that meets the definitions of 'soil', 'rock', other engineered matter (i.e., concrete, bricks etc.) or non-engineered matter (organics, contaminated refuse, deleterious material).
- **May** – Indicates that the statement is an option.
- **Must** – Indicates that the statement is mandatory.
- **Natural** – In the context of soil or rock, material which is present as a result of natural geological processes and has not been subject to anthropogenic engineering processes (such as filling, excavation, replacement, etc).
- **Organic** – In the context of soil, material derived from living matter, primarily plants.
- **Overconsolidated** – a soil that has been subjected to a greater vertical stress than its current state.
- **Permeable Soil** – soil that meets the civil design permeability requirements to allow relatively rapid flow of water through the soil matrix.
- **Rock** – Any aggregate of minerals and/or materials that cannot be disaggregated by hand in air or water without prior soaking.
- **Sand** – a component of soil with particle size between 0.075 mm and 2.36 mm.
- **Select Fill** – a controlled fill which has been chosen for particular engineering characteristics (such as strength, CBR, grading, permeability, etc), commonly for use as a higher-grade capping layer or adjacent to structures. Contrast with Bulk Fill.
- **Shall** – Indicates that the statement is mandatory.
- **Should** – Indicates that the statement is a recommendation.
- **Silt** – A component of a soil with particles between 0.075 mm and 0.002 mm in size.
- **Soil** – Particulate materials that occur in the ground and can be disaggregated or remoulded by hand in air or water without prior soaking.
- **Sand** – A component of a soil with particle between 0.075 mm and 2.36 mm in size.
- **Uncontrolled Fill** – Any material that has been deposited by anthropogenic process, which does not meet the definition of 'controlled fill'.

GDR3 GEOTECHNICAL TEST METHODS AND INTERPRETATION

GDR3.1 Test Pit Excavation

Test pit excavations are formed using mechanical excavation equipment (typically an excavator) or hand dug, with the objective of inspecting (or profiling) the soil exposed in the excavation.

Typical limitations on test pit excavations are:

- Limited depth of excavation – typically governed by reach of the excavator arm.
- Cannot be excavated below groundwater in cohesionless soils, due to collapse and water ingress.
- Cannot be excavated through very stiff / very dense soils (i.e., desiccated clays or cemented soils) or most rock.
- Cannot typically obtain rock samples that are suitable for strength testing.

Test pits are usually mechanically excavated with a toothed bucket (intended for excavation in clay or weak rock) or a flat-edged bucket (typically for sands).

When hand-dug test pits are excavated, it is usually for recovery of near-surface soils or inspection of shallow in-ground elements.

We note that where test pits are excavated on a site, they are only ever loosely backfilled during our studies. They must always be located during site preparation works, over-excavated to their full depth and plan extents and re-filled with approved fill in compacted layers.

GDR3.2 Cone Penetration Tests (CPTs)

Cone penetration testing (CPT) is done by Galt or specialist contractors and typically to AS1289.6.5.1. The test involves pushing an instrumented cone into the soil with a hydraulically operated pushing frame. The test measures tip resistance and sleeve friction on the cone, which are then plotted with depth.

We interpret soil types and associated geotechnical soil parameters from CPT data using the following:

Technical Interpretations and International Guides

- Robertson P.K., Campanella R.G., Gillespie D. and Grieg J. (1986). "Use of piezometer cone data". Proceedings of the ASCE Speciality Conference In Situ '86: Use of In Situ Tests in Geotechnical Engineering, Blacksburg, pp 1263-80, American Society of Civil Engineers (ASCE).
- Robertson, P.K., Cabal K.L. (2016) "Guide to Cone Penetration Testing for Geotechnical Engineering 6th Edition 2015". Gregg Drilling & Testing, Inc., California.
- Baldi G., Bellotti R., Ghionna V.H., Jamiolkowski M., Lo Presti D. C. (1989) "Modulus of sands from CPTs and DMTs". Proc. 12th Int. Conf. on SMFE, Rio de Janeiro, Vol 1, p165-170, Balkema, Rotterdam.

Local (Perth and Western Australia) Research, Interpretation and Guides

- Fahey, M., Lehane, B., Stewart, D. (2003) "Soil stiffness for shallow foundation design in the Perth CBD". Australian Geomechanics Vol. 8 No. 3.
- Main Roads Western Australia (MRWA) (2009) "Structures Engineering Design Manual". Document 3912/03, Perth.
- Lehane B. (2017). "CPT-Based Design of Foundations", E.H. Davis Memorial Lecture, Australian Geomechanics, Vol 54. No. 4' and
- Galt's in-house correlations between CPT data and other geotechnical testing.

GDR3.3 Borehole Drilling

Boreholes are drilled for sampling of the soil and rock, with a small disturbance footprint. Typical techniques are:

- Auger drilling (hand auger or machine auger) – for recovery of soil at relatively shallow depths only. Cannot penetrate cemented soils or rock.
- Push probe drilling – for recovery of soil at relatively shallow depths and below groundwater. Cannot penetrate cemented soils or rock.
- Air core drilling – for recovery of soil, cemented soil and rock (typically up to high strength rock). Not suited to drilling of very high strength rock.
- Diamond coring (or rotary coring) – for recovery of cemented soil, rock and some soil types (typically not sand). Suited to all strengths of rock.

If used, standard penetration tests (SPTs) are done in accordance with AS1289.6.3.1. Correlations for consistency and density are based on:

- Standards Australia (2016), "HB160-2006, Soils Testing".

GDR3.4 Dynamic Cone Penetrometer (DCP)

The DCP is a hand-held tool for assessing penetration resistance of a soil. This comprises a 16 mm rod equipped with a 20 mm cone, hammered into the ground using a falling 9 kg weight on a 510 mm slide hammer on the top of the rod. This is done in accordance with AS1289.6.3.2 and the blow counts to hammer in the rod are measured in 100 mm penetration increments. Where provided, correlations for consistency and density are based on:

- Standards Australia (2016), "HB160-2006, Soils Testing".

GDR3.5 Perth Sand Penetrometer (PSP)

The PSP is a variation on a DCP and uses a 9 kg weight on a 600 mm slide hammer to hammer in a 16 mm rod with a blunt (square-faced) end. Testing is done in accordance with AS1289.6.3.3, with the following typical variations:

- Testing is often done to a greater depth than the 450 mm covered in the standard.
- Blow counts are sometimes recorded in 150 mm intervals (compared to 300 mm intervals used in the standard) to provide better resolution on the tests.

Where provided, correlations for density are based on:

- Standards Australia (2016), "HB160-2006, Soils Testing".

GDR3.6 Dynamic Probing Super Heavy (DPSH)

The DPSH test involves driving a solid cone (20 cm²) into the ground using a 63.5 kg hammer falling 760 mm. Testing is done in accordance with EN ISO 22476-2 – Geotechnical engineering – Field testing – Part 2: Dynamic probing – DPSH-B.

Results may be presented as either:

- N10 (No. of blows required for every 100 mm penetration);
- N30 (No. of blows required for every 300 mm penetration); or
- q_d (dynamic tip resistance, analogous to CPT q_c).

GDR3.7 Inverse Auger Hole Infiltration Test (Falling Head, Unsaturated Soil)

Infiltration tests are carried out using the 'inverse auger hole' method described by:

- Cocks, G (2007), "Disposal of Stormwater Runoff by Soakage in Perth Western Australia", Journal and News of the Australian Geomechanics Society, Volume 42 No. 3, pp 101-114

This test is an unsaturated falling head test, in that it is carried out above the groundwater table and is intended to mimic the behaviour of soak wells and similar drainage elements (i.e. soakage basins), which discharge stormwater into an unsaturated medium.

The hole is wetted only for a short period prior to the testing.

The test is usually repeated three times, with the intention that the second and third tests provide similar results (within about 10%-20%). Tests are done over a short duration, typically 2 minutes to 10 minutes. The focus of the testing is generally when the head is low (200 mm or lower), such that the relevant lateral zone is as saturated as the zone directly below the borehole.

The hydraulic conductivity derived from this test is not to be used for applications where saturated hydraulic conductivity is relevant, e.g.:

- Subsoil drainage design; and
- Dewatering estimations.

Based on Galt's in-house research, this method does not completely saturate the soil in any reasonable test length, and thus may not be suitable for assessment of soils at sites where the critical drainage condition is a fully saturated soil (i.e., in areas with high groundwater tables). Our research on sand sites indicates that the test does correlate well with actual soak well performance, in unsaturated sand zones without impermeable zones.

GDR3.8 Guelph Permeameter Test (Constant Head, Quasi-Saturated Soil)

The Guelph permeameter test, conducted in accordance with the constant head test method outlined in Appendix G of AS1547, is a constant-head test in nominally "saturated" soil (in that the test is conducted until a "steady state" is reached). However, we note that this test can only be done above the groundwater table and as such, is in an unsaturated zone. Therefore, the hydraulic conductivity derived from this test should be used with caution and evaluated against other test methods (such as saturated, constant-head permeability testing from laboratory samples, or in situ saturated hydraulic conductivity testing below the groundwater table).

GDR4 GEOLOGICAL UNITS

GDR4.1 Limestone

The term 'Limestone' is used to describe a carbonate rock. Tamala Limestone is the common limestone in Western Australia, and typically comprises cemented quartz and shell fragments cemented together by calcium carbonate.

Limestone can vary significantly across short distances in composition, strength and cementation. Tamala limestones in Western Australia also have known possible geological features including:

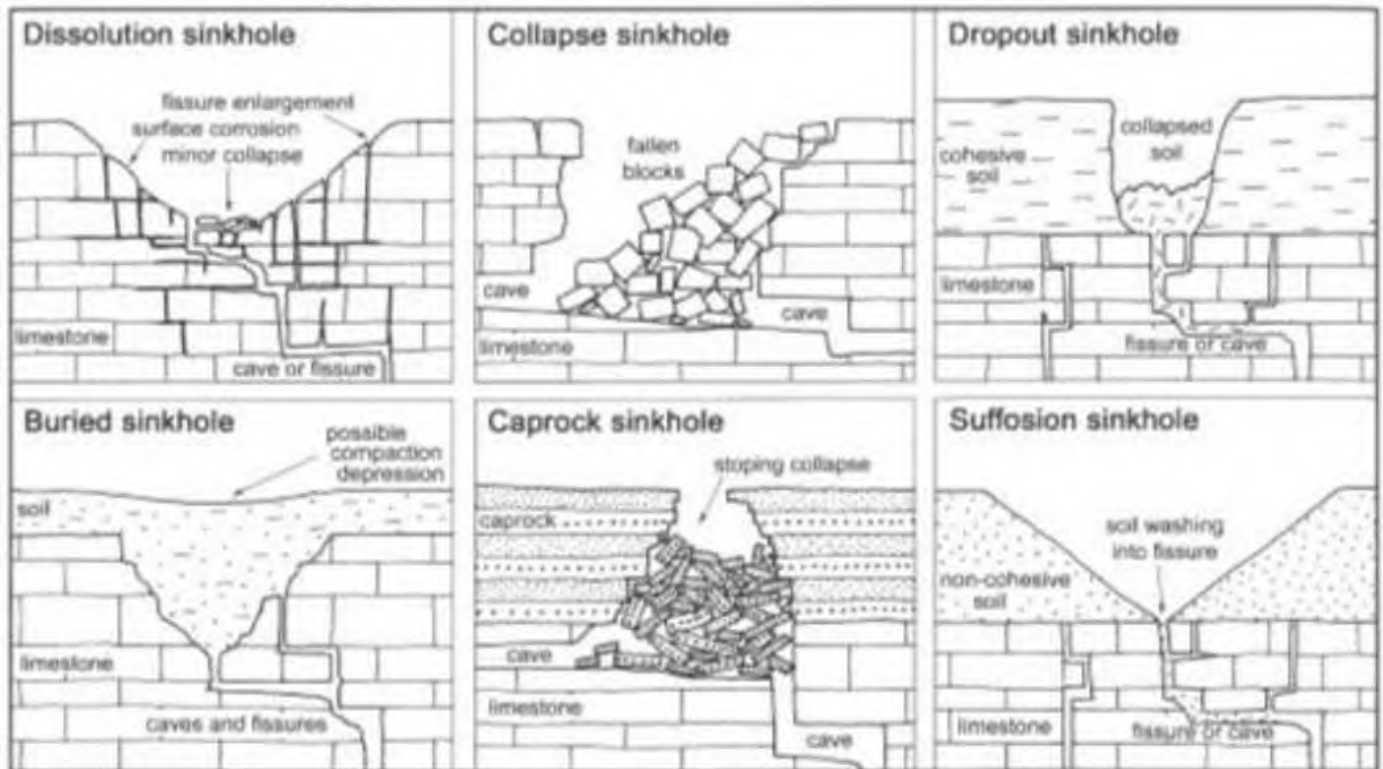
- Caprock/calcrete – The formation of a very hard duricrust, usually due to sun exposure. Caprock may be up to 3 m thick, but typically around 1.5 m thick. Caprock is very difficult to excavate and may require the use of hydraulic rock breakers or rock saws to excavate.
- Solution features/tubes – Often initially formed due to the presence of Eucalypt and Jarrah roots during limestone formation, and often increasing in depth and size due to ongoing weathering. May be up to 500 mm in diameter. These are typically filled with very loose, unconsolidated sand.
- Pinnacles – Pinnacles are usually the limestone that is left around surrounding solution features. Often can comprise very hard limestone/caprock that can be substantially higher than surrounding areas. Pinnacles may have also been formed by surrounding erosion (i.e., wind/water).
- Karst/caves – Karst is caused by the dissolution of limestone, typically where there is interaction in low-lying areas with water and limestone. Karst manifests itself as loose near-surface sand with cavities (caves) in the underlying limestone. This can lead to sinkholes and collapse of overlying structures.

Inline images showing typical pinnacle/solution features and Karstic features follow. These are taken from:

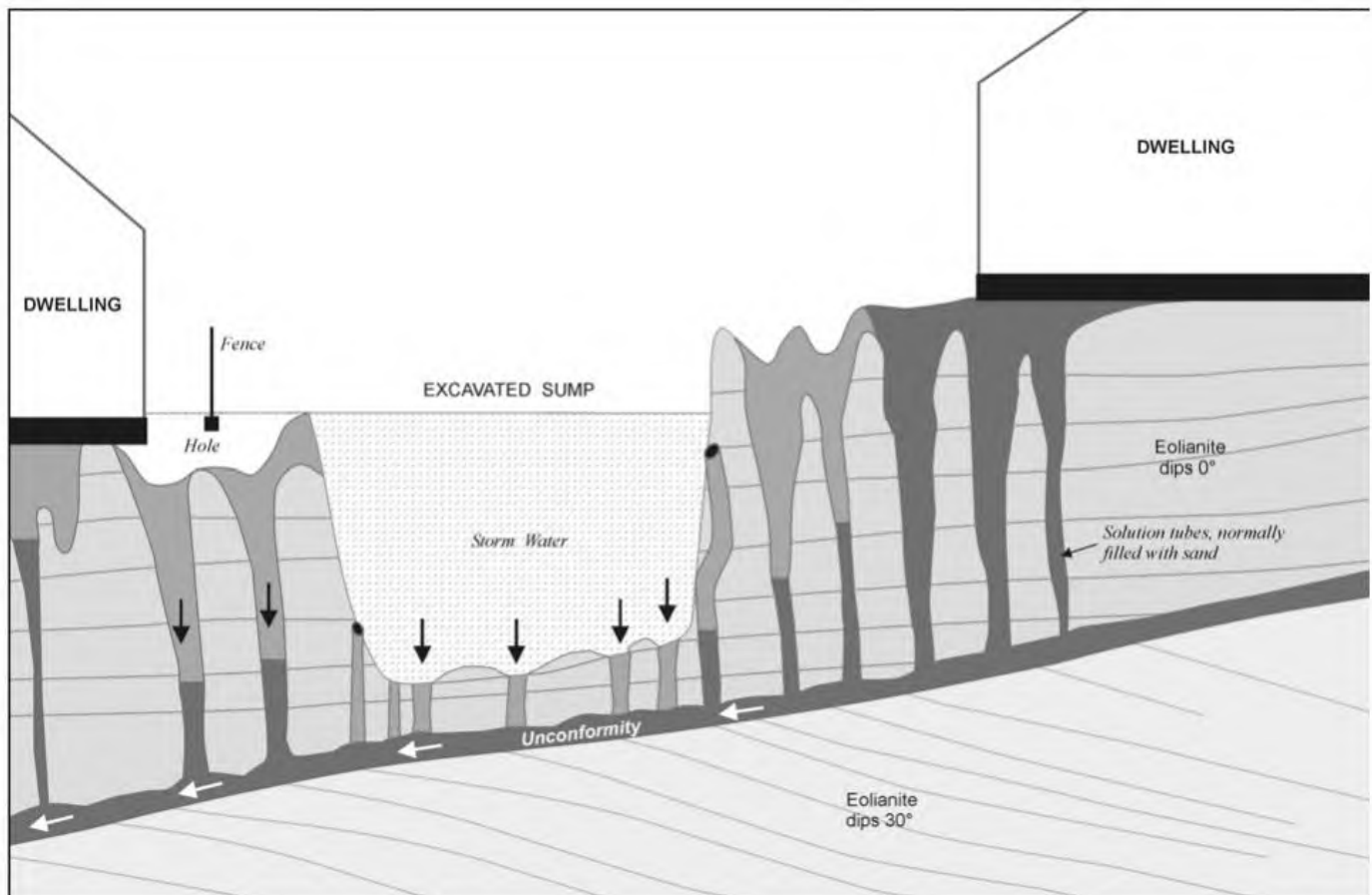
- Gordon, R. (2003). "Coastal Limestones". Australian Geomechanics Vol.38 No. 4, The Engineering Geology of Perth.

- Waltham, A. & Fookes, P. (2003). "Engineering Classification of Karst Ground Conditions: Quarterly Journal of Engineering Geology and Hydrogeology, Vol 36.

Inline Image GDR 1 - Karstic Sinkhole Features from Waltham and Fookes (2003)



Inline Image GDR 2: Pinnacle/Solution Features from Gordon (2003)



GDR4.2 Pindan Sands and Collapsible Soils

In the Western Australian context, Pindan sands are sandy soils present predominantly across the Pilbara and Kimberley regions. Pindan sands are typically:

- Red brown in colour.
- Between 10% and 40% fines.
- Of aeolian origin, usually resulting in unconsolidated in situ conditions (nuclear density gauge testing often indicates these soils have in situ density ratios of 80%-85% of modified maximum dry density).
- Very strong when dry due to high soil suctions in the fine fraction, which create strong bonds between the sand particles.

As the grains are usually held in place by the dry fine fraction, this can lead to:

- very high settlements (i.e., “collapse”) as the grain-to-grain bonds are weakened as matric suction decreases on soaking; and
- loss of vertical and horizontal strength/stiffness as the grain-to-grain bonds weaken.

The risks associate with Pindan sands are usually quantified in terms of the collapse potential/magnitude of possible collapse events.

Other similar soils are present in Western Australia that may exhibit similar collapse potential and may not strictly be Pindan sands (i.e., have other grain-to-grain bonding mechanisms).

GDR5 SITE CLASSIFICATION

Site classification refers to the assessment of a site in reference to AS2870-2011, “Residential slabs and footings”. The method for assessing the site class is outlined in Section 2 of AS2870-2011, which indicates that this may be done by:

- assessing the characteristic surface movement, due to seasonal moisture changes in the soil profile;
- assessing the performance of existing foundations; or
- assessment of the soil profile (where there are deleterious inclusions, landfill, putrescible waste etc.).

The site classifications based on the expected characteristic surface movement are summarised in Table GDR 1.

Table GDR 1: Summary of Site Classifications (AS2870-2011)

Class	Description	Characteristic Surface Movement (y_s)
A	Most sand and rock site with little or no ground movement from moisture change	Not Defined (typically <5 mm)
S	Slightly reactive clay sites with only slight ground movement from moisture changes	0 – 20 mm
M	Moderately reactive clay sites, which may experience moderate ground movements from moisture change	20 – 40 mm
H1	Highly reactive sites, which may experience high ground movements from moisture change	40 – 60 mm
H2	Highly reactive sites, which may experience very high ground movements from moisture change	60 – 75 mm
E	Extremely reactive sites, which may experience extreme ground movements from moisture change	>75 mm
P	Sites which include soft soils, such as soft clay or silt or loose sands; landslip; mine subsidence; collapsing soils; soils subject to erosion; reactive sites subject to abnormal moisture conditions or sites which cannot be classified otherwise	Not Defined

The calculated characteristic surface movement is predominantly based on:

- the reactivity (i.e., the shrink-swell potential) of the soil (and any proposed fill);

- the design depth of soil suction change, which is the maximum expected depth of soil suction change due to seasonal soil moisture changes; and
- the depth to any bedrock and groundwater table.

The design depth of soil suction change for Western Australia has been refined using the Thornthwaite Moisture Index (TMI). We have carried out assessment using the depths as detailed in:

- Hu Y, Saraceni P, Cocks G, Zhou M (2016). "TMI assessment and climate zones in Western Australia". Australian Geomechanics Journal, Vol.51 No.3.
- Hu Y, Raj A, Cocks G, Verheyde F (2019). "Re-assessment of TMI based climate zones in metropolitan Perth, WA". ANZ Geomechanics Conference 2019, Perth Australia.

The design depth of soil suction change for Northern Territory is based on the research presented in:

- Jackson, S (2022), "Thornthwaite moisture index and climate zones in the Northern Territory", Australian Geomechanics Journal, Vol. 57 No. 3.

We highlight that AS2870-2011 does not make any reference to the fines content of a soil when assessing the site classification.

Where a site classification is provided in our reports, it is always predicated on the requirement that the recommended site preparation procedures are carried out.

We also highlight that the footing performance and shrink-swell movements of a site can be impacted by the planting or removal of trees. This should be considered where appropriate, and we refer to the CSIRO BTF 18-2011 "Foundation Maintenance and Footing Performance: A Homeowner's Guide" for further information.

AS 2870 is limited to single and double storey residential buildings with normal shallow footings with a maximum bearing pressure of 100 kPa and is not applicable where development types other than this are proposed.

GDR6 SITE PREPARATION

GDR6.1 General

The intent of the site preparation guidelines provided in the above report are to ensure that the earthworks can be constructed to meet specific requirements, i.e., minimum compaction, fill requirements, removal of unsuitable material etc. The site preparation guidelines are not exhaustive, and on-site conditions may dictate that other preparation measures may be required to meet geotechnical requirements.

GDR6.2 Site Preparation

Site preparation measures outlined in this section relate to bulk earthworks at the site in preparation for the construction of buildings, pavements and other structures.

The preparation of a site in accordance with outlined measures below or those presented in the report text does not imply that the site is suitable for heavily loaded plant or eccentric loads. This is especially applicable for working platforms for mobile plant including cranes, crawlers or the like. The site surface may still not be trafficable for mobile plant. Individual working platform assessments must be done if heavily loaded mobile plant are proposed.

GDR6.2.1 Common Measures

The common measures outlined below are to prepare standard sites in advance of proof compaction, bulk excavation and filling. These measures are applicable to most sites, however the applicability of these measures is stated in the main report.

Table GDR 2: Common Measures

Measure	Commentary
Demolish and remove structures and pavements	Demolish existing structures and pavements, including removal of all buried services and footings and dispose off-site.
Remove demolition debris and other deleterious material	Remove any demolition debris and other deleterious material from site including old footings, slabs, soak wells, buried services, paving and building rubble.
Strip uncontrolled fill (where present)	Strip any uncontrolled fill from the site (where encountered) and, if suitable, stockpile it for potential re-use as non-structural fill. If contaminated, dispose off-site. Refer to the report text for discussions on the presence of detected uncontrolled fill and its composition. It is important to realise that undetected uncontrolled fill may be present between test locations and the absence of its identification in our report does not preclude its presence. If uncontrolled fill is detected during site works, please contact us for inspection and to provide recommendations.
Remove trees	All tree roots must be removed, this may result in significant excavation in places. Where tree roots and stumps are removed, the disturbed soil must be over-excavated and replaced with controlled, compacted fill. Backfilling of over-excavations is discussed in the following sections.
Strip and stockpile topsoil.	Strip and stockpile topsoil from unpaved areas of the site for potential re-use in non-structural applications. The topsoil strip is only necessary to remove roots and we recommend a topsoil strip as necessary to remove all roots from the soil.
Carry out bulk excavation	Excavate to the required level. Stockpile suitable excavated material for potential re-use as fill (the re-use of spoil as fill, if appropriate, is discussed in the report text) and remove unsuitable or excess material off-site.
Batter edges of excavation	Excavations should be battered to a temporary slope as given in the report text where applicable and not in close proximity to adjacent structures etc. If required, construct temporary/permanent retaining walls where batters cannot be accommodated.

By following these measures, the site should have been prepared to a point where topsoil and vegetation has been removed to expose either natural soil or controlled fill. Over-excavation to the required levels may then be required for some projects. Once complete, the site is now ready for proof compaction and filling.

GDR6.2.2 Sand Sites

The preparation measures outlined below are provided for sand sites meeting the following criteria:

- Site underlain by sand.
- No collapsible soils present.
- No deep loose sand.
- Compaction of a loose upper horizon to maximum 1 m depth.
- No shallow groundwater (<1 m deep).
- No limestone or other rock present at shallow depth.
- "Common Measures" outlined in Section GDR6.2.1 have been completed (as required).

The applicability of these measures is stated in the main report. These measures must be carried out for all areas where structures, footings, pavements and any other settlement-sensitive infrastructure is proposed.

Unless specified otherwise in the report, the **Approved Fill** to be used is outlined in Section GDR8 (**Permeable Sand** where permeable fill is required, else **General Sand**). The specific selection is subject to the requirements of the civil designer.

Table GDR 3: Sand Site Measures

Measure	Commentary
Moisture condition and proof compact.	Moisture condition and compact the exposed sandy ground to achieve the density specified in Section GDR7.1 ("sand") to a depth of at least 900 mm.
Test proof compaction	Check that the density specified in Section GDR7.1 ("sand") has been achieved to a depth of at least 900 mm. We note that the applicability of the use of the PSP for compaction control is discussed in the report. Unless specifically approved for use on the subject site, the contractor must not assume that the use of the PSP is appropriate.
Treat areas of loose or unsuitable material	Any areas of loose sand or unsuitable material (including over-excavated areas of former trees and root balls) must be removed and replaced with Approved Fill as outlined in the report or as noted above. The report will explain the suitability of site-derived materials for re-use as approved fill.
Carry out bulk filling	Where fill is required to build up levels, use Approved Fill , placed and compacted in layers of no greater than 300 mm loose thickness. Test compaction to achieve the density specified in Section GDR7.1.

In following this method, shallow/surficial loose sand will be compacted, and the site will be filled (where required) in preparation for supporting footings, ground slabs, pavements and the like.

GDR6.2.3 Deep Loose Sand Sites

The preparation measures outlined below are provided for sand sites meeting the following criteria:

- Site underlain by sand.
- Collapsible soils or deep loose sand present (if applicable, this is discussed in the report).
- Over-excavation, compaction and replacement of loose sand required.
- No shallow groundwater (<1 m deep).
- No limestone or other rock present at shallow depth.
- "Common Measures" outlined in Section GDR6.2.1 have been completed.

The greatest depth of compaction that can be achieved with standard compaction equipment (vibrating roller, etc) is around 1 m (for sands). As such, it is necessary to cut down the site level to a point where this compaction can be done to the lowest level needed to be improved.

The applicability of these measures is stated in the main report. These measures must be carried out for all areas where structures, footings and any other settlement-sensitive infrastructure are proposed. Not typically required for pavement subgrades, however, this is discussed in the report if required.

Unless specified otherwise in the report, the **Approved Fill** to be used is outlined in Section GDR8 (**Permeable Sand** where permeable fill is required, else **General Sand**). The specific selection is subject to the requirements of the civil designer.

Table GDR 4: Deep Loose Sand Site Measures

Measure	Commentary
Over-excavate to the required depth.	Over-excavate sand soil to the depth stated in the report and, if appropriate (discussed in report) retain it for re-use as fill. Over-excavation is likely to be done in stages depending on the site area available for earthworks. Excavations must be battered to a temporary slope as given in the report text where applicable and not in close proximity to adjacent structures etc. If required, construct temporary/permanent retaining walls where batters cannot be accommodated.
Moisture condition and proof compact.	Moisture condition and compact the exposed sandy ground to achieve the density specified in Section GDR7.1 ("sand") to a depth of at least 900 mm.
Test proof compaction	Check that the density specified in Section GDR7.1 ("sand") has been achieved to a depth of at least 900 mm. We note that the applicability of the use of the PSP for compaction control is discussed in the report. Unless specifically approved for use on the subject site, the contractor must not assume that the use of the PSP is appropriate.
Treat areas of loose or unsuitable material	Any areas of loose sand or unsuitable material (including over-excavated areas of former trees and root balls) must be removed and replaced with compacted Approved Fill as outlined in the report or as noted above. The report will explain the suitability of site-derived materials for re-use as approved fill.

Measure	Commentary
Carry out bulk filling	Where fill is required to build up levels (including restoration of the site surface level to the original level), use Approved Fill , placed and compacted in layers of no greater than 300 mm loose thickness. Test compaction as specified in Section GDR7.1.

In following this method, deep, loose sand will be compacted to a sufficient depth to reduce settlement impacts and the site will be filled (where required) in preparation for supporting footings, ground slabs, pavements and the like.

GDR6.2.4 Clayey Sites

The preparation measures outlined below are provided for sand sites meeting the following criteria:

- Site underlain by cohesive soils (typically >12% fines, i.e., clayey enough for the fines proportion of the soil to dominate behaviour).
- No collapsible soils present.
- No deep soft soils or organic soils.
- Over consolidated clayey soils present which will not be subject to significant primary or secondary consolidation (settlements expected to be within the limit of typical seasonal movements occasioned by moisture content changes, which would be captured in assignment of an AS2870 site classification).
- No shallow groundwater (<1 m deep)
- No rock present at shallow depth.
- “Common Measures” outlined in Section GDR6.2.1 have been completed.

The applicability of these measures is stated in the main report. These measures must be carried out for all areas where structures, footings, pavement subgrades and any other settlement-sensitive infrastructure is proposed.

Unless specified otherwise in the report, the **Approved Fill** to be used is **Clay** as outlined in Section GDR8.

Table GDR 5: Clay Site Measures

Measure	Commentary
Moisture condition and proof compact.	Moisture condition and compact the exposed clayey ground to achieve the density specified in Section GDR7.1 (“fine grained soils”) to a depth of at least 300 mm.
Test proof compaction	Check that the density specified in Section GDR7.1 (“fine grained soils”) has been achieved to a depth of at least 300 mm. The use of a penetrometer for compaction control of cohesive soils is not an appropriate substitute for in situ NDG testing.
Treat areas of loose or unsuitable material	Any areas of soft clayey soils or unsuitable material (including over-excavated areas of former trees and root balls) must be removed and replaced with compacted Approved Fill . The report will explain the suitability of site-derived materials for re-use as approved fill.
Carry out bulk filling	Where excavations are done into clayey soils (e.g. to treat soft zones, remove root balls and the like), they must not be backfilled filled with sand fill (even where a sand topping layer is proposed). Where fill is required (including backfilling of excavations to remove trees), only use Approved Fill , moisture conditioned, placed and compacted in layers of no greater than 300 mm loose thickness. Test moisture and compaction as specified in Section GDR7.1.
Grade completed clayey surface	Surface water control is essential for clayey sites. This also applies to control of infiltrated water into sand topping layers or the like. The surface of clayey ground must be graded at a minimum of 1% crossfall to drain. This is a general recommendation and an appropriate civil design must be done to account for surface and subsoil drainage.
Install sand topping layer	Where a sand topping layer is proposed, this should be done as outlined in Section GDR6.2.5.

These measures do not take into account the objectives of the civil design for the site, particularly with regard to surface water drainage and groundwater control (including clay grading, subsoil drainage, thickness and composition of a sand topping layer and the like). This must be taken into account by the civil designer. General commentary on drainage control measures is presented in Section GDR14.

GDR6.2.5 Sand Topping Layer

Where a sand topping layer is required:

Unless specified otherwise in the report, the **Approved Fill** to be used is outlined in Section GDR8 (**Permeable Sand** where permeable fill is required, else **General Sand**). The specific selection is subject to the requirements of the civil designer.

Table GDR 6: Sand Topping Layer Measures

Measure	Commentary
Prepare Substrate	Prepare the clayey or other substrate as separately outlined prior to installing the topping layer.
Build up sand topping layer	Build up level to the required level with Approved Fill , placed and compacted in layers of no greater than 300 mm loose thickness to achieve the density specified in Section GDR7.1.

For the purposes of achieving the allowable bearing pressures and site classification discussed in the report, it is not necessary to have the bases of slabs and footings in the sand topping layer, i.e. if required, they may extend through the sand topping layer into clayey soil below.

GDR6.2.6 Limestone Sites

The preparation measures outlined below are provided for sites underlain by limestone (refer to Section GDR4.1), meeting the following criteria:

- Site underlain by sand overlying limestone.
- Compaction of a loose upper horizon to maximum 1 m depth, with localised deeper treatments between pinnacles if required.
- No shallow groundwater (<1 m deep)
- “Common Measures” outlined in Section GDR6.2.1 have been completed.

The site preparation measures outlined below are aimed at improvement of the site in preparation for construction of the structures including on-ground slabs, shallow footings, retaining walls and pavements.

Unless specified otherwise in the report, the **Approved Fill** may comprise one of the following as specified in Section GDR8 (the specific selection is subject to the requirements of the civil designer):

- **Permeable Sand** where permeable fill is required
- **General Sand** where permeable fill is not required
- **Mixed Sand/Limestone Fill** where permeable fill is not required

The re-use of any limestone for fill is subject to the requirements of the civil design and discussions in the report text. The use of **Mixed Sand/Limestone Fill** is discussed in Section GDR6.2.7. The preparation measures outlined in Table GDR 7 assume sand fill.

Table GDR 7: Standard Limestone Site Measures (Bulk Earthworks)

Measure	Commentary
Treat zones of loose sand	Where deep loose sand is present (particularly, but not exclusively, between limestone pinnacles), over-excavate to the depth as noted in the report. Sand should be retained for re-use as fill if recommended in the report. Limestone debris and pinnacles should be separated and only re-used if recommended in the report.
Moisture condition and proof compact.	Moisture condition and compact the exposed sandy ground to achieve the density specified in Section GDR7.1 ("sand") to a depth of at least 900 mm. Proof compaction of intact limestone is not required.
Test proof compaction	Check that the density specified in Section GDR7.1 ("sand") has been achieved to a depth of at least 900 mm. We note that the applicability of the use of the PSP for compaction control is discussed in the report. Unless specifically approved for use on the subject site, the contractor must not assume that the use of the PSP is appropriate. If refusal to the test method is encountered within the target test depth on limestone and the results to the refusal depth are acceptable, it is not necessary to repeat compaction testing at that location. Compaction control of intact limestone is not required.
Treat areas of loose or unsuitable material	Any areas of loose sand or unsuitable material (including over-excavated areas of former trees and root balls) must be removed and replaced with compacted Approved Fill as outlined in the report or as noted above. The report will explain the suitability of site-derived materials for re-use as approved fill.
Carry out bulk filling	Where fill is required to build up levels, use Approved Fill , placed and compacted in layers of no greater than 300 mm loose thickness. Test compaction to achieve the density specified in Section GDR7.1.

These measures do not take into account the specifics of the civil design, including the requirement (if any) for excavatable and/or free draining layers to achieve construction and drainage objectives. The civil design must take precedence and is not specifically considered in this advice.

Soakwells can perform poorly in limestone and specific advice may apply to the installation of soakwells in limestone areas. If not discussed in our report, please contact us for further advice.

Without further consultation with the structural designer, footings for any one structure must not be founded on a mixture of sand and intact limestone. This is due to potential differential settlements between limestone zones (relatively stiff) and soil zones (relatively soft). Where this is the case, the measures outlined in Table GDR 8 must be followed, only with guidance from the structural designer and Galt.

Table GDR 8: Standard Limestone Site Measures (Footing and Slab Preparation)

Measure	Commentary
Excavate and compact for slabs, subgrades, pad or strip footings	Excavate for pad and strip footings. Where a mix of soil and limestone is present below any one structure, one of the following must be done (to be agreed with structural designer and us): ▪ Over-excavate limestone and replace with compacted soil: Typically where the foundation largely comprises soil and a relatively small amount of limestone is present. Where footings and slabs are founded partly on soil and partly on limestone, over-excavate the limestone by at least 300 mm below the base of footing or slab and replace the excavated material with compacted Approved Fill. ▪ Remove soil from over limestone and replace with concrete: Typically where the foundation largely comprises limestone and a relatively small amount of soil is present. Localised zones of sand and mixed sand/limestone rubble must be removed and replaced with lean-mix concrete, e.g. 10 MPa blinding concrete. ▪ Design the structure to accommodate differential foundation movements: For example, include construction joints or use a more heavily reinforced footing (subject to the structural designer's requirements).
Test compaction of footing bases, slabs or subgrades.	Compact the exposed bases to achieve the density specified in Section GDR7.1 ("sand"), to a depth of at least 900 mm, or to the depth where limestone is intersected. If refusal to the test method is encountered within the target test depth on limestone and the results to the refusal depth are acceptable, it is not necessary to repeat compaction testing at that location. Compaction control of intact limestone is not required. Remove, replace and compact as required with approved fill any zone not achieving the density specified in Section GDR7.1 ("sand")

GDR6.2.7 Mixed Sand/Limestone Filling

On sites where deemed appropriate by the Civil Design, **Approved Fill** may comprise limestone rubble fill (**Mixed Sand/Limestone**, as specified in Section GDR8).

The preparation measures outlined below are provided for sites meeting the following criteria:

- No shallow groundwater (<1 m deep)
- “Common Measures” outlined in Section GDR GDR6.2.1 have been completed.
- Substrate preparation for the relevant site type has been done in preparation for further filling (as relevant for sand, limestone or clayey sites discussed in the preceding sections).

The site preparation measures outlined below are required prior to construction of structures including on-ground slabs, shallow footings, retaining walls and pavements.

Table GDR 9: Mixed Sand/Limestone Fill Measures

Measure	Commentary
Develop a method specification for the filling	A performance specification is not appropriate for compaction control in Mixed Sand/Limestone fill, due to oversized limestone particles and the limitations of test methods. Therefore, a method specification is required. Development of a method specification is discussed in Section GDR7.5. A tentative method specification for Mixed Sand/Limestone Fill preparation is also provided.
Carry out bulk filling	Where fill is required to build up levels, use Approved Fill , placed and compacted in accordance with the developed method specification.
Maintain Construction Records	As performance testing cannot be done, quality assurance records are limited. Therefore, the parameters mentioned in Section GDR7.5.1 must be kept in a comprehensive record of the earthworks done to the developed method specification. The use of the PSP is possible <u>only to check for loose sand zones between limestone particles</u> . High PSP blow counts, where limestone particles are intersected, are meaningless in terms of assessing density of the prepared fill. The primary means of validation of the earthworks is conformance with the developed method specification.
Install sand topping layer	Where a sand topping layer is proposed, this should be done as outlined in Section GDR6.2.5.

These measures do not take into account the specifics of the civil design, including the requirement (if any) for excavatable and/or free draining layers to achieve construction and drainage objectives. The civil design must take precedence and is not specifically considered in this advice.

Soakwells can perform poorly in limestone fill and specific advice may apply to the installation of soakwells in limestone fill areas. If not discussed in our report, please contact us for further advice.

GDR6.3 Guidance on Sites with Cohesive Soils

Cohesive soils (most commonly, “clayey” soils) require careful moisture conditioning to facilitate compaction. We recommend that the moisture content of the material is between optimum moisture content (OMC) and 2% wet of OMC at the time of placement and compaction. We note that compaction to the densities specified in Section GDR7.1 can be difficult to achieve for clayey material when not appropriately moisture conditioned.

Vibratory padfoot rollers are preferred for compacting cohesive fill to promote proper kneading and interlocking of subsequent layers.

Clayey soils will drain poorly when inundated following rain events and result in saturated conditions that may inhibit compaction of the soil. In general, it is preferable to avoid trying to re-work clayey sites within several days of any substantial rainfall.

We recommend that the surfaces of clayey sites are sealed by compaction (i.e., final compaction should be with a smooth drum roller) and graded to drain (to avoid low spots where water can pond and cause softening) prior to any

rain events. Stripping back of softened materials to expose competent natural or compacted clayey soil is required before continuing earthworks.

If difficulties are experienced during compaction due to water, further advice should be sought from a geotechnical engineer.

GDR6.4 Preparation and Testing of Shallow Footings

It is preferable to dig all footing excavations carefully with a flat-edged bucket to minimise the disturbance of underlying foundation soil.

Where the footing base is disturbed, or compaction is required, this must be done using appropriate compaction equipment particular to the task (as evaluated by the contractor) – typically a 'jumping jack', self-propelled plate compactor or an excavator-mounted plate compactor.

All footing bases must be tested to achieve the density requirements of Section GDR7.1. PSP testing of sand foundations is only applicable where the use of the PSP is specifically approved in the report, otherwise all testing is to be done using the NDG.

Sand Topping Layer - Where a sand topping layer is present over a different soil (i.e., clay, limestone etc.), testing of the density of the sand topping layer is only necessary within the thickness of the sand topping layer. Testing does not need to extend into the underlying compacted substrate, which is separately subjected to compaction control.

Mixed Sand/Limestone Fill – Where mixed sand/limestone fill has been installed to a method specification, no compaction control testing is required, however re-compaction of the base must be done as noted above.

In situ limestone – where in situ limestone (weakly or more cemented limestone, with no sand zones or voids) is present at a footing base and no over-excavation has been done (refer to Section GDR6.2.6 regarding over-excavation of footing bases in limestone), then no compaction control testing is required.

Where loose or soft material is encountered, one of the following actions must be taken:

- Over-excavate the loose / soft layer to expose a suitable layer that does meet the required density (Section GDR7.1) and either:
 - Place and compact Approved Fill (relevant to the appropriate preparation measures outlined in Section GDR6.2) to achieve the required density (Section GDR7.1); or
 - Pouring blinding concrete ($f_c > 15$ MPa at 28 days) from the competent layer up to the underside of the footing.

All foundations must be assessed by a competent person prior to blinding.

Measures must be taken to minimise moisture changes in clayey foundation soils at the base of footing excavations. Concrete footings are to be poured soon after excavation to minimise the potential for excessive moisture change. The use of a concrete blinding layer following foundation preparation should be considered.

GDR7 COMPACTION AND MOISTURE CONDITIONING

GDR7.1 Requirements

Any soil within the significant founding zone of structures (buildings, slabs, pavements, etc.) must be suitably moisture conditioned and compacted. These soils must be compacted to the requirements as outlined below.

Table GDR 10: Compaction and Moisture Requirements

Soil Description	Soil Particle Limits	Moisture Requirement	Density Requirement (DDR)	Possible QA/QC Test Methods
Sand	<5% fines <5% gravel <i>Maximum particle size 9.5 mm</i>	MOMC $\pm 2\%$	95% MMDD	PSP NDG
Gravel	<5% fines >50% gravel <i>Maximum particle size 19.0 mm</i>	MOMC $\pm 2\%$	95% MMDD	NDG
Clayey/Silty Gravel	5-35% fines >50% gravel <i>Maximum particle size 19.0 mm</i>	MOMC $\pm 2\%$	95% MMDD	NDG
Sand with fines or gravel	5-35% fines; and/or 5-50% gravel <i>Maximum particle size 19.0 mm</i>	MOMC $\pm 2\%$	95% MMDD	NDG Method Specification
Fine grained soils (Clayey or Silty)	>35% fines <i>Maximum particle size 19.0 mm</i>	MOMC $\pm 2\%$; or SOMC $\pm 2\%^2$	92% MMDD; or 95% SMDD	NDG Method Specification
Oversize/rubbly soil	Any soils with particles >19.0 mm	MOMC $\pm 2\%$	95% MMDD (Or equivalent to)	Method Specification Detailed Assessment Based on Specific Material

- NOTES:**
1. DDR – Dry Density Ratio
MMDD – Modified maximum dry density (AS1289.5.2.1)
MOMC – Modified optimum moisture content (AS1289.5.2.1)
SMDD – Standard maximum dry density (AS1289.5.1.1)
SOMC – Standard optimum moisture content (AS1289.5.1.1)
PSP – Perth Sand Penetrometer
NDG – Nuclear Density Gauge
 2. Preferably OMC to OMC +2%, for ease of compaction and producing a homogenous fill
 3. Test frequencies are specified in Section GDR7.6.

The soil groups and definitions outlined above are generally based on AS1726-2017. Test methods are discussed in subsequent sections.

GDR7.2 Construction Recommendations

Over-excavation and replacement of loose material must be done where the minimum DDR cannot be achieved.

Fill must be placed in horizontal layers of not greater than 300 mm loose thickness. Each layer must be compacted by suitable compaction equipment, and carefully controlled to ensure even compaction over the full area and depth of each layer.

Care will need to be taken if compacting in the vicinity of existing structures, such as the adjacent properties. This is particularly important if vibratory compaction is being carried out.

- Tynan (1973), "Ground Vibration and Damage Effects on Buildings", Australia Road Research Board, Special Report No. 11.

Tynan (1973) provides guidance on the selection of compaction equipment for use adjacent to structures. The distance of influence (i.e., the definition of "vicinity") will vary depending on the size of compaction plant proposed for use. Where there is concern regarding the impact on nearby structures, a dilapidation study should be done.

Care must be taken when compaction is undertaken when the site surface is within 1 m of the groundwater level, as compaction (particularly with vibration) can draw the water up to the surface. In this instance, consideration should be given to:

- Static rolling only;
- Using a pioneering layer (if possible); or
- Dewatering to keep the water at least 1 m below the surface being compacted.

GDR7.3 Nuclear Density Gauge

Where applicable, a nuclear density gauge (NDG) must be used in accordance with AS1289.5.8.1. NDG tests must be done to a depth of 300 mm or as otherwise indicated in the text of the attached report.

GDR7.4 Perth Sand Penetrometer

Where clean sand is used (<5% fines and <5% gravel), a Perth sand penetrometer (PSP) may be used for compaction control in accordance with AS1289.6.3.3. Refer to the report for recommended blow counts correlating to the specified density.

Where the fines or gravel contents of a sand soil exceed the maximum contents noted above, a PSP must not be used exclusively for compaction control. As a minimum, ongoing confirmation testing with an NDG is required. If not specified in our report, please contact us for further advice regarding test frequencies.

If difficulties are experienced recording the required blow counts, a site-specific PSP correlation should be carried out to determine the PSP blow count correlating to a DDR of 95% MMDD. In addition, a particle size distribution (PSD) test should be carried out to verify that the use of a PSP is suitable for the sands being tested. A site-specific PSP correlation must:

- be done on site;
- use the nuclear density gauge (NDG) to determine density at a minimum of 5 points with varying density to a depth of 300 mm below surface;
- include at least 1 point where the dry density ratio is in excess of 95% MMDD;
- use a calibrated PSP to determine the PSP blow count from 150 mm to 450 mm at each NDG test point; and
- be plotted on a chart of PSP blow count vs DDR.

Only where specifically stated as applicable in the report and where the use of the PSP is relevant as noted above, the following values may be taken as deemed to conform to a dry density ratio of 95% MMDD for the relevant sand type.

Table GDR 11: Deemed-to-comply Values for PSP Results in Perth Sands

Depth Interval (mm)	Bassendean	Tamala	Calcareous
0-150	SET	SET	SET
150-450	7	8	12
450-750	9	10	14
750-1050	11	12	16

- NOTES:**
1. Blows per 300 mm interval
 2. Bassendean Sand is typically a white - grey, low-fines quartz sand found on the eastern part of the Perth coastal plain
 3. Tamala / Spearwood sand is typically yellow or orange, low-fines quartz sand found on the western part of the Perth coastal plain
 4. Calcareous sands are typically white or yellow, calcareous sand found in low-lying areas on the western fringe of the Perth coastal plain

5. Values derived from Galt experience on PSP correlations done on sites across Perth for the 150-450 mm interval.

GDR7.5 Method Specifications

GDR7.5.1 General

Where proposed, a method specification should be developed by a geotechnical engineer or similarly qualified person and ratified by us (including a site visit by us). The method specification should be confirmed by the construction of a trial pad or trial area and the compaction methodology should be checked against either:

- density, as assessed using a nuclear density gauge; or
- settlement, as assessed using a dGPS.

Specific advice should be requested for the development of a method specification, taking into consideration the material being compacted.

Method specification compliance should be maintained for all areas on a minimum 20 m grid, with the compliance to include:

- Roller used (weight, style, vibration);
- Water application rate (per lift);
- Layer thickness placed; and
- Number of passes with roller.

GDR7.5.2 Indicative Method Specification – Sand/Limestone Rubble Mix

Where mixed sand/limestone is used as structural fill, a performance specification is not appropriate due to the inaccuracies of standard test methods (NDG/PSP etc.) in this type of material. A method specification can be used instead. The following indicative method specification is provided for evaluation and trial but must be trialled and ratified by us prior to widespread employment on site. The following would be typically adopted:

- Maximum particle size: 250 mm
- Maximum loose layer thickness: 350 mm
- Minimum watering rate: 10 L/m²/100 mm thickness of loose material (e.g. 35 L/m² for a 350 mm thick layer)
- Minimum 8 passes with a vibrating padfoot roller, minimum static weight 10 tonnes.
- The compacted fill must comprise closely packed particles without any significant voids between the larger particles.

GDR7.6 Testing Frequency

After compaction, verify that the required density has been achieved by testing at the base of excavation and through the full depth of any fill, and to a minimum depth of:

- 900 mm where a PSP is used; or
- 300 mm where a NDG is used.

The frequency of testing (when a method specification is not used) should be as follows:

Table GDR 12: Compaction Testing Frequency Requirements

Area	Minimum Testing Frequency	Minimum Tests Per Lot
Proof Compacted Area	1 test per 1,000 m ² (30 m grid)	2
Structural Fill Outside of Building and Pavement Footprints	1 test per 500 m ³ 2 tests per layer <i>Whichever is greater</i>	2
Structural Fill Within Building and Pavement Footprints	1 test per 500 m ³ 4 tests per layer <i>Whichever is greater</i>	4
Spread/Pad Footings	1 test per 9 m ² per footing	1
Strip Footings/Retaining Wall Foundations	Minimum 2 tests At 5 m centres <i>Whichever is greater</i>	2
On-ground slabs, pavements and rafts	Minimum 2 tests At 10 m centres 1 test per 100 m ² <i>Whichever is greater</i>	2

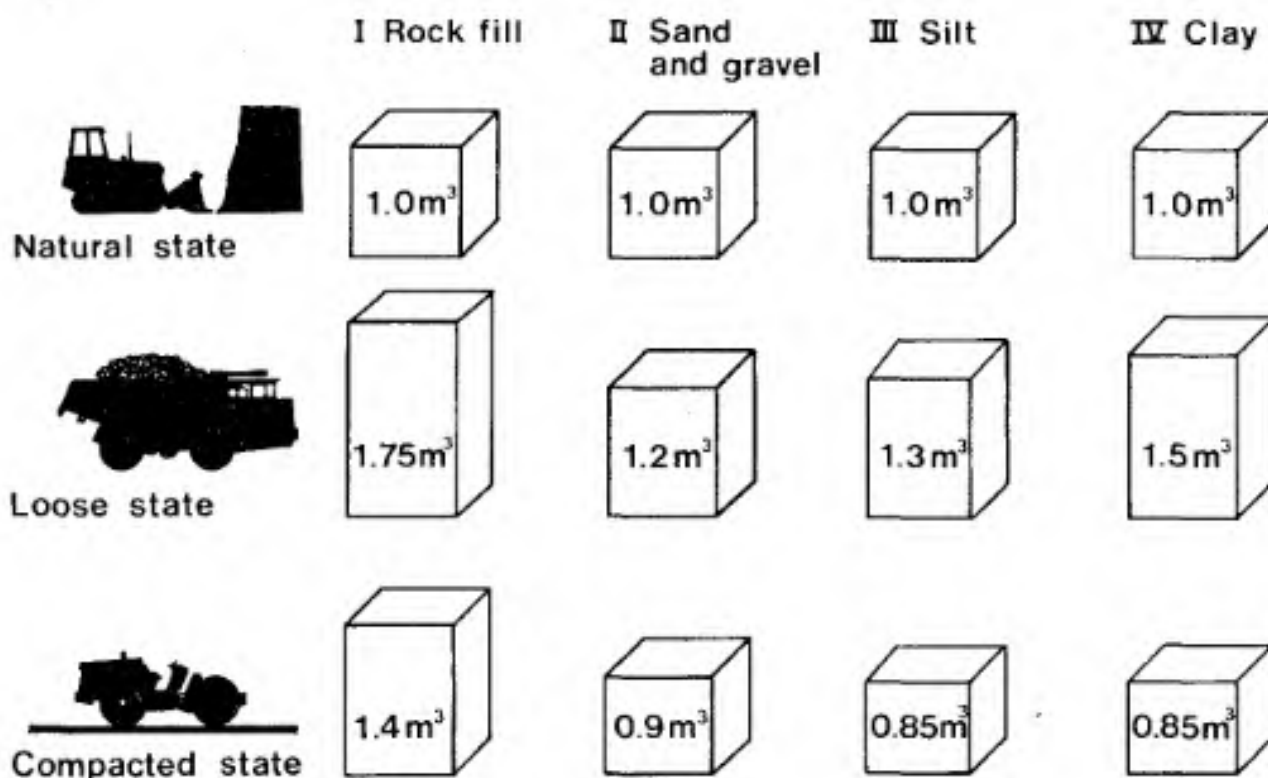
- NOTES:**
1. A 'lot' is defined in the context of this section as a section of earthworks that is undertaken in one operation where the equipment, personnel, materials and methodology are consistent throughout the entire process. This would typically be limited to operations done in one day, but this is not mandatory.
 2. There will frequently be multiple 'lots' in an earthworks process, therefore the number of tests must be adjusted according to the minimum number per lot in this table (where this is more than the frequency specified in 'testing requirements').

GDR7.7 Bulking and Compaction Factors

All soils will "bulk" when excavated to stockpile, and "compact" when placed from stockpile to earthworks layers. Published bulk and compaction factors are presented below for conventional materials, taken from:

- Forssblad, L (1981), "Vibratory Soil and Rock Fill Compaction", Dynapac Maskin AB

Inline Image GDR 3: Volumes of Different Types of Fill Materials in Natural, Loose and Compacted State



These values are indicative only and will vary according to site specific conditions. The values provided here must not be used for commercial volume estimates or settling disputes regarding volumes.

GDR8 APPROVED FILL AND CONFORMANCE TESTING

Imported fill must comply with the material requirements as stated in AS 3798-2007, "Guidelines on Earthworks for Commercial and Residential Developments".

Where doubt exists, a geotechnical engineer must be engaged to inspect and approve the use of potential fill materials.

The following table presents recommended material parameters for standard fill types. This does not take account of availability of materials either on site or in the local area. Refer to the report text for specific advice on fill at the subject site.

Table GDR 13: Standard Fill Recommendations

Soil Description	Application	Soil Particle Limits (%) ³				k_{min} ¹ (m/d)	OC ² (%)	Atterberg Limits		CBR ⁶ (%)	Test Method ⁴
		Fines	Sand	Gravel	Max.			LL (%)	PI (%)		
Permeable Sand	Permeable bulk fill Retaining wall backfill Permeable select fill	≤5	≥90	≤5	9.5	5	≤2	NP	NP	≥12	PSP NDG
General Sand	Bulk fill Select fill (permeability not required)	≤5	≥90	≤5	9.5	N/A	≤2	NP	NP	≥12	PSP NDG
Silty Sand	Bulk fill Select fill	≤35	≥55	≤10	9.5	N/A	≤2	<35	<11	≥12	NDG
Clayey Sand	Bulk fill Select fill	≤35	≥55	≤10	9.5	N/A	≤2	<40	N/A	≥12	NDG
Mixed Sand/Limestone	Bulk fill (permeability not required)	≤5	≥20	≤80	250	N/A	≤2	NP	NP	N/A	NDG Method
Blue Metal Gravel ⁸	Retaining wall backfill Drainage trench backfill	≤3	≤5	≥90	37.5	5	≤1	NP	NP	N/A	NDG
Clay ⁷	Reinstatement of localised excavations in clay Bulk fill	≥12	Varies	≤30	19	N/A	≤2	Varies			NDG

- NOTES:**
- k_{min} – minimum saturated hydraulic conductivity (AS1289.6.7.1, remoulded to minimum DDR 100% MMDD).
 - OC – organic content (Walkley-Black method recommended, AS1289.4.1.1 – not loss on ignition methods)
 - % by mass.
 - Test method indicates possible compaction control methods for this material.
PSP – Perth sand penetrometer (AS1289.6.3.3). Where a PSP is used, a site-specific correlation must be done unless otherwise noted in the report.
NDG – Nuclear density gauge (AS1289.5.8.1)
Method – method specification
 - Atterberg Limits: LL – liquid limit PI – plasticity index NP – non-plastic
 - CBR: California bearing ratio (for sand - remoulded to DDR 95% MMDD @ OMC, 4.5 kg surcharge). CBR values may be changed depending on the design pavement requirements.
 - “Clay” fill type is included for broad reference only and to illustrate preferred applications, particle size limits and recommended test method. Specific discussion on the use of clayey fills is included in the report text if applicable. Atterberg limit and CBR testing of clayey fills may be required and advice must be sought from us if not stated in the report.
 - “Blue metal” gravel refers to single sized, crushed, washed igneous rock gravel used for drainage purposes.
 - In the absence of specific test frequencies by the civil designer, the testing shown in Table GDR 14 must be done (highlights in Table GDR 13 show where the test is required).

Table GDR 14: Conformance Testing Frequency Requirements

Parameter	Frequency (m ³)	Minimum Tests per Source	AS1289 Reference
Particle size distribution	5,000	1	3.6.1
Hydraulic conductivity (permeability)	10,000	2	6.7.1
Organic content	5,000	1	4.1.1
Atterberg limits	5,000	1	3.1.1, 3.2.1, 3.3.1
CBR	10,000	2	6.1.1

- NOTES:**
1. Frequency is for the nominal number of cubic metres of compacted fill.
 2. Unless stated otherwise in the report text, the conformance testing must also be carried out on site-derived materials to confirm suitability.

GDR9 SHALLOW FOUNDATIONS

GDR9.1 Design

Footings and slabs may be designed in accordance with the assigned site classification in accordance with AS2870-2011. We note that AS2870-2011 is limited to single and double storey residential and commercial developments and may not be strictly applicable.

Where the report provides tables for shallow footing design, custom footings may be designed by the structural engineer using the data provided therein.

GDR9.2 Interpretation of Provided Values

BEARING PRESSURES

All settlement and bearing pressures estimates are provided on the assumption that the site preparation requirements outlined in the report are completed below all structures plus a minimum distance of 1 m beyond the outside edge of any footing or slab. It is essential that the soil below all foundations is appropriately prepared as outlined and meets the relevant compaction requirements.

Allowable bearing pressures for footings of intermediate plan dimensions (to any tabulated) can be interpolated. Footings that have a plan dimension either smaller or larger than those presented in the report will need to be considered individually along with other embedment depths.

Allowable bearing pressures, where provided, are considered to be the upper limit for shallow footings to limit total and differential settlements. Footings carrying eccentric loading, such as below retaining walls, must be assessed separately.

SETTLEMENTS

The reporting of settlements to any precision level is not intended to imply a high accuracy of settlement prediction. Settlements as reported should be considered 'order of magnitude'.

Estimated settlements represent vertical downwards movement due to loading and do not take into account potential additional movement associated with the characteristic surface movement of the soil (which must be taken in addition to these settlements from loading, refer Section GDR5). The site classification is discussed in the report.

The actual settlement of any proposed structure will depend upon a number of factors including the applied pressures, footing size and base preparation. The estimated settlement(s) provided in this report are for the working bearing pressures as indicated. Differential settlements are likely between footings of similar sizes, loads and elevations (as

stated in the report text). A proportion of the settlement is expected to occur during construction (i.e., during initial loading).

The provided settlement estimates (unless otherwise stated) do not include interaction effects from footings founded near other footings (i.e., groups of footings). Interaction effects will need to be considered if the spacing between adjacent footings is smaller than the dimension of the footings (i.e., the centre-to-centre spacing between footings is less than twice the width of the footing). This could act to double provided settlements, dependent on the footing configuration. Where an assessment of footing groups is required, a more detailed numerical or finite-element modelling analysis would need to be undertaken.

CREEP AND CONSOLIDATION

Creep settlement is an irreversible component of long-term soil settlement caused by sustained vertical stress. Consolidation is a time-dependent irreversible compression in a soil layer caused by a reduction in pore pressure between soil particles. Both creep and consolidation can occur in natural materials as a result of earthworks or the placement of loads on to soil layers. The settlements as presented for short-term loading do not include consideration for creep and consolidation settlements unless specifically stated.

GDR9.3 Raft Foundations

Where moduli of subgrade reactions are provided for the design of raft foundations, we highlight that these are an estimate of the elastic reaction of the soil. The values are provided based on an expected load and loaded area size. Soils are typically non-linear in their response and will have different stiffnesses at different levels of strain and load repetitions. This is due to the physical interaction of soil particles under different levels of stress.

The possibility of a non-linear response must be considered by the designer of any raft foundation.

GDR10 PILED FOUNDATIONS

Piles must be designed and tested in accordance with AS2159-2009, "Piling – Design and Installation". We use the following interpretation/design methods to provide pile design parameters:

- Franki Africa Pty Ltd (2008) "A Guide to Practical Geotechnical Engineering in South Africa". 4th ed.
- AFNOR (2012) "NF P 94-262 – Justification des ouvrages géo-techniques, Normes d'application nationale de l'Eurocode 7", Afnor, Paris, July 2012.
- Lehane, B. (2017) "CPT-Based Design of Foundations". E.H Davis Memorial Lecture, Australian Geomechanics Vol 54. No. 4.
- Lehane, B. et al. (2020) "A New 'Unified' CPT-Based Axial Pile Capacity Design for Drivel Piles in Sand". Proceedings of the Fourth International Symposium on Frontiers of Offshore Geotechnics.
- Doan., Lehane, B. (2021) "CPT-Based Design Method for Axial Capacities of Drilled Shafts and Cast-in-place Piles." American Society of Civil Engineers (ASCE), Journal of Geotechnical and Geoenvironmental Engineering.

The pile designer must:

- consider the possible variation in subsurface conditions at each pile location;
- consider any pile group effects based on the final piling configuration;
- assume that the unit shaft resistance in tension is less than 80% of the unit shaft resistance in compression to account for Poisson's effect in sand;
- ignore pile resistance in the surficial 0.5 m or 1 x pile diameter (whichever is greater), if relevant;

- consider the impact of weak layers underlying stiffer layers (or vice versa) on end bearing capacity; and
- reduce the pile capacity in tension to no greater than 0.8 of the pile capacity in compression.

The piling contractor must:

- make their own assessment on the suitability of their equipment to install any piles at the subject site; and
- carry out or appoint a suitably experienced contractor to test the piles in accordance with AS2159.

Where dynamic or static testing of the piles does not occur, we consider that a design geotechnical reduction factor (ϕ_g) of 0.4 is applicable for the pile design. If testing of the piles is proposed by the piling contractor, a higher ϕ_g could be adopted.

Unless otherwise stated, providing pile design parameters does not specifically indicate the driveability of any piles into soil units.

A separate driveability study may be required and must be considered by the pile designer and installer. The given pile design parameters must not be used for driveability assessments as these parameters are likely to be un-conservative.

GDR11 EARTH RETAINING STRUCTURES

GDR11.1 General

Retaining structures may be designed in accordance with AS4678 (2002) "Earth Retaining Structures". Unless otherwise specifically stated, we recommend that all retaining walls are backfilled with free-draining soil (Permeable Sand or Blue Metal Gravel as defined in Section GDR8).

Where the cohesive soil is used as retaining wall backfill, a suitable, permanent drainage system must be placed behind the wall such that a build-up of pore pressure is prevented. A separator geotextile (Bidim A24, or similar, or heavier) must be used between the interface of any granular backfill and the cohesive soil.

Where drainage is not provided, the retaining wall must be designed to accommodate water pressure behind the wall (10 kPa per metre height).

GDR11.2 Earth Pressure Coefficients and Strength Parameters

Where earth pressure coefficients are provided for retaining walls, the wall designer must make an independent assessment of the parameters appropriate to the construction method to be used, including alternative values of wall friction. Unless otherwise stated, we have assumed a horizontal ground surface behind and in front of the retaining wall for provided parameters.

GDR11.2.1 Cohesionless Soils

Where cross-referenced for suitability in the report, the following parameters may be adopted for design of earth retaining structures in cohesionless soils (sand and gravel).

Table GDR 15: Retaining Wall Geotechnical Parameters (Cohesionless Soils)

Density	γ (kN/m ³)	ϕ' (°)	k_0	Wall Friction=0		Wall Friction=0.5 ϕ		Wall Friction=0.67 ϕ	
				k_a	k_p	k_a	k_p	k_a	k_p
Very Loose	17	30	0.44	0.33	3.00	0.29	4.81	0.28	5.74
Loose	17	32	0.42	0.31	3.25	0.27	5.55	0.26	6.83
Medium Dense	18	34	0.39	0.28	3.54	0.25	6.47	0.23	8.26
Dense	19	36	0.36	0.26	3.85	0.22	7.63	0.21	10.18
Very Dense (1)	19	38	0.34	0.24	4.20	0.21	9.11	0.20	12.85
Very Dense (2)	19	40	0.31	0.22	4.60	0.19	11.06	0.18	16.73

- NOTES:**
- Earth pressure coefficients are provided in this table for conditions of zero friction between the wall and the soil and with wall friction of 0.5 ϕ' or 0.67 ϕ' .
 - A horizontal ground surface behind and in front of the wall has been assumed.
 - The retaining wall designer should make an independent assessment of the parameters appropriate to the construction method to be used, including alternative values of wall friction.
 - γ – bulk unit weight
 ϕ' – effective friction angle
 k_a – coefficient of active earth pressure (Coulomb – AS4678-2002, Appendix E)
 k_p – coefficient of passive earth pressure (Coulomb – AS4678-2002, Appendix E)
 k_0 – coefficient of at-rest earth pressure (Jaky)
 - Maximum fines content 12% for applicability of this table for design purposes.
 - Unit weights based on Table D1 of AS4678-2002, for moist bulk weight.
 - Friction angle based on Equation D1 and Table D2 of AS4678-2002, based on rounded, moderately graded siliceous sand.

GDR11.2.2 Cohesive Soils

Where cohesive soils (i.e. clayey or silty soils) are proposed for backfill, geotechnical design parameters may be provided in the form of effective strength and undrained strength parameters. We note that:

- Undrained strength parameters should be used for analysis of short-term stability, or stability under sudden loading of cohesive soils.
- The effective strength parameters should be used for analysis of free-draining soils and the long-term stability of cohesive soils.

Table GDR 16: Retaining Wall Geotechnical Design Parameters (Cohesive Soils – Undrained)

Consistency	γ_b (kN/m ³)	c_u (kPa)
Soft	17	12
Firm	18	25
Stiff	19	50
Very Stiff	20	100
Hard	20	200

- NOTES:**
- γ_b – bulk unit weight
 c_u – undrained cohesion
 $\phi_u = 0^\circ$ (undrained friction angle)
 - Unit weights based on Table D1 of AS4678-2002
 - Undrained cohesion based on lower end of shear strengths as define in AS1726-2017, Table 11

Table GDR 17: Retaining Wall Geotechnical Design Parameters (Cohesive Soils – Drained)

Fines Content	PI (%)	γ_b (kN/m ³)	ϕ' (°)	c' (kPa) ⁵
12-35%	All	19	32	0
>35%	10	20	30	0 – 5
>35%	20	20	26	0 – 5
>35%	30	20	23	0 – 5
>35%	40	20	21	0 – 5

- NOTES:**
1. γ_b – bulk unit weight
 c' – drained cohesion
 ϕ' – effective friction angle
PI – plasticity index
 2. Unit weights based on Table D1 of AS4678-2002, assuming generally stiff to hard overconsolidated soils.
 3. For fines contents <35% (silty sand and clayey sand), strength parameters based on:
 - Lehan, B. et al (2007) "A Laboratory Investigation of the Upper Horizons of the Perth/Guildford Formation in Perth CBD", Australian Geomechanics Vol 42. No. 3.
 4. For fines content >35% (sandy clay), strength parameters based on:
 - CIVL5503 course notes (2004), "Underground Construction", University of Western Australia
 5. $c' = 0$ recommended for long-term design. Table D4 of AS4678 suggests c' up to 5 kPa for 'poor' fine grained soils and 10 kPa for 'average' fine-grained soils. The use of c' for design is subject to the designer's judgement but recommended by us only for temporary works.

Per AS4678-2002 Appendix E, horizontal earth pressures for frictional-cohesive soils may be calculated in accordance with the Rankine-Bell design model (illustrated in Figure E2 of AS4678). The earth pressures are as follows (Z = depth, all other terms have the meanings given in the above tables):

- Active: $p_a = \gamma Z \tan^2 \left(45 - \frac{\phi}{2} \right) - 2c \tan \left(45 - \frac{\phi}{2} \right)$
- Passive: $p_p = \gamma Z \tan^2 \left(45 + \frac{\phi}{2} \right) + 2c \tan \left(45 + \frac{\phi}{2} \right)$

GDR11.3 Design and Construction Considerations

Compaction plant can augment the lateral earth pressure acting on retaining walls. Hand operated compaction equipment is recommended within 2 m of any retaining walls to minimise compaction pressures.

Retaining walls can move and rotate under imposed soil loading resulting in settlement behind the wall. This must be considered in the design and during construction of the retaining walls in order that adjacent infrastructure is not adversely affected.

It is important to note that some ground movement will occur behind any soil retaining system, including gravity retaining walls.

GDR12 EXCAVATIONS, BATTERS AND SLOPES

GDR12.1 Excavatability

Our assessment of the excavatability of rock is based on a combination of:

- Our experience on earthworks and construction projects across Australia; and
- Figure 10 of the revised graphical method of assessing excavatability of rock by:
- Pettifer, G.S. & Fookes, P.G., "A revision of the graphical method for assessing the excavatability of rock", Quarterly Journal of Engineering Geology, 27, pp145-164, 1994.

GDR12.2 Safety

All excavations must be carried out in accordance with:

- Commission for Occupational Safety and Health (2022). "Excavation: Code of Practice", Department of Mines, Industry Regulation and Safety, 89pp, Perth.

Excavations in cohesionless soils are particularly prone to instability unless support is provided. Care must be exercised in such excavations and appropriate safety measures adopted where necessary, particularly in the vicinity of existing buildings, structures and infrastructure.

The toe of any batter must be at least 500 mm above groundwater (including perched groundwater).

Unless a specific slope stability assessment or retention design has been done, the toe of any excavation should not encroach within a line of 1V:3H to any nearby footings, pavements or other settlement-sensitive structures.

Surcharges (such as structures, plant and soil stockpiles) must not be placed at or close to the crest of unsupported excavations, without a specific slope stability assessment.

A geotechnical engineer must be consulted where there is any doubt regarding the stability or safety of unsupported excavations.

GDR12.3 Batters

Temporary batter slopes provided in the report are subject to the following conditions, unless otherwise stated:

- The maximum slope height is 2 m without specific advice and slope stability analysis.
- The groundwater level for the duration of the excavation must be at least 500 mm below the toe of the slope.
- No surcharges are present in the vicinity of the slope (i.e. must be outside a line of 1V:3H from the toe of the slope).

Unless noted specifically in the report, the following batters may be adopted (maximum height: 2 m):

Table GDR 18: Default Batter Angles

Situation	Material	Batter
Temporary	Cohesionless Soils (Sand/Gravel)	1V:2H
Temporary	Cohesive Soils – Soft	1V:2H
Temporary	Cohesive Soils – Firm, Stiff, Very Stiff or Hard	1V:1H
Temporary	Limestone – Variably Cemented	1V:1H
Temporary	Limestone – Well Cemented	1V:0.5H
Permanent	All Soils	1V:3H
Permanent	Limestone – Variably Cemented	1V:2H
Permanent	Limestone – Well Cemented	1V:1H

Where specified batters cannot be accommodated in the vicinity of existing footings, roads and services, temporary or permanent lateral support will be required.

Specific advice is required for batters higher than 2 m.

Erosion control must be considered for permanent slopes.

Rock slopes must be inspected, and all loose cobbles / boulders removed. Permanent rock slopes may require dentition works or possibly rock catch drains.

GDR12.4 Grouting

Permeation or jet grouting involves injecting a microfine cement into soil to form a grouted soil block (soilcrete) to support excavation and structures. Grouting is typically only effective where the soil has the capacity to “take” the grout and form a uniformly cemented soil mass. Permeation grouting is generally limited to relatively permeable, coarse-grained cohesionless soils (sands and gravels with <5% fines).

If grouting is proposed, we recommend the following:

- Grouting must be carried out by a suitably experienced contractor.
- Only microfine cement grout should be used (not GP or coarse cement blends) to ensure adequate penetration into the soil matrix.
- Grouting should be done on a grid of not greater than 300 m.
- Application rates must be discussed with the contractor.
- The grouted soil mass must have intimate contact with any structures it is intended to support.
- The contractor must satisfy themselves that the proposed grouting can be installed with their equipment and into the subsurface conditions encountered at the site, considering possible obstructions, groundwater, cemented layers, loose sands etc.
- Testing of the grouted soil mass must be done to ensure that the grout has adequately permeated through the soil matrix. This can be done by drilling into the soil mass to ensure the cementation is continuous.

Grouting is most effective on permeable, relatively loose natural sand. Where historical filling or other ground disturbances have occurred, the grouting process can be less effective due to the tendency of grout (or other liquids) to follow more permeable paths / zones through the disturbed soil.

GDR13 STORMWATER DISPOSAL AND DRAINAGE DESIGN

GDR13.1 Groundwater Separation – Controlled Groundwater

These recommendations ONLY apply to where regional controls on groundwater (primarily: subsoil drainage, but also surficial ‘main drains’) exist, i.e. only to areas where groundwater is actively controlled.

The following reference:

- IPWEA (2016), “Specification: Separation Distances for Groundwater Controlled Urban Development”, Institute of Public Works Engineering Australasia

recommends the following separation distances from drainage infrastructure to groundwater:

- Underground infiltration systems: 0 mm from the 50% AEP (annual exceedance probability) phreatic surface.
- Surface infiltration systems (vegetated): 300 mm from the 50% AEP phreatic surface.

The above IPWEA reference also states that performance measures for underground infiltration systems are to have a: *demonstration of acceptable volumetric capacity when groundwater is elevated above base of system and that the groundwater recedes below the invert of the system during mosquito breeding seasons (grated or partially open systems).*

GDR13.2 Groundwater Separation – Uncontrolled Groundwater

These recommendations apply where regional controls on groundwater levels are not present. For infiltration into soakwells and soakage basins to be the full theoretical value, an adequate separation to groundwater must be achieved, because otherwise performance is hindered by inadequate separation to groundwater or partial submergence of the infiltrative element.

We recommend a minimum separation of 500 mm from the underside of infiltrative elements to maximum groundwater level.

- To average annual maximum groundwater level (AAMGL), where this has been defined for the site; or
- To historical maximum groundwater level, where this has been defined to the site.

GDR13.3 Design Hydraulic Conductivity Values

Where provided, the values of hydraulic conductivity (k) should be considered the maximum/upper limit design values. As discussed in Section GDR3.7, the inverse auger hole test is an unsaturated field test carried out above the groundwater table and, as such, presents the best-case conditions for drainage.

For soak wells in sand, we provide the design value taking into consideration the variability in materials and reduced permeability as a result of:

- Densification of sand during site preparation works; and
- Natural variation in sands.

Design k_{unsat} values provided for soak wells are only appropriate for the design of unsaturated soils where the base of disposal area is at least 500 mm above groundwater and 500 mm above any impermeable layer.

Where design values of k_{unsat} have been provided, clogging of the base of the soakwell / drainage basin has not been considered. Clogging will need to be controlled with maintenance over the life of the soakwell / drainage basin.

For the design of subsoil drains or modelling of saturated soil performance, a k_{sat} value must be given (in the report text) or assessed by laboratory testing (or a combination of field and laboratory testing). Unless specifically stated, k_{unsat} values presented in our report are for unsaturated conditions and intended for design of stormwater disposal elements above groundwater. If no k_{sat} value has been provided, do not use the provided k_{unsat} value for saturated drainage design. Please contact us for further advice.

For saturated or semi-saturated sands, the hydraulic conductivity must be assessed by testing of representative soil samples at a NATA accredited laboratory to determine:

- The modified maximum dry density (MMDD); and
- The constant-head permeability (AS1289.6.7.1) on a sample remoulded to at least 5% greater than the proposed specification density (i.e., sample should be remoulded to 100% MMDD if the earthworks specification requires a density ratio of 95% MMDD).

For saturated or semi-saturated clayey or silty soils, the hydraulic conductivity must be assessed by testing of representative soil samples at a NATA accredited laboratory to determine:

- The standard maximum dry density (SMDD); and
- The falling-head permeability (AS1289.6.7.2) on a sample remoulded to at least 3% greater than the proposed specification density (i.e., sample should be remoulded to 101% SMDD if the earthworks specification requires a density ratio of 98% SMDD).

GDR13.4 Soakwells

In uncontrolled groundwater environments, the base of any soakwell must be the higher of:

- At least 500 mm above the average annual maximum groundwater level (AAMGL).
- At least 500 mm above any low permeability/impermeable layers (clay, rock or otherwise).

In controlled groundwater environments (refer to Section GDR13.1), the base of any soakwell may be 0 mm above the controlled groundwater level at the location of the soakwell (as determined by the civil engineer).

Soak wells must be placed outside a line of 1V:2H extending below the edge of the nearest footing, subject to local council regulations. Discharge from soak wells has been known to promote densification of loose sandy soils, leading to settlements of footings and slabs. Soak wells should be carefully wrapped with geotextile to prevent migration of sand and fines into the soak well.

Where soak wells are proposed to dispose of water within a line of 1V:2H from any basement walls or similar, the walls must be waterproofed to prevent seepage or damp within the basement wall.

In potentially karstic terrain or areas of potentially collapsible soils, soakwells should typically be located 10 m from the nearest footing, slab or pavement.

GDR13.5 Design Groundwater Elevation

Where applicable, a recommended design groundwater elevation will be provided in the report and will be identified as such.

In the absence of a specific statement on design groundwater elevation, **do not assume** that:

- Absence of comments about groundwater indicates an absence of groundwater (in particular, sites that are dry in the dry season to the investigated depth may well become waterlogged in the rainy season).
- Where groundwater depths/levels are noted, that these are fixed (groundwater fluctuations occur over the course of the year and between wetter and drier years).

Where groundwater elevations are likely to be critical for a development (particularly where large-scale subdivision or large developments are proposed with substantial channelling of stormwater into on-site disposal by infiltration), a site-specific hydrology study is likely to be required to confirm design groundwater elevations.

GDR14 DRAINAGE CONTROL

In addition to the site preparation measures outlined for cohesive soils (refer Section GDR6.2.4), careful control of surface water and stormwater is essential to minimise the likelihood of cohesive soils decreasing in strength and affecting the installed infrastructure. These measures include:

- The ground surface of clayey soils should be graded to drain any seepage away from structures and prevent standing water over the cohesive soils. A grade of at least 1% is recommended.
- Pavements should be sealed to minimise water ingress.
- Stormwater disposal swales should be located at least 10 m away from buildings, retaining walls and pavements.
- Runoff from hardstandings and pavements must either be collected and discharged via pipes into discrete locations (via swales or soakage basins) at least 10 m away from structures and pavements or, alternatively, discharged over a wide area, but not allowed to collect and discharge into concentrated areas, particularly near structures and pavements.

- Spoon drains should be used to collect water at the crest of slopes to capture surface runoff and direct it away from running directly down slopes or seeping into the ground behind slopes.

These measures are general in nature only and do not take into account the civil design objectives, which must be addressed separately by the civil designer.

GDR15 DEWATERING

Dewatering may be required for excavations and construction below groundwater or perched groundwater tables. Common dewatering methods are summarised below:

Table GDR 19: Dewatering Recommendations

Material	Recommended Methods
Sandy Soils	Spears Deep Well Point
Impermeable Clay	Sump Pumping

Dewatering spears are typically suitable for small scale excavations below groundwater, with a typical recommendation for spears to be installed at 1 m below the base of any excavation. Dewatering spears may not be suitable where there are impermeable/cemented/strong transition layers, i.e., it may not be possible to extract water near an impermeable layer (rock/clay), or the spear may not be readily driven through a hard clay/cemented layer (i.e., coffee rock).

Sump pumping can be done by grading a clayey excavation to drain (i.e., by using spoon drains), and excavating a sump in the excavation. A sump can typically be backfilled with a blue metal gravel, with a pump wrapped in a geofabric (i.e., Bidim A14 or similar), with disposal of water away from the excavation.

Deep well point dewatering is typically suitable for larger excavations, where there are transitional layers or where the aquifer is confined. It may not be suitable where there are impermeable layers within the profile. It involves the installation of a deep filtered well to a depth required to draw down the groundwater level at the entire site. A deep well dewatering system must be designed by a suitable designer to provide design flow rates, draw down depths etc.

GDR16 PAVEMENT SUBGRADES

Unless otherwise specified, the provided subgrade California bearing ratio (CBR) is not a pavement design, but an assessment of the subgrade as an input into any required pavement designs.

Provided design values are based on the assumption that the relevant site preparation measures are completed for all pavement subgrades, including the use of appropriate approved fill and adequate compaction. We highlight that specific requirements such as those outlined by Main Roads WA (MRWA) or the local council in their construction specifications may have different requirements.

The provided design value is based on laboratory testing (where done), local experience, and the advice as outlined in:

- Main Roads Western Australia (2013). "Engineering Road Note 9 – Procedure for the Design of Road Pavements". Western Australia Supplement to the Austroads Guide to Pavement Technology Part 2: Pavement Structural Design, East Perth.

Where the subgrade differs from that described in the text, the subgrade CBR must be confirmed.

The performance of any pavement is highly dependent on the surface and subsurface drainage provided (also considering factors like capillary rise from seasonally high groundwater tables). Adequate drainage must be provided to any pavements, and capillary rise must be considered by the designer.

GDR17 SOIL CORROSIVITY AND AGGRESSIVITY

The relevant exposure classifications for concrete and steel piles in soils based on the exposure conditions are presented in Table GDR 20 and Table GDR 21 respectively.

The relevant exposure classifications for concrete in sulfate soils based on the exposure conditions are presented in Table GDR 22.

Table GDR 20: Exposure Classification for Concrete Piles in Soil

Exposure Conditions				Exposure Classification	
Sulfates (expressed as SO ₄) ¹		pH	Chlorides in Groundwater (ppm)	Soil Conditions A ²	Soil Conditions B ³
In Soil (ppm)	In Groundwater (ppm)				
< 5,000	< 1,000	> 5.5	<6000	Mild	Non-aggressive
5,000 – 10,000	1,000 – 3,000	4.5 – 5.5	6,000-12,000	Moderate	Mild
10, 000 – 20,000	3,000 – 10,000	4 – 4.5	12,000-30,000	Severe	Moderate
> 20,000	> 10,000	< 4	>30,000	Very Severe	Severe

- NOTES:**
1. Approximately 100 ppm SO₄ = 80 ppm SO₃
 2. Soil Conditions A – high permeability soils (e.g. sands and gravels) which are in groundwater
 3. Soil Conditions B – low permeability soils (e.g. silts and clays) or all soils above groundwater
 4. Table reproduced from Table 6.4.2(C) of AS2159-2009

Table GDR 21: Exposure Classification for Steel Piles in Soil

pH	Chlorides		Resistivity (ohm.cm)	Exposure Classification	
	In Soil (ppm)	In Water (ppm)		Soil Conditions A ²	Soil Conditions B ³
> 5	< 5,000	< 1,000	> 5,000	Non-aggressive	Non-aggressive
4–5	5,000-20,000	1,000–10,000	2,000 – 5,000	Mildly aggressive	Non-aggressive
3–4	20,000-50,000	10,000–20,000	1,000 – 2,000	Moderately aggressive	Mildly aggressive
< 3	> 50,000	> 20,000	< 1,000	Severely aggressive	Moderately aggressive

- NOTES:**
1. 1 ppm (parts per million) is equivalent to 1 mg/kg
 2. Soil Conditions A – high permeability soils (e.g. sands and gravels) which are in groundwater
 3. Soil Conditions B – low permeability soils (e.g. silts and clays) or all soils above groundwater
 4. Table reproduced from Table 6.5.2(C) of AS2159-2009

Table GDR 22: Exposure Classification for Concrete in Sulfate Soils

Exposure Conditions			Exposure Classification	
Sulfates (expressed as SO ₄) ¹		pH	Soil Conditions A ²	Soil Conditions B ³
In Soil (ppm)	In Groundwater (ppm)			
< 5,000	< 1,000	> 5.5	Mild	Non-aggressive
5,000 – 10,000	1,000 – 3,000	4.5 – 5.5	Moderate	Mild
10, 000 – 20,000	3,000 – 10,000	4 – 4.5	Severe	Moderate
> 20,000	> 10,000	< 4	Very Severe	Severe

- NOTES:**
1. Approximately 100 ppm SO₄ = 80 ppm SO₃
 2. Soil Conditions A – high permeability soils (e.g. sands and gravels) which are in groundwater
 3. Soil Conditions B – low permeability soils (e.g. silts and clays) or all soils above groundwater
 4. For disturbed soils, the assumption of soil A conditions where accelerated corrosion is possible should be considered.
 5. Table reproduced from Table 4.8.1 of AS3600-2018

GDR18 LIQUEFACTION

Soil liquefaction can occur when loose, granular, Holocene age material below the groundwater table is subjected to a seismic event (typically within 15 m of the ground surface). This can cause a loss of strength and result in vertical and lateral movements of the site surface.

Where a liquefaction analysis is carried out and outlined in the report, this has been done in accordance with consideration to the design earthquake details as presented in AS1170.4-2007:

- The hazard factor is taken from Figure 3.2 (C) and Table 3.2. The Hazard Factor (Z) for Western Australia represents the 1 in 500-year annual probability of exceedance of ground motions measured in gravity (g).
- The probability factor (k_p) is taken from Table 3.1.

Unless otherwise stated, an earthquake magnitude of 7.5 for the south-west of WA is based on research by:

- Dhu T., Sinadinovski C., Edwards M., Robinson D., Jones T., Jones A. (2004) "Earthquake Risk Assessment for Perth, Western Australia". 13th World Conference on Earthquake Engineering, Vancouver, B.C., Canada. Paper No. 2748.

GDR19 EXPECTATIONS OF THE REPORT

The following sections have been prepared to clarify what is and is not provided in your report. It is intended to inform you of what your realistic expectations of this report should be and how to manage your risks associated with the conditions on site.

Geotechnical engineering and environmental science are less exact than other engineering and scientific disciplines. We include this information to help you understand where our responsibilities begin and end. You should read and understand this information. Please contact us if you do not understand the report or this explanation. We have extensive experience in a wide variety of projects and we can help you to manage your risk.

GDR20 THIS REPORT RELATES TO PROJECT-SPECIFIC CONDITIONS

This report was developed for a unique set of project-specific conditions to meet the needs of the nominated client. It took into account the following:

- the project objectives as we understood them and as described in this report;
- the specific site mentioned in this report; and
- the current and proposed development at the site.

It should not be used for any purpose other than that indicated in the report. You should not rely on this report if any of the following conditions apply:

- the report was not written for you;
- the report was not written for the site specific to your development;
- the report was not written for your project (including a development at the correct site but other than that listed in the report); or
- the report was written before significant changes occurred at the site (such as a development or a change in ground conditions).

You should always inform us of changes in the proposed project (including minor changes) and request an assessment of their impact.

Where we are not informed of developments relevant to your report, we cannot be held responsible or liable for problems that may arise as a consequence.

Where design is to be carried out by others using information provided by us, we recommend that we be involved in the design process by being engaged for consultation with other members of the project team. Furthermore, we recommend that we be able to review work produced by other members of the project team that relies on information provided in our report.

GDR21 DATA PROVIDED BY THIRD PARTIES

Where data is provided by third parties, it will be identified as such in our reports. We necessarily rely on the completeness and accuracy of data provided by third parties in order to draw conclusions presented in our reports. We are not responsible for omissions, incomplete or inaccurate data associated with third party data, including where we have been requested to provide advice in relation to field investigation data provided by third parties.

GDR22 SOIL LOGS

Our reports often include logs of intrusive and non-intrusive investigation techniques prepared by Galt. These logs are based on our interpretation of field data and laboratory results. The logs should only be read in conjunction with the report they were issued with and should not be re-drawn for inclusion in other documents not prepared by us.

GDR23 THIRD PARTY RELIANCE

We have prepared this report for use by the client. This report must be regarded as confidential to the client and the client's professional advisors. We do not accept any responsibility for contents of this document from any party other than the nominated client. We take no responsibility for any damages suffered by a third party because of any decisions or actions they may make based on this report. Any reliance or decisions made by a third party based on this report are the responsibility of the third party and not of us.

GDR24 CHANGE IN SUBSURFACE CONDITIONS

The recommendations in this report are based on the ground conditions that existed at the time when the study was undertaken. Changes in ground conditions can occur in numerous ways including anthropogenic events (such as construction or contaminating activities on or adjacent to the site) or natural events (such as floods, groundwater fluctuations or earthquakes). We should be consulted prior to use of this report so that we can comment on its reliability. It is important to note that where ground conditions have changed, additional sampling, testing or analysis may be required to fully assess the changed conditions.

GDR25 SUBSURFACE CONDITIONS DURING CONSTRUCTION

Practical constraints mean that we cannot know every minute detail about the subsurface conditions at a particular site. We use professional judgement to form an opinion about the subsurface conditions at the site. Some variation to our evaluated conditions is likely and significant variation is possible. Accordingly, our report should not be considered as final as it is developed from professional judgement and opinion.

The most effective means of dealing with unanticipated ground conditions is to engage us for construction support. We can only finalise our recommendations by observing actual subsurface conditions encountered during construction. We cannot accept liability for a report's recommendations if we cannot observe construction.

GDR26 ENVIRONMENTAL AND GEOTECHNICAL ISSUES

Unless specifically mentioned otherwise in our report, environmental considerations are not addressed in geotechnical reports. Similarly, geotechnical issues are not addressed in environmental reports. The investigation techniques used for geotechnical investigations can differ from those used for environmental investigations. It is the client's responsibility to satisfy themselves that geotechnical and environmental considerations have been taken into account for the site.

Geotechnical advice presented in a Galt Environmental report has been provided by Galt Geotechnics under a sub-contract agreement. Similarly, environmental advice presented in a Galt Geotechnics report has been provided by Galt Environmental under a sub-contract agreement.

Unless specifically noted otherwise, no parties shall draw any inferences about the applicability of the Western Australian state government landfill levy from the contents of this document.

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